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NASA Technical Memorandum 81336

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# An Experimental Study of Transonic Flow About a Supercritical Airfoil

*Static Pressure and Drag Data Obtained  
From Tests of a Supercritical Airfoil and  
an NACA 0012 Airfoil at Transonic Speeds*

Frank W. Spaid,  
John A. Dahlin,  
Frederick W. Roos,  
and Louis S. Stivers, Jr.

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August 1983

**NASA**



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an NACA 0012 Airfoil at Transonic Speeds*

Frank W. Spaid  
*McDonnell Douglas Research Laboratories  
St. Louis, Missouri*

John A. Dahlin  
*Douglas Aircraft Company  
Long Beach, California*

Frederick W. Roos  
*McDonnell Douglas Research Laboratories  
St. Louis, Missouri*

Louis S. Stivers, Jr.  
*Ames Research Center  
Moffett Field, California*



National Aeronautics  
and Space Administration

Scientific and Technical  
Information Branch

1983





## SUMMARY

Surface static-pressure and drag data obtained from tests of two slightly modified versions of the original NASA Whitcomb airfoil section and a model of the NACA 0012 airfoil section are presented. Data for the supercritical airfoil were obtained for a free-stream Mach number range of 0.5 to 0.9, and a chord Reynolds number range of  $2 \times 10^6$  to  $4 \times 10^6$ . The NACA 0012 airfoil was tested at a constant chord Reynolds number of  $2 \times 10^6$  and a free-stream Mach number range of 0.6 to 0.8.

## INTRODUCTION

Data presented in this report were obtained from a cooperative program conducted by McDonnell Douglas Research Laboratories (MDRL), Douglas Aircraft Company (DAC), and Ames Research Center. This program was an experimental study of the steady and non-steady components of flow about (1) two slightly modified versions of the original NASA Whitcomb integral (unslotted), supercritical airfoil section, designated DSMA 523 (table 1), and (2) the NACA 0012 airfoil section. Although data from this program are presented and analyzed in references 1-7, most of the data presented in this report were excluded from those publications because of space limitations.

## SYMBOLS

ALPHA	angle of attack, roughly corrected for wind-tunnel-wall interference
AU	uncorrected angle of attack
$C_p$	pressure coefficient, $(p - p_\infty)/q_\infty$
$c_d$	airfoil section drag coefficient
$c_l$	airfoil section lift coefficient
MINF	free-stream Mach number
p	static pressure

$q_{\infty}$  free-stream dynamic pressure,  $1/2 \rho_{\infty} U_{\infty}^2$   
REC Reynolds number based on chord  
T bead diameter of boundary-layer trip, in.  
 $x/c$  distance along the chord line from the leading edge, normalized by the chord

## FACILITIES AND EQUIPMENT

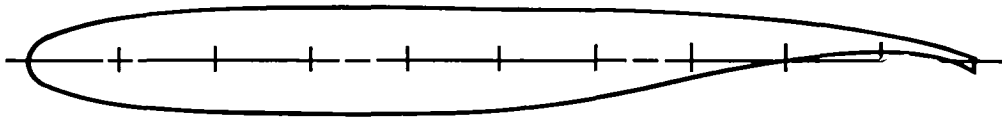
The experiments were conducted in the 2- by 2-Foot Transonic Wind Tunnel at Ames Research Center. This tunnel is a variable-speed, continuous-flow, ventilated-wall, variable-pressure facility, which was reengineered for optional two-dimensional research testing by adding rotating, model-supporting glass side windows mounted in unventilated, plane sidewalls. A unit Reynolds number of  $26.3 \times 10^6/m$  generally can be maintained while a high subsonic Mach number is held to within  $\pm 0.002$ . A remotely actuated 82-tube drag rake is programmed to provide total pressure readings at 1.3-mm intervals and static-pressure readings at 25.4-mm intervals across the wake of a model.

Airfoil models were mounted between the sidewall windows, and a traversing rig or a drag rake was mounted on the tunnel sting. Two 15.24-cm-chord models of the supercritical airfoil were used during these experiments. One model has a nominally sharp trailing edge, and the other has a blunt trailing edge equal to 1% chord, formed by downward rotation of the aft lower-surface contour from 65% chord to the trailing edge. Coordinates for these models are given in table 1. The NACA 0012 model has a chord of 15.24 cm.

## DATA PRESENTATION

The data are presented in appendixes A through C in the form of plotted static-pressure distributions; geometric or roughly corrected angle of attack ( $\alpha$ ), lift coefficient ( $c_l$ ), and drag coefficient ( $c_d$ ) values tabulated on the plots. The data were obtained from several tunnel-occupancy periods over a period of several years; the data are identified by run number and year. Run schedules, tables A1, B1, and C1, are presented at the beginning of each appendix as a guide to the plotted data.

TABLE 1.- DSMA 523 AIRFOIL COORDINATES, SHARP AND BLUNT TRAILING EDGES



$x/c$	$z_{upper}$ c	$z_{lower}$ c	$x/c$	$z_{upper}$ c	$z_{lower}$ c (sharp TE)	$z_{lower}$ c (blunt TE)
0.000500	0.005069	-0.005096	0.440000	0.055247	-0.053009	
0.001000	0.007096	-0.007128	0.460000	0.055146	-0.052143	
0.002500	0.011063	-0.011078	0.480000	0.054973	-0.051136	
0.005000	0.015320	-0.015320	0.500000	0.054723	-0.049915	
0.007500	0.018417	-0.018417	0.520000	0.054390	-0.048483	
0.010000	0.020716	-0.020671	0.540000	0.053976	-0.046780	
0.012500	0.022651	-0.022548	0.560000	0.053486	-0.044613	
0.015000	0.024267	-0.024135	0.580000	0.052917	-0.052006	
0.020000	0.026918	-0.026744	0.600000	0.052269	-0.038885	
0.030000	0.030729	-0.030667	0.620000	0.051540	-0.035181	
0.040000	0.033459	-0.033607	0.640000	0.050726	-0.030940	
0.060000	0.037407	-0.038087	0.660000	0.049826	-0.026087	-0.026390
0.080000	0.040367	-0.041739	0.680000	0.048832	-0.020633	-0.021541
0.100000	0.042987	-0.044648	0.700000	0.047725	-0.015445	-0.016958
0.120000	0.045198	-0.046796	0.720000	0.046494	-0.010574	-0.012692
0.140000	0.047017	-0.048616	0.740000	0.045130	-0.006027	-0.008750
0.160000	0.048543	-0.050114	0.760000	0.043625	-0.001872	-0.005200
0.180000	0.049828	-0.051348	0.780000	0.041942	0.001892	-0.002041
0.200000	0.050902	-0.052370	0.800000	0.040043	0.005224	(+)0.000686
0.220000	0.051802	-0.053207	0.820000	0.037907	0.008108	0.002965
0.240000	0.052563	-0.053890	0.840000	0.035502	0.010505	0.004757
0.260000	0.053199	-0.054423	0.860000	0.032780	0.012374	0.006021
0.280000	0.053729	-0.054808	0.880000	0.029666	0.013645	0.006687
0.300000	0.054161	-0.055056	0.900000	0.026155	0.014169	0.006606
0.320000	0.054513	-0.055163	0.920000	0.022185	0.013798	0.005630
0.340000	0.054788	-0.055137	0.950000	0.017708	0.012338	0.003565
0.360000	0.054998	-0.054978	0.960000	0.012642	0.009726	(+)0.000348
0.380000	0.055149	-0.054701	0.980000	0.006842	0.005773	-0.004210
0.400000	0.055240	-0.054283	1.000000	(+)0.000308	0.000498	-0.010109
0.420000	0.055272	-0.053719	Leading-edge radius/c = 0.023			

## APPENDIX A

### DSMA 523 MODEL, SHARP TRAILING EDGE, 1975 AND 1977

The data obtained during 1975 are labeled 02/02/76 or 02/03/76 on each plot, and have run numbers 41-111. Drag data were obtained only during the 1975 occupancy period. Values of  $T$  for the 1975 data are bead diameters of the boundary-layer trip, in inches. The quantity  $\text{ALPHA}$  is the angle of attack, roughly corrected for wind-tunnel-wall interference. At the higher Mach numbers, this correction produces lift-curve slopes for this airfoil that are obviously too large. The data obtained during 1977 have the year in the plot titles, and have run numbers 2-84. The quantity  $\text{AU}$  is the uncorrected angle of attack.

TABLE A1.- RUN SCHEDULE, DSMA 523 MODEL, SHARP TRAILING EDGE

(1975 data)

Run no.	Nominal $M_\infty$	Nominal $Re_c$	Boundary-layer trip			
			Upper		Lower	
			x/c	T (in.)	x/c	T (in.)
41-43	0.76	$4 \times 10^6$	0.35	0.0030	0.18	0.0030
44	.78	$4 \times 10^6$				
45-46	.76	$4 \times 10^6$				
47	.80	$3 \times 10^6$				
48	.76	$4 \times 10^6$				
49	.80	$3 \times 10^6$			↓	↓
52-55	.76	$4 \times 10^6$			.06	.0020
56	.80	$3 \times 10^6$			.06	.0020
59-60	.76	$4 \times 10^6$			.35	.0035
61-62	.80	$3 \times 10^6$			.35	.0035
65	.76	$4 \times 10^6$			.35	.0035
66	.76	$4 \times 10^6$			natural	
67	.76	$4 \times 10^6$			.06	.0020
68	.80	$3 \times 10^6$			.06	.0020
69	.76	$4 \times 10^6$			.18	.0038
70	.76	$4 \times 10^6$		↓	.18	.0049
71	.76	$2 \times 10^6$		.0049	.35	.0049
72	.80	$2 \times 10^6$		↓	↓	↓
73-76	.76	$2 \times 10^6$				
77	.50	$2 \times 10^6$			↓	↓
78	.80	$2 \times 10^6$				
79	.76	$2 \times 10^6$		↓	.18	.0045
80	.80	$2 \times 10^6$				.0045
81	.76	$4 \times 10^6$		.0030		.0035
82	.80	$3 \times 10^6$		↓		.0035
83-84	.76	$4 \times 10^6$				.0038
85	.76	$4 \times 10^6$				.0030
86	.80	$3 \times 10^6$				.0038
87-88	.76	$4 \times 10^6$				↓
89	.80	$3 \times 10^6$				
90	.50	$4 \times 10^6$	↓	↓	↓	↓

TABLE A1.- Concluded.

(1975 data)

Run no.	Nominal $M_\infty$	Nominal $Re_c$	Boundary-layer trip			
			Upper		Lower	
			x/c	T (in.)	x/c	T (in.)
91	0.50	$4 \times 10^6$	0.35	0.0030	0.18	0.0049
92	.74	$4 \times 10^6$	↓	↓	↓	↓
93	.60	$4 \times 10^6$	↓	↓	↓	↓
94	.74	$4 \times 10^6$	↓	↓	↓	↓
95	.78	$3 \times 10^6$	↓	↓	↓	↓
97	.50	$4 \times 10^6$	↓	↓	↓	↓
98-99	.72	$4 \times 10^6$	↓	↓	↓	↓
100	.82	$3 \times 10^6$	↓	↓	↓	↓
101	.64	$4 \times 10^6$	↓	↓	↓	↓
102	.68	$4 \times 10^6$	↓	↓	↓	↓
103	.78	$3 \times 10^6$	↓	↓	↓	↓
106	.76	$4 \times 10^6$	↓	↓	↓	↓
					plus tape triangle at $x/c = 0.52$	
107	.50	$4 \times 10^6$	.05	.0020	.18	.0049
108	.68	$4 \times 10^6$	.05	.0020	↓	.0049
109	.76	$4 \times 10^6$	.35	.0030	↓	.0063
110	.80	$3 \times 10^6$	.35	.0030	↓	.0063
111	.50	$4 \times 10^6$	.35	.0030	↓	.0063
			(1977 data)			
2	0.80	$2 \times 10^6$	0.35	0.0053	0.18	0.0053
38	↓	$3 \times 10^6$	↓	.0032	.06	.0019
50	↓	$3 \times 10^6$	↓	↓	.18	.0032
61	↓	$3 \times 10^6$	↓	↓	.35	.0038
72	↓	$3 \times 10^6$	↓	↓	.18	.0053
84	.60	$4 \times 10^6$	.05	.0020	.18	.0053

WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

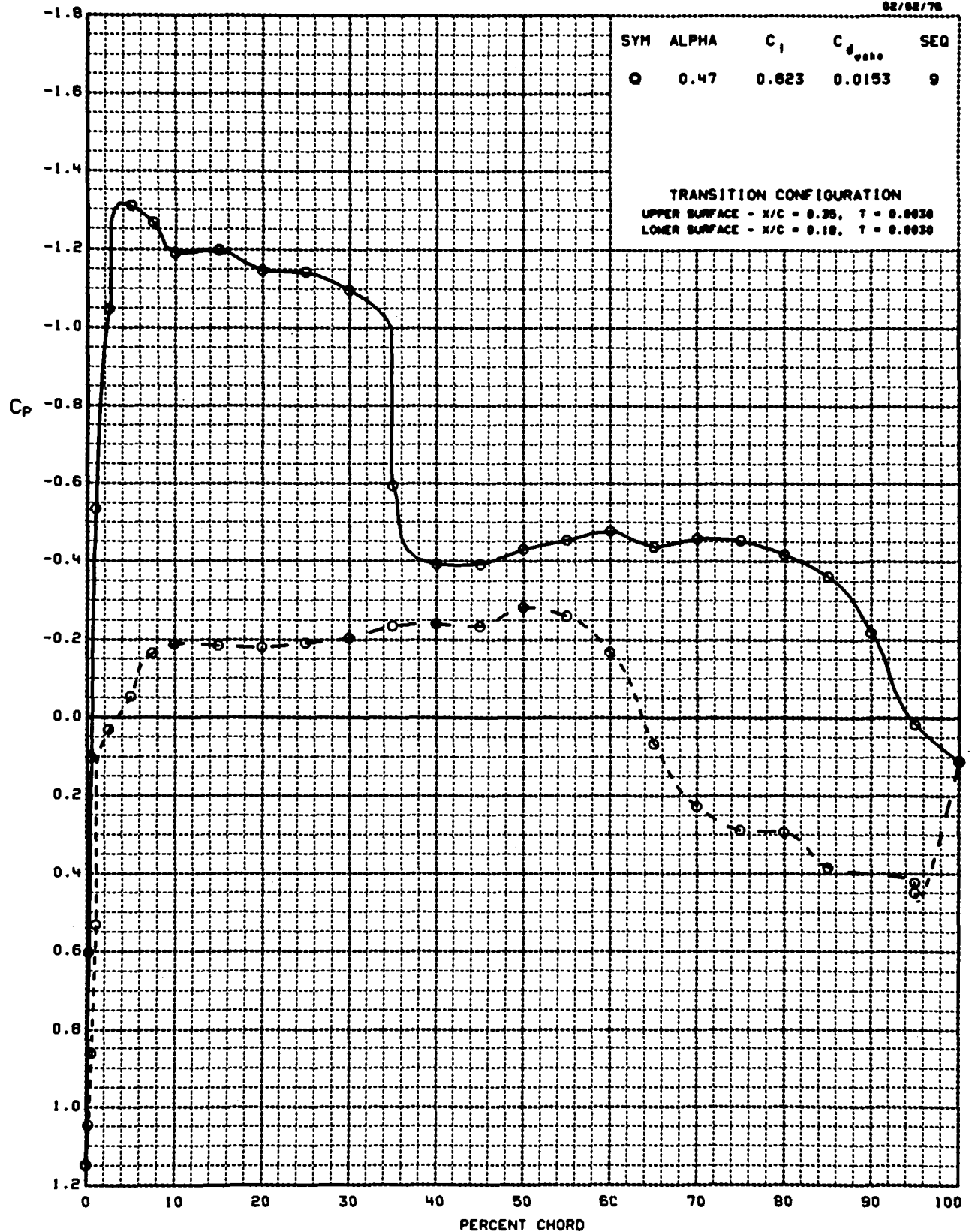
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RUN = 41

AMES 22-060-5

02/02/76



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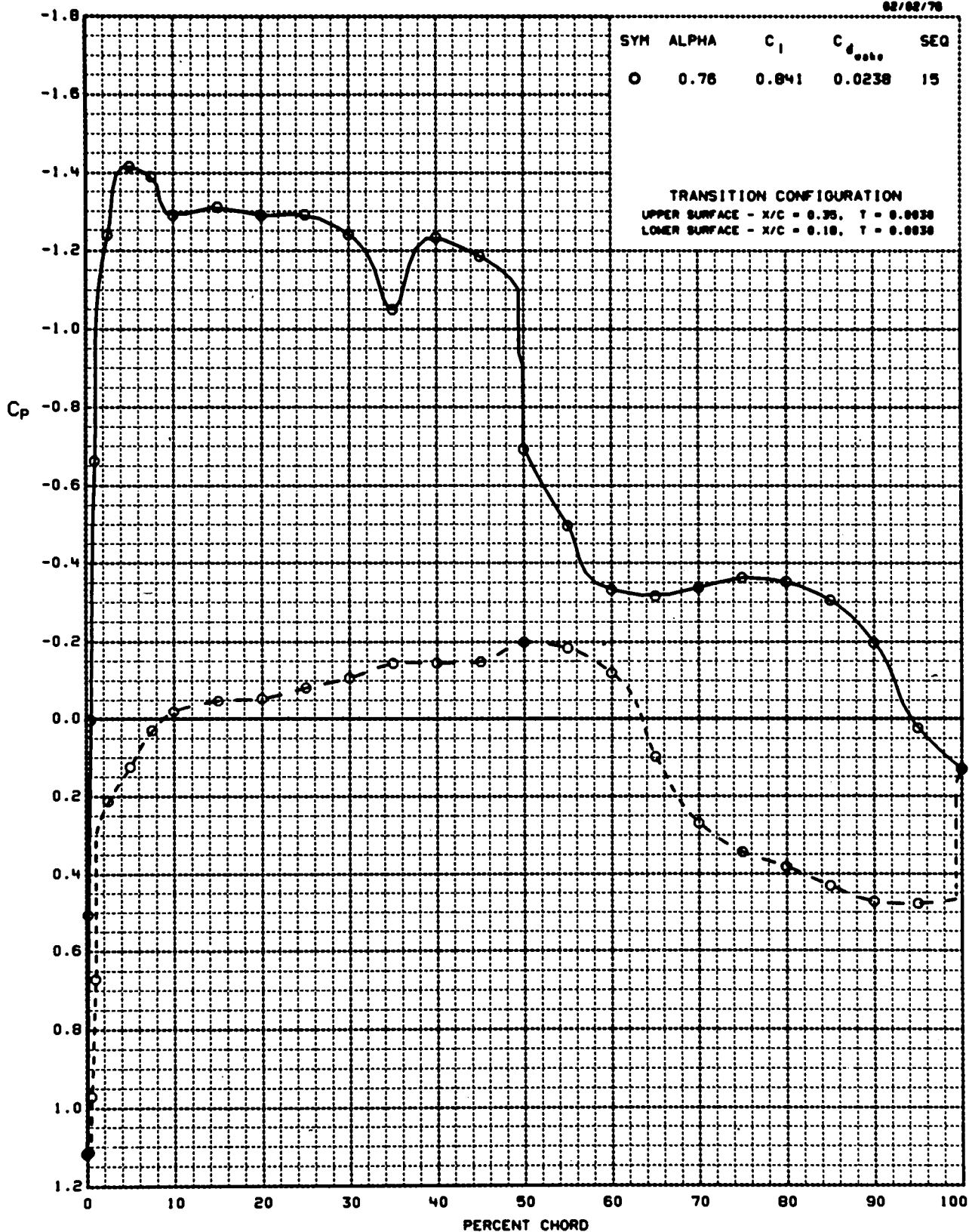
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REYNOLDS NUMBER =  $3.93 \times 10^6$

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AMES 22-060-5

02/02/78





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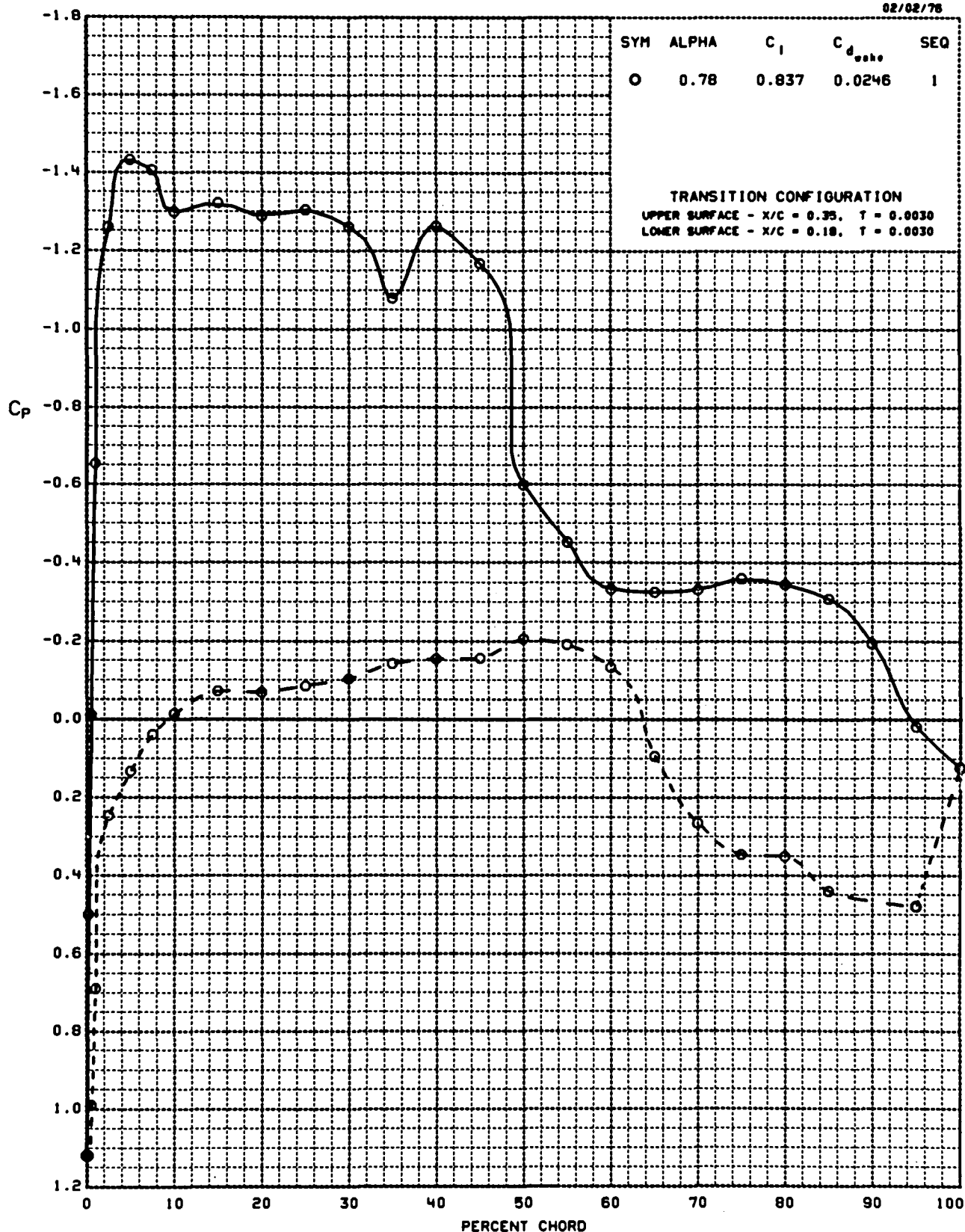
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RUN = 43

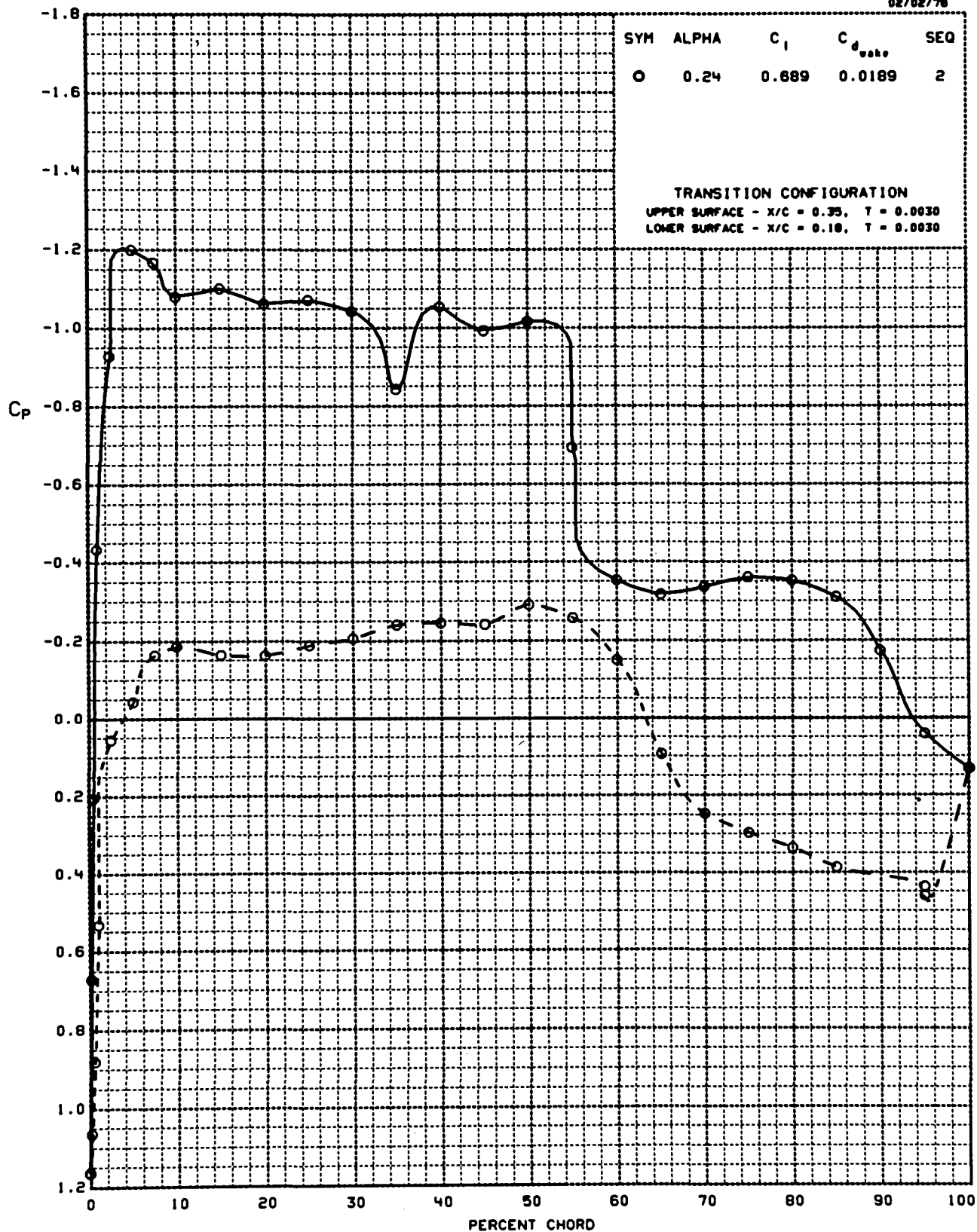
AMES 22-060-5

02/02/76



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
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MACH NUMBER = 0.784 REYNOLDS NUMBER =  $3.91 \times 10^8$  RUN = 44 AMES 22-060-5

02/02/78



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
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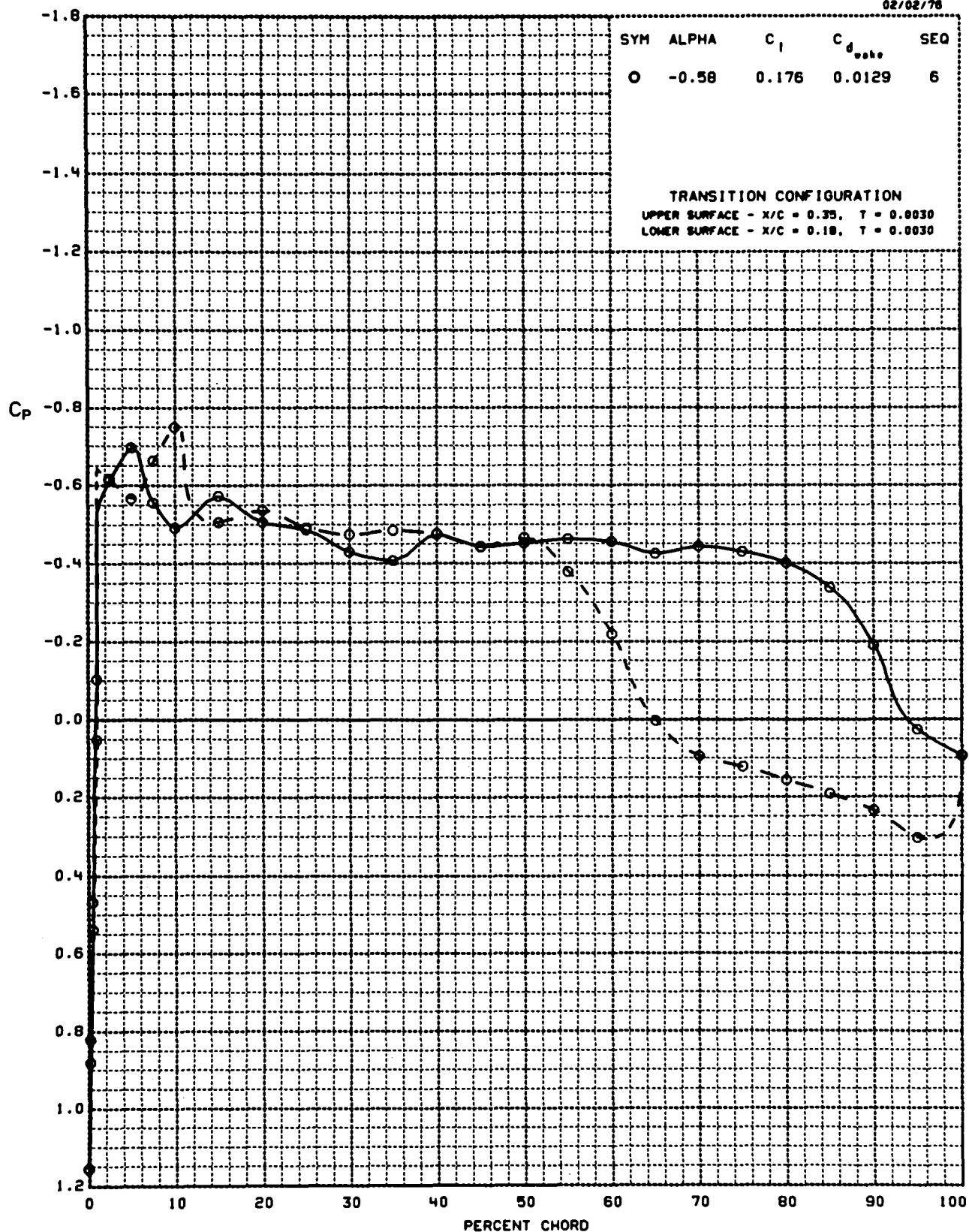
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RUN = 45

AMES 22-060-5

02/02/76



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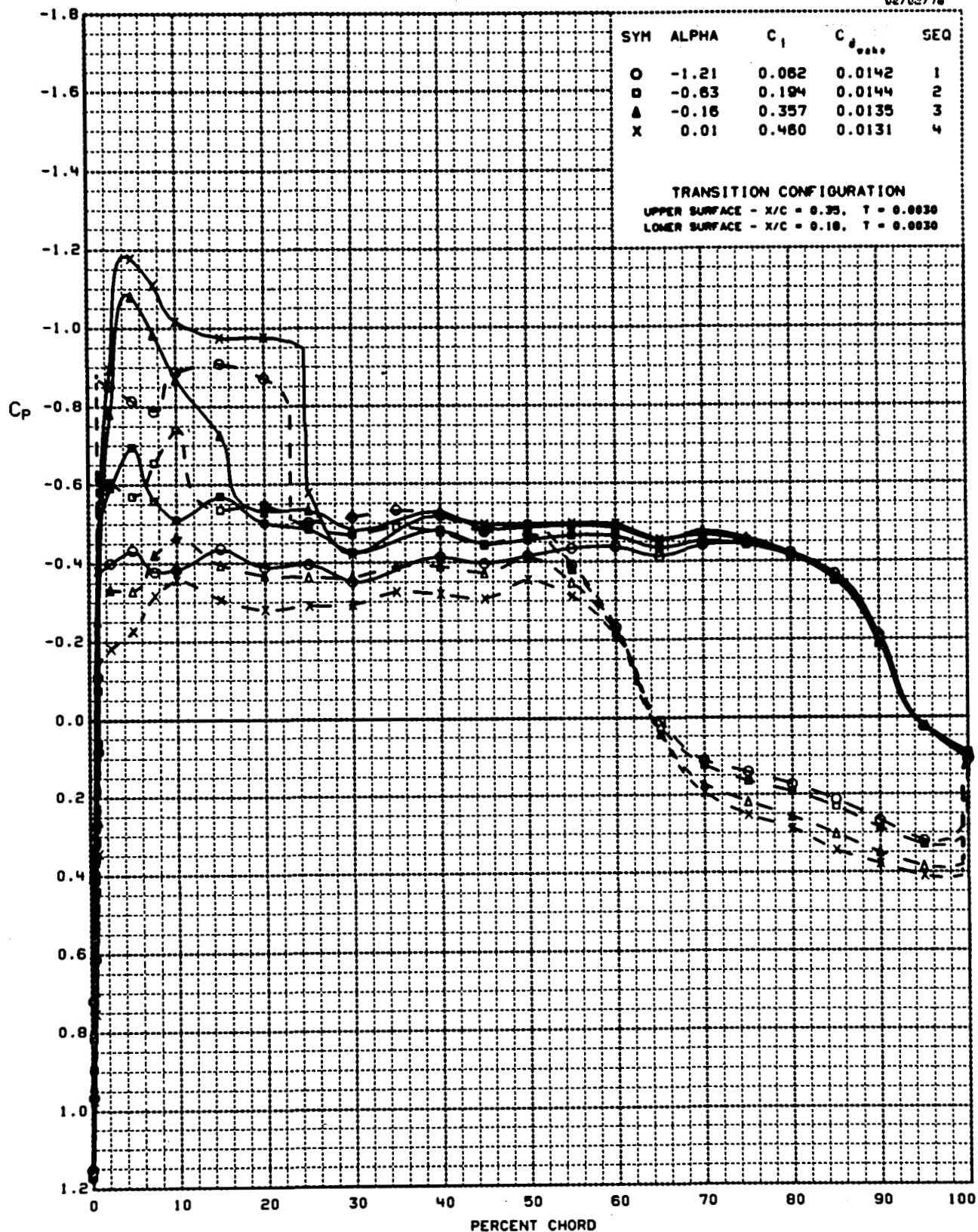
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REYNOLDS NUMBER =  $3.96 \times 10^6$

RUN = 46

AMES 22-000-5

02/03/78



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

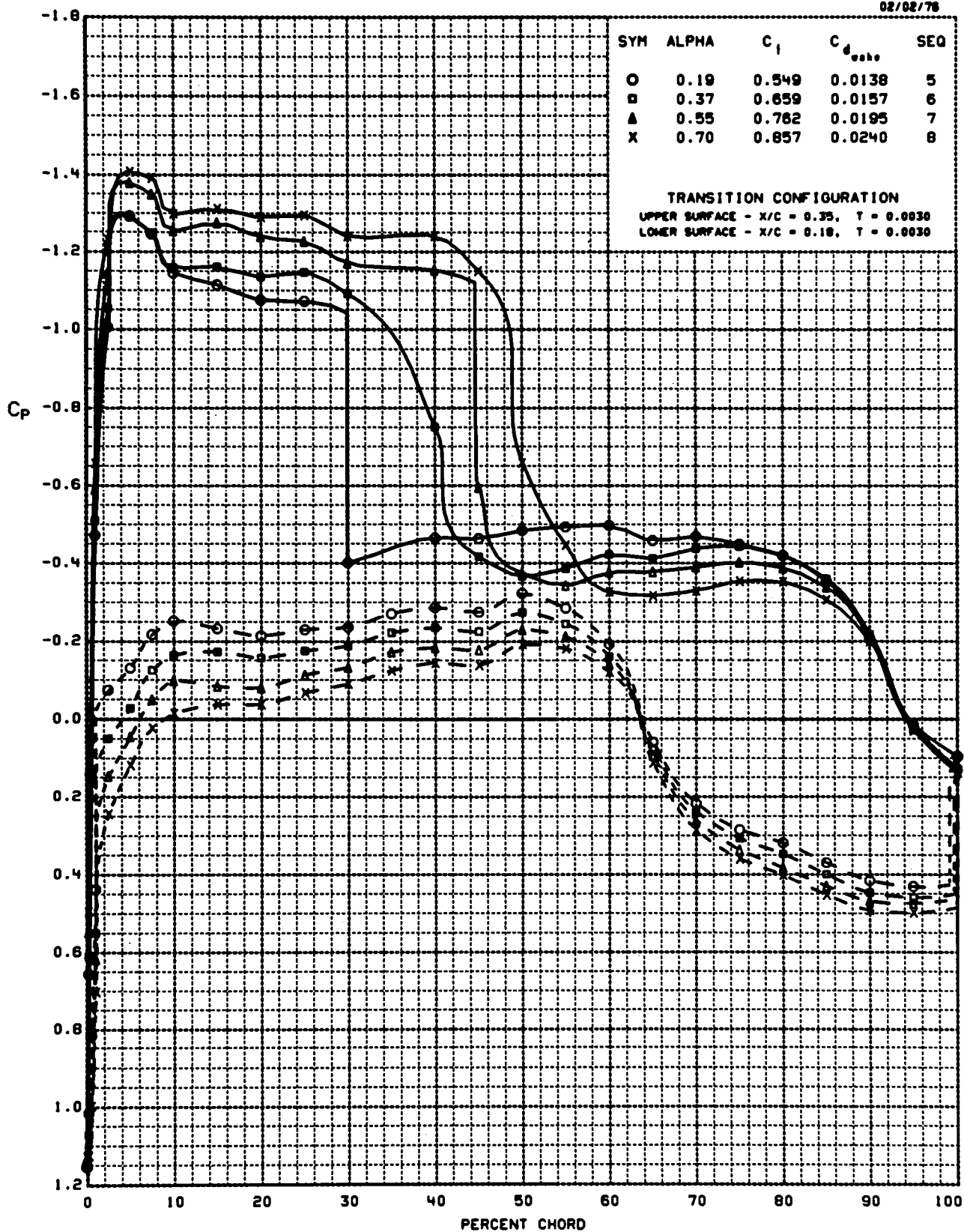
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AMES 22-060-5

02/02/76



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

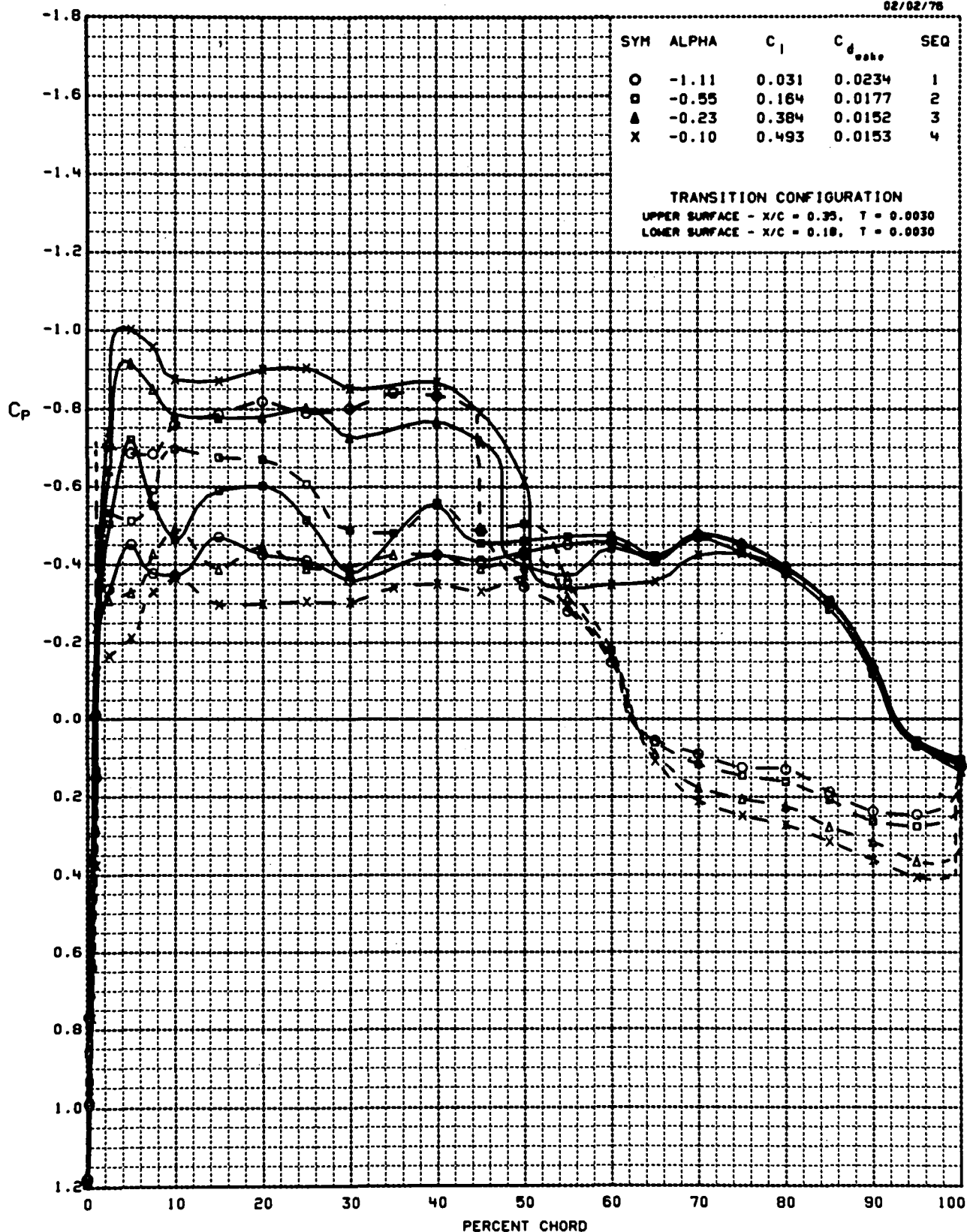
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RUN = 47

AMES 22-060-5

02/02/78



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

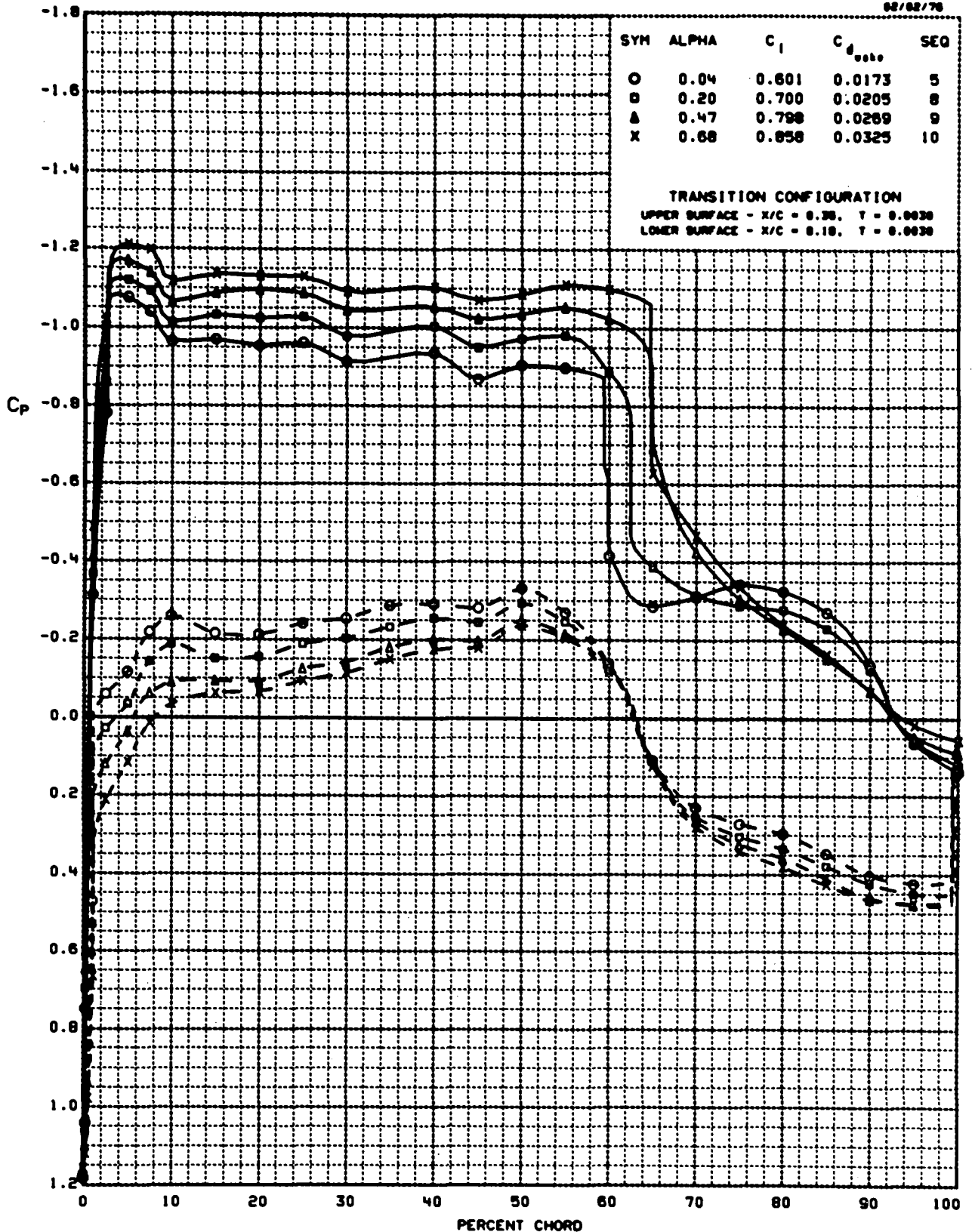
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REYNOLDS NUMBER =  $2.99 \times 10^6$

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AMES 22-060-5

02/02/78





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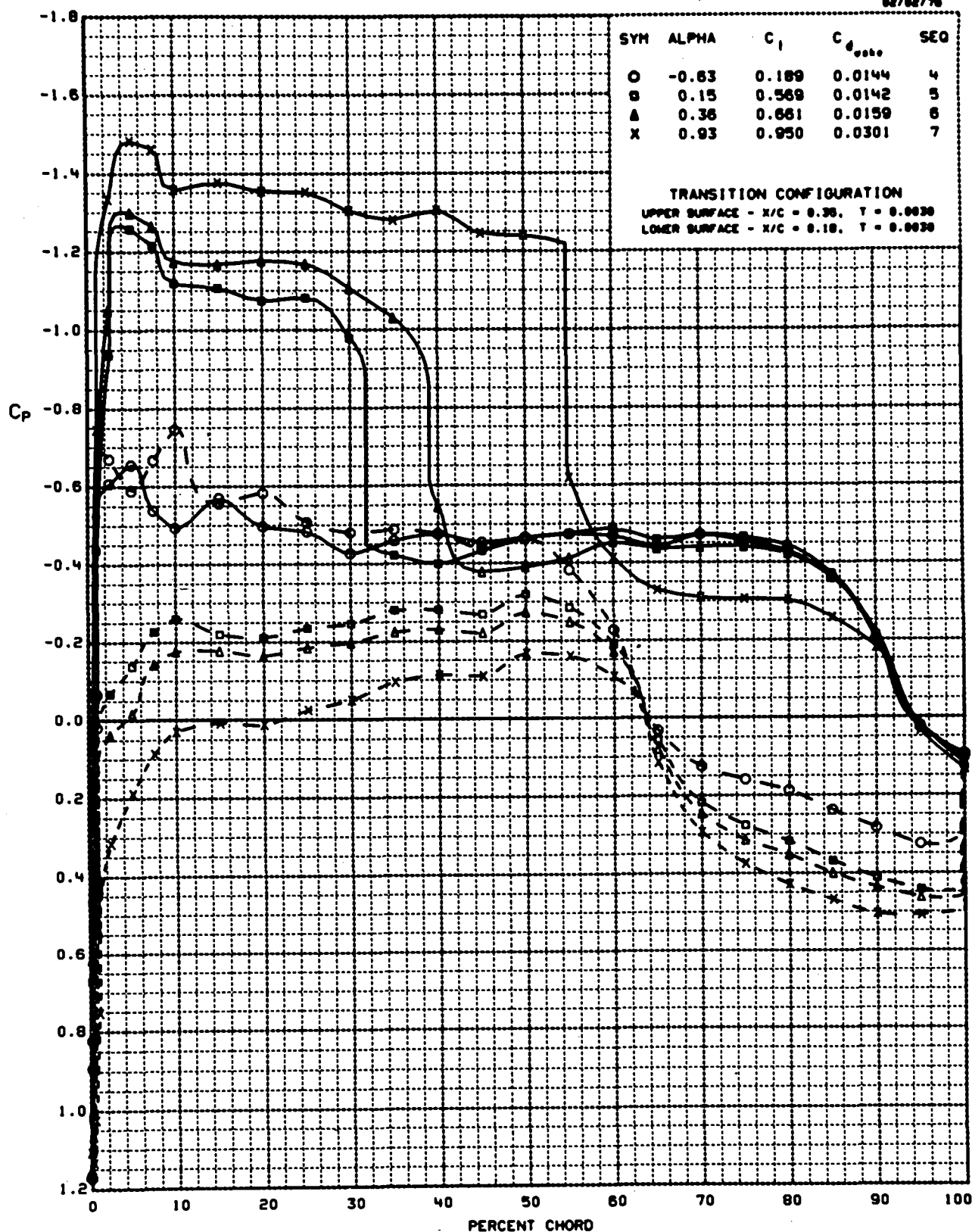
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RUN = 48

AMES 22-060-5

02/02/78





WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

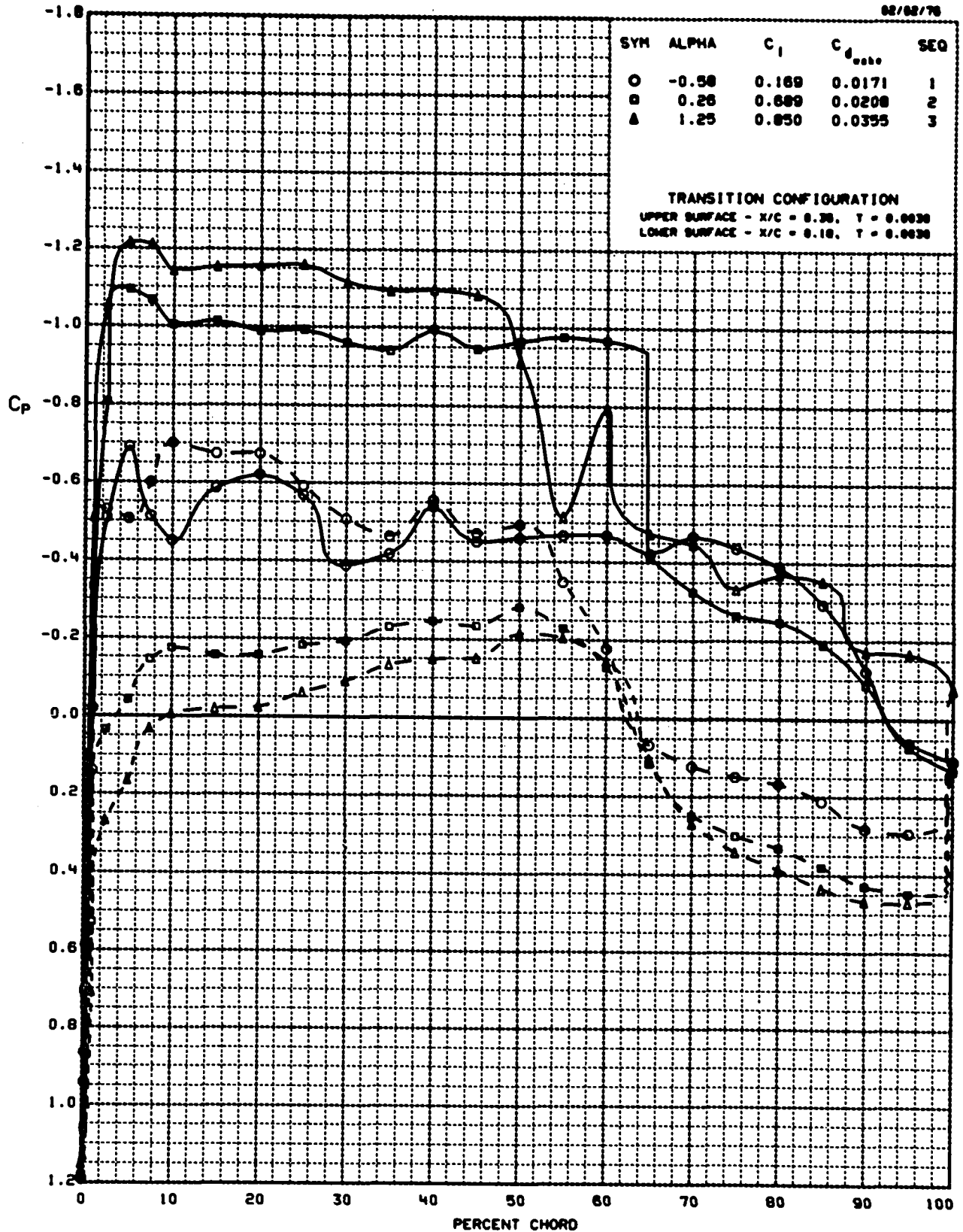
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AMES 22-060-5

02/02/78



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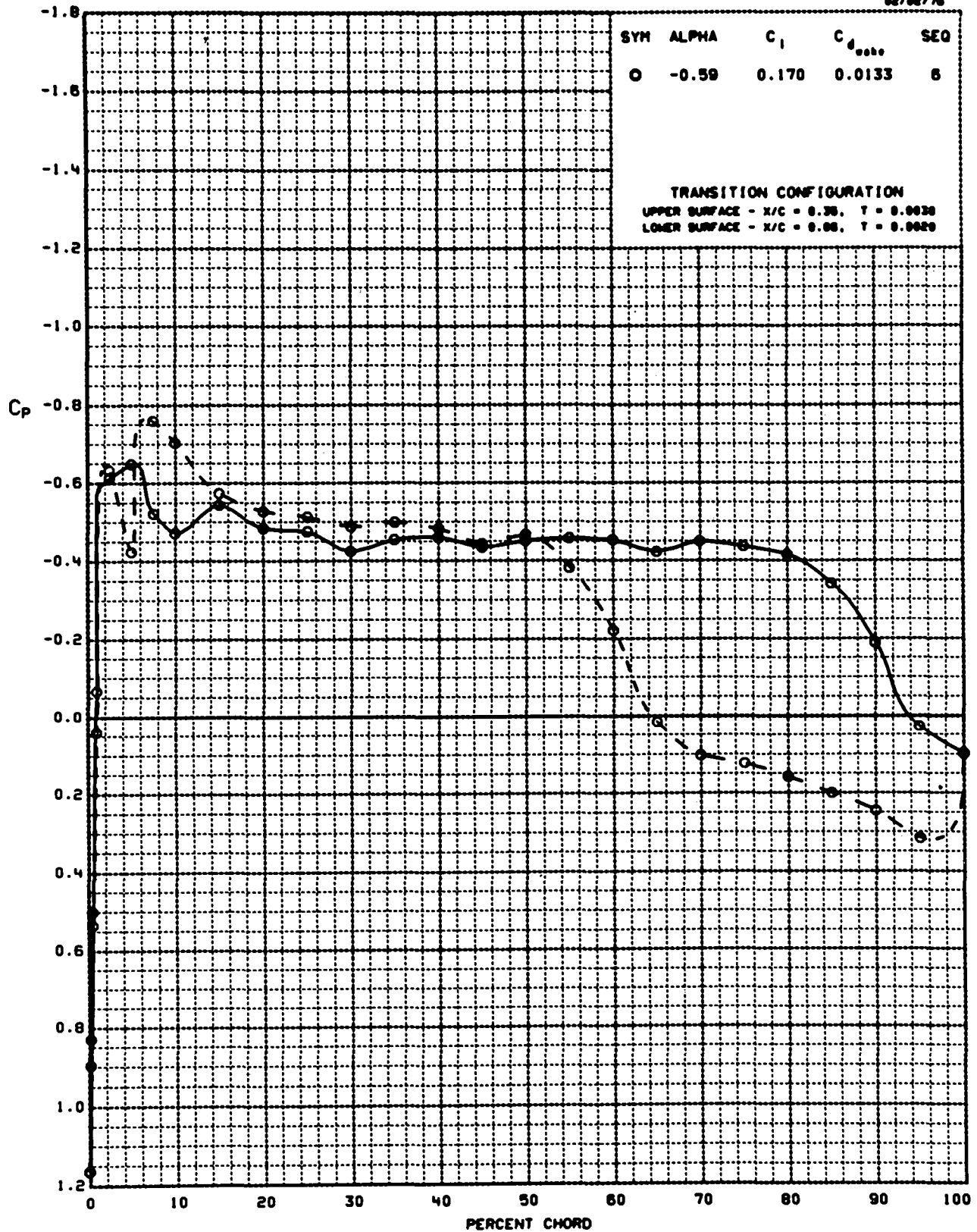
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RUN = 52

AMES 22-060-5

02/02/76



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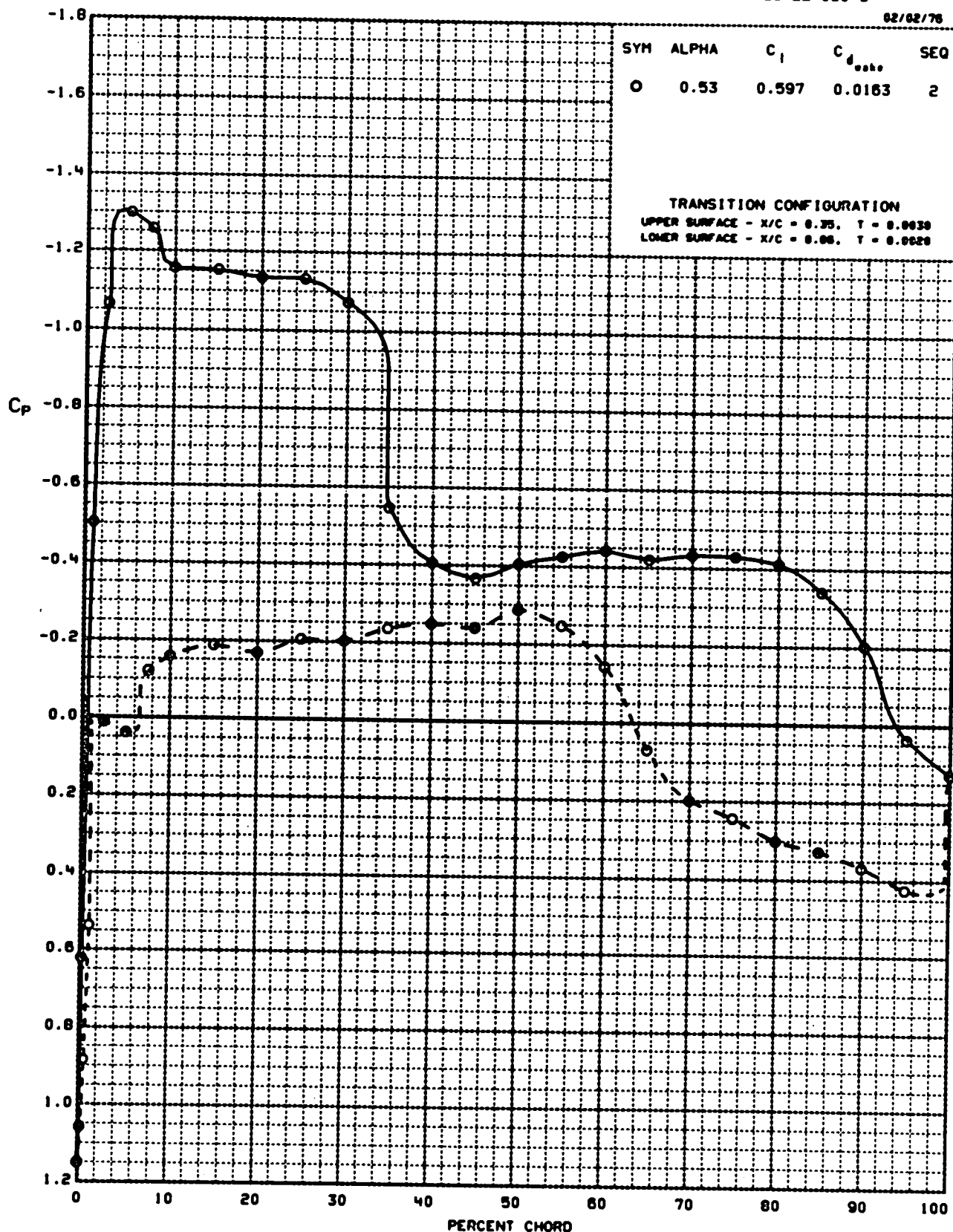
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AMES 22-060-5

62/62/76



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

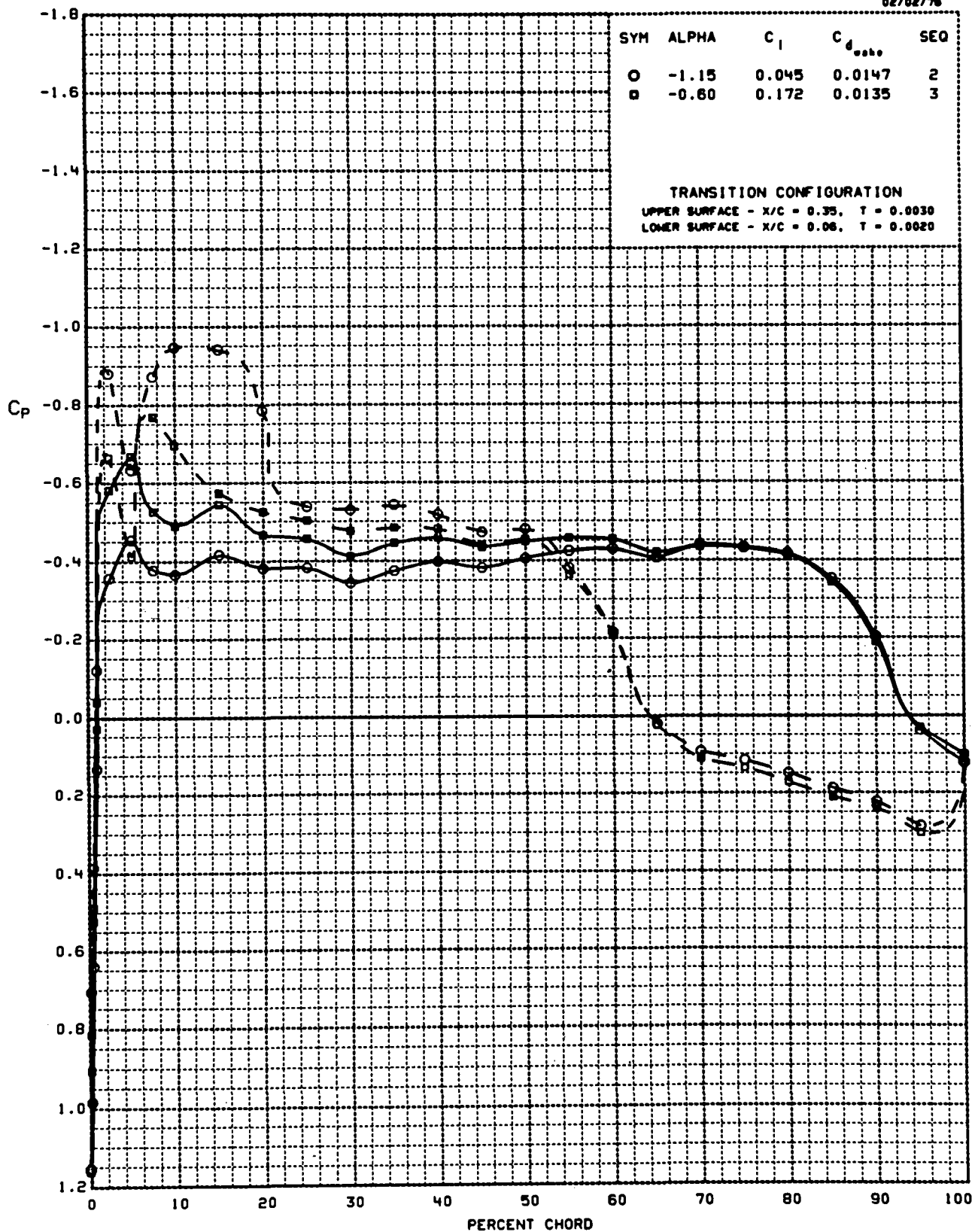
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RUN = 54

AMES 22-060-5

02/02/78



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

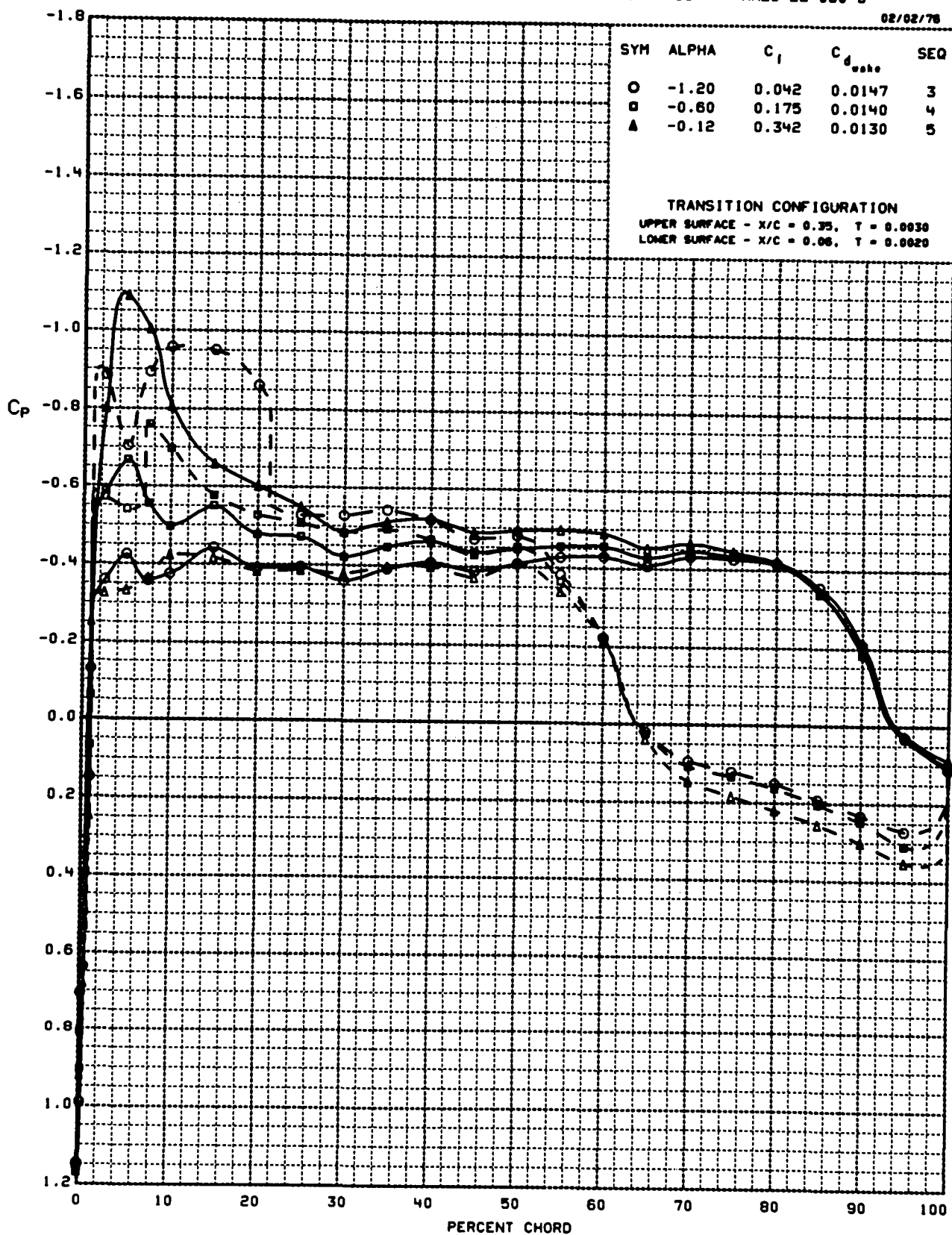
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RUN = 55

AMES 22-060-5

02/02/76



# WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

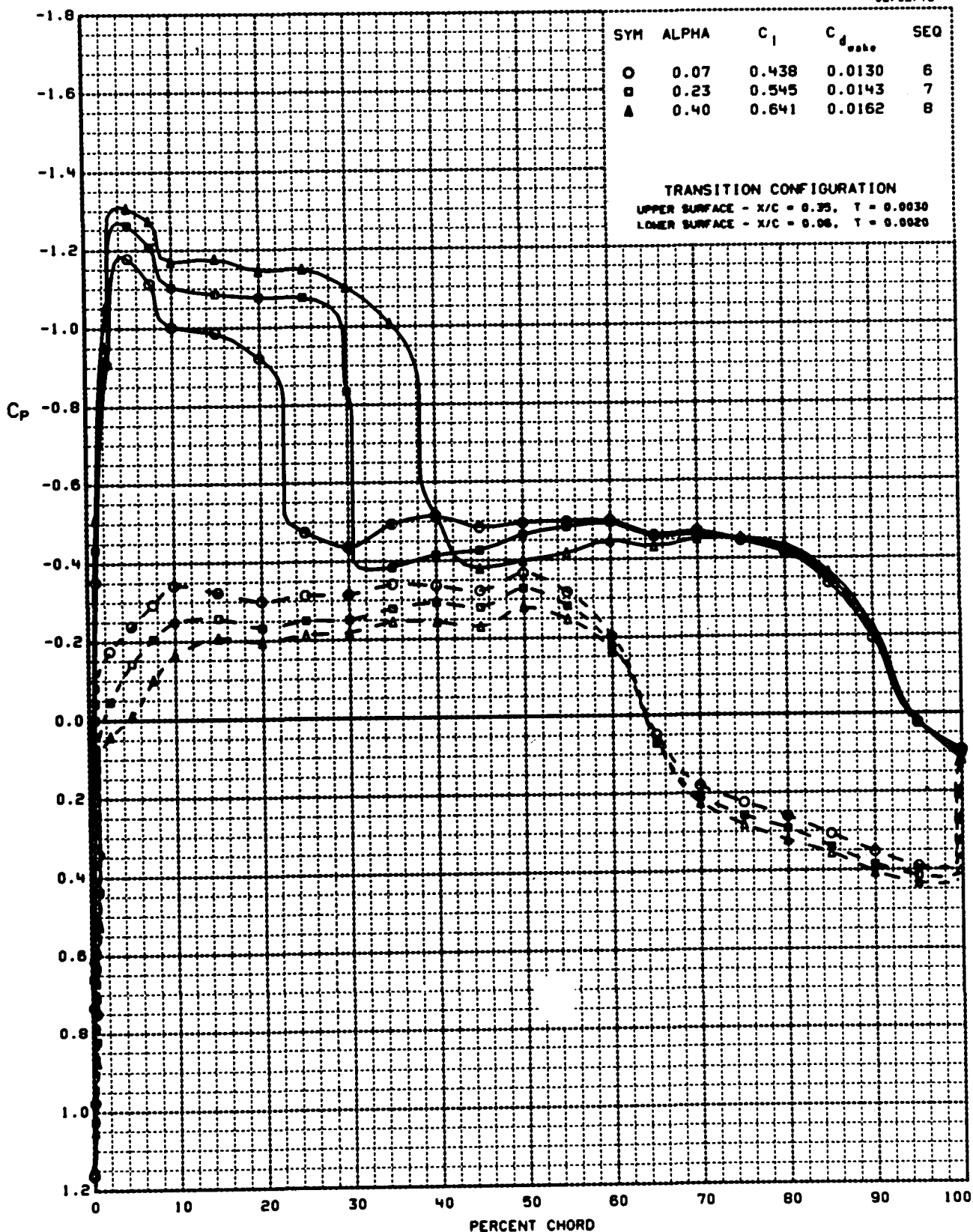
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REYNOLDS NUMBER =  $3.92 \times 10^8$

RUN = 55

AMES 22-060-5

02/02/76



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

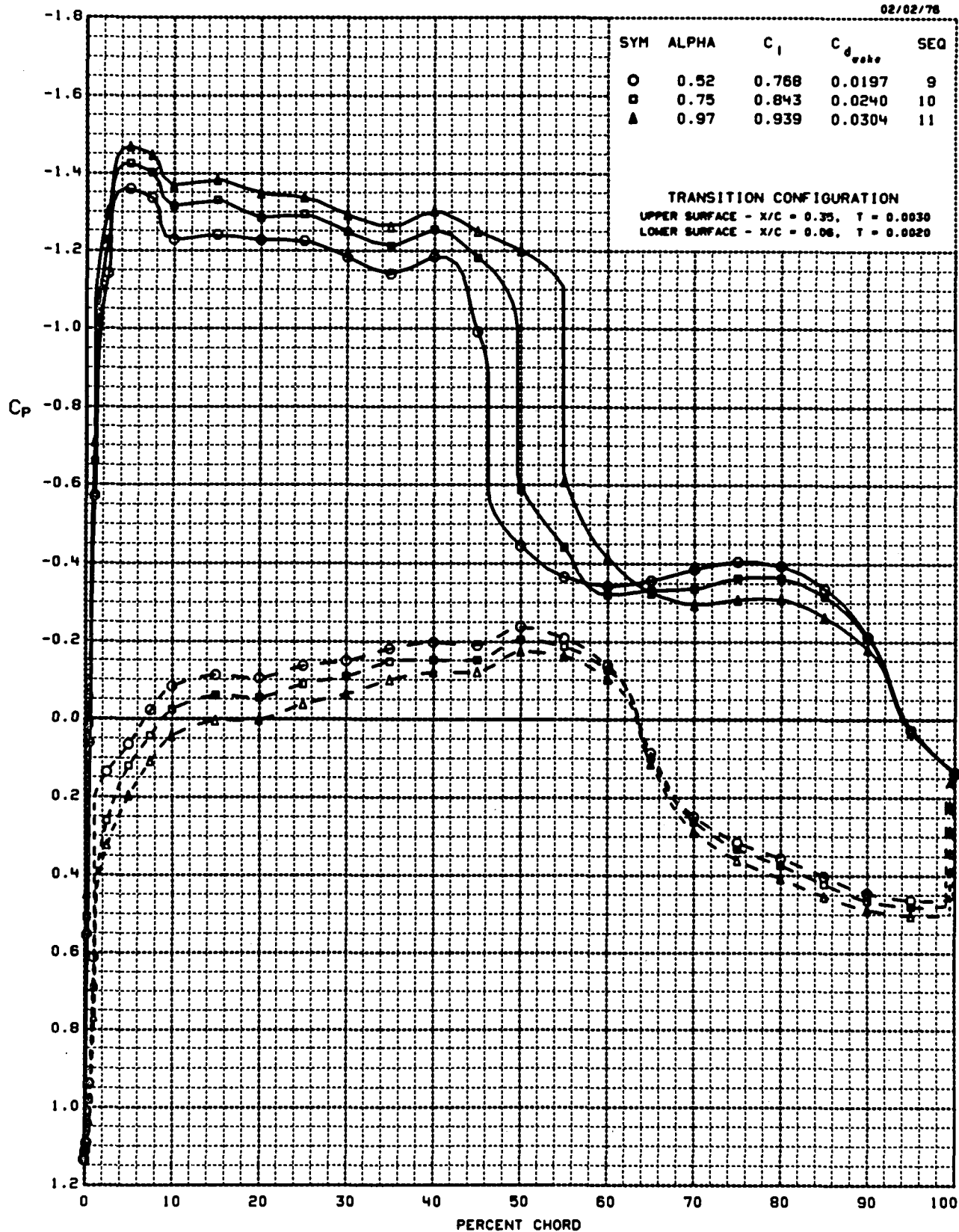
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REYNOLDS NUMBER =  $3.95 \times 10^6$

RUN = 55

AMES 22-060-5

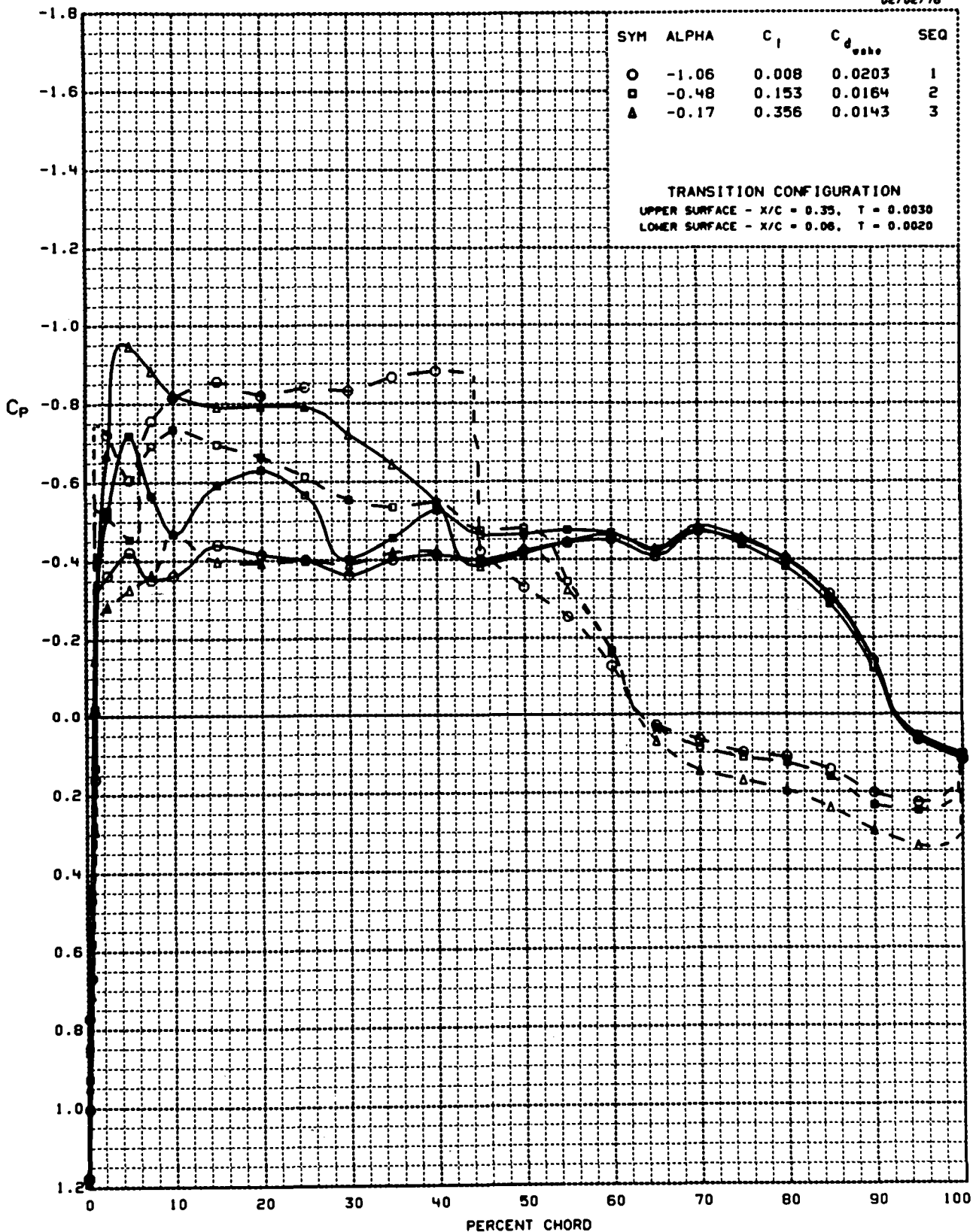
02/02/78





WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS  
MACH NUMBER = 0.801 REYNOLDS NUMBER =  $3.03 \times 10^6$  RUN = 56 AMES 22-060-5

02/02/78





# WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

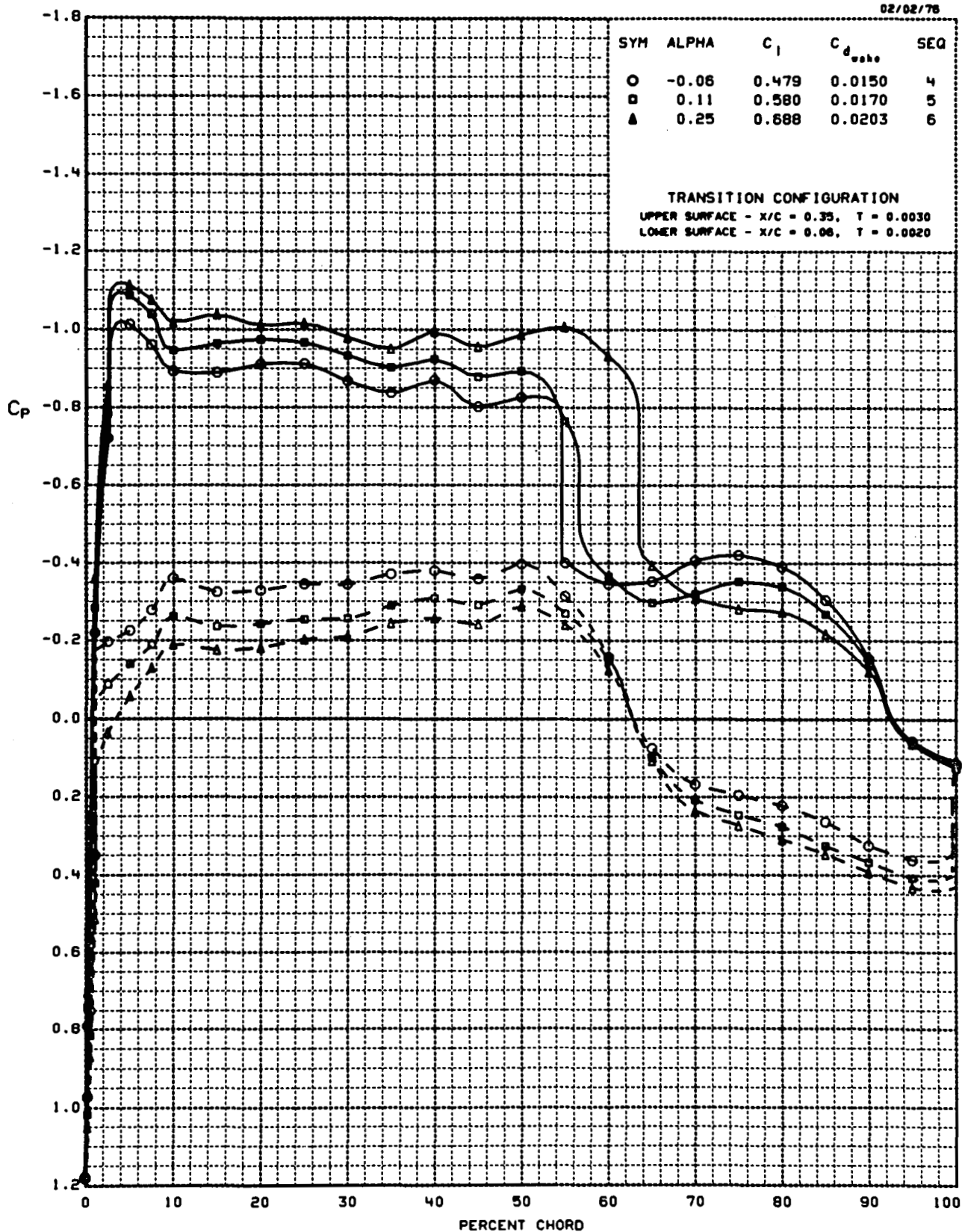
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RUN = 56

AMES 22-060-5

02/02/76



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

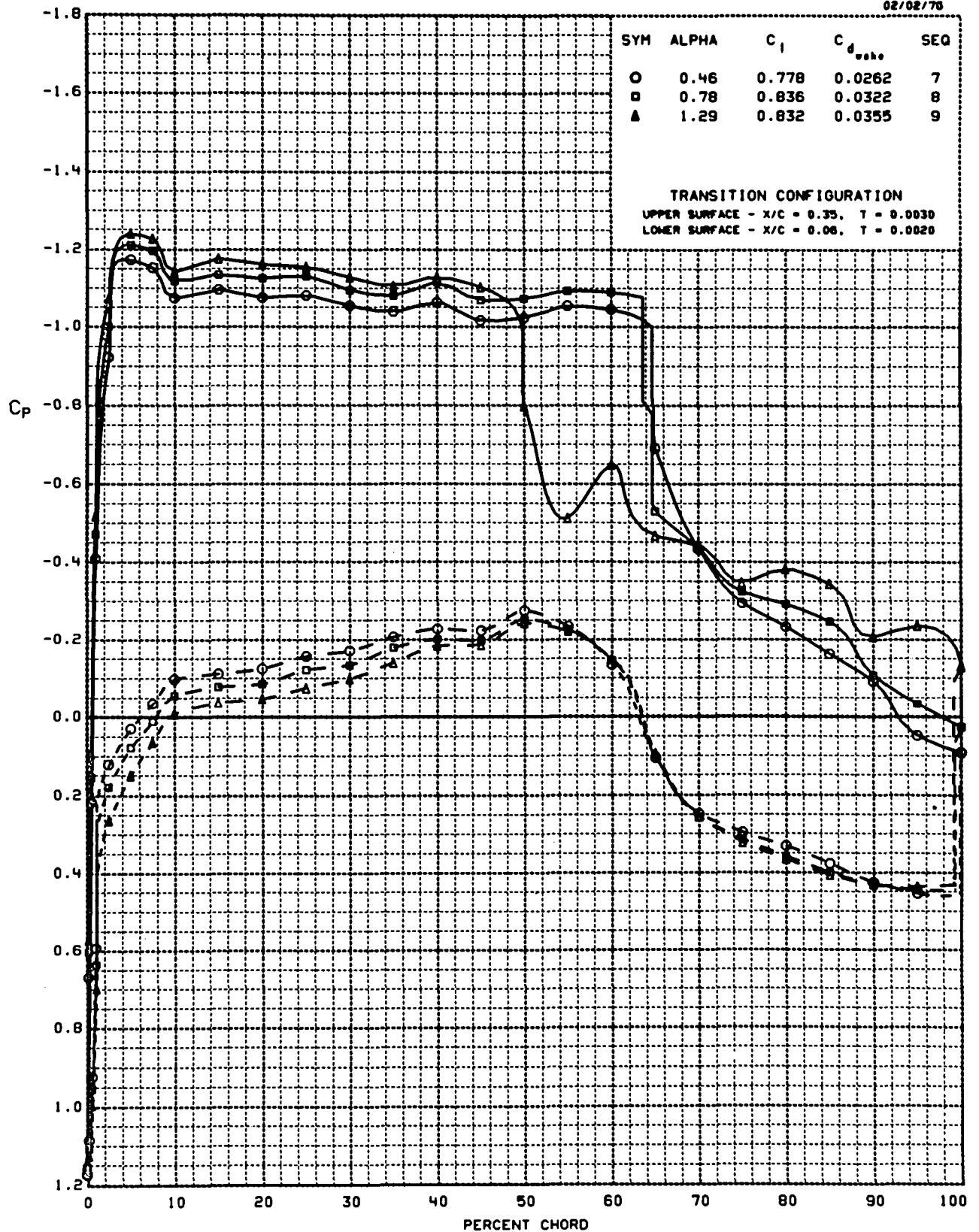
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REYNOLDS NUMBER =  $2.95 \times 10^6$

RUN = 56

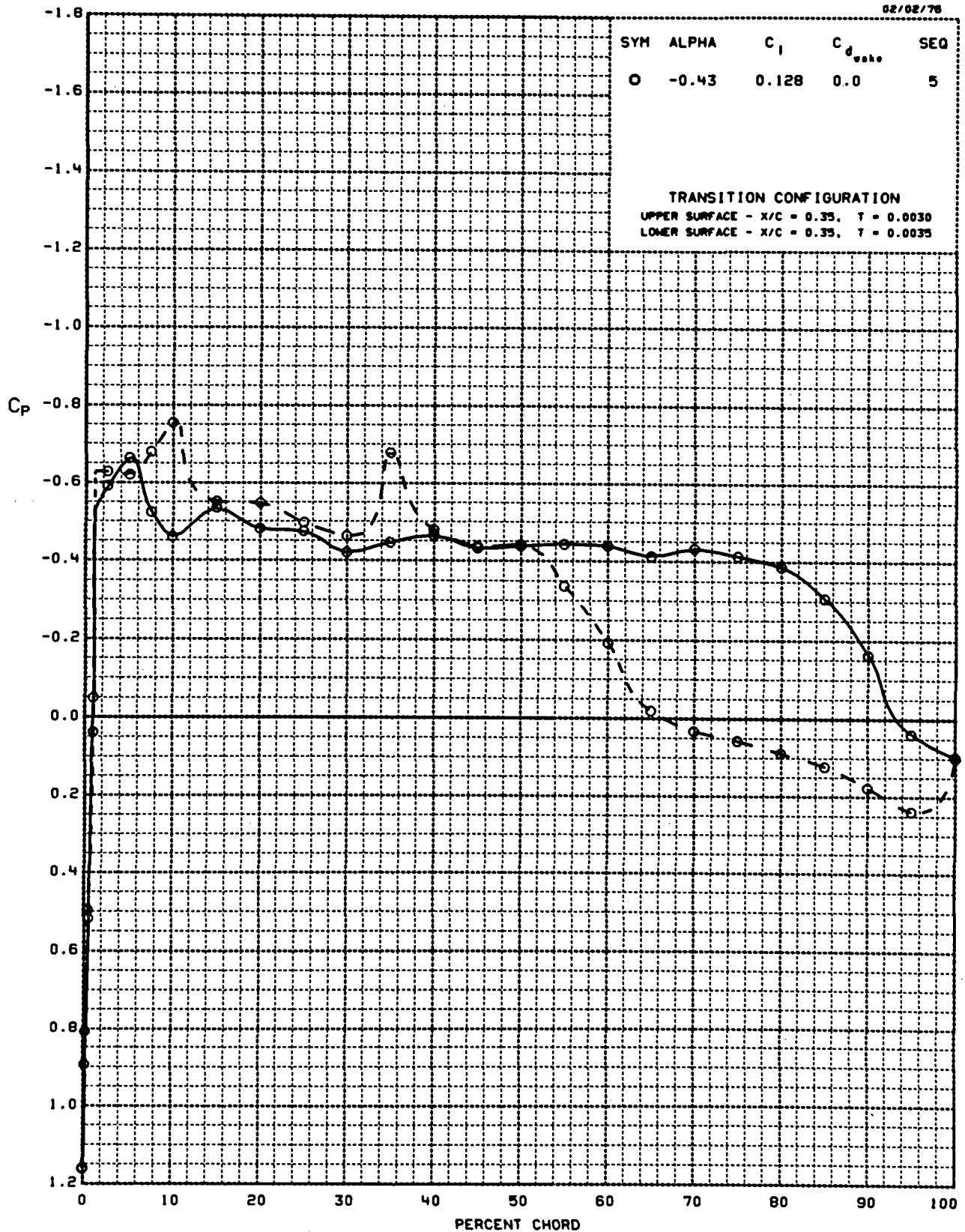
AMES 22-060-5

02/02/78



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS  
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02/02/76



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

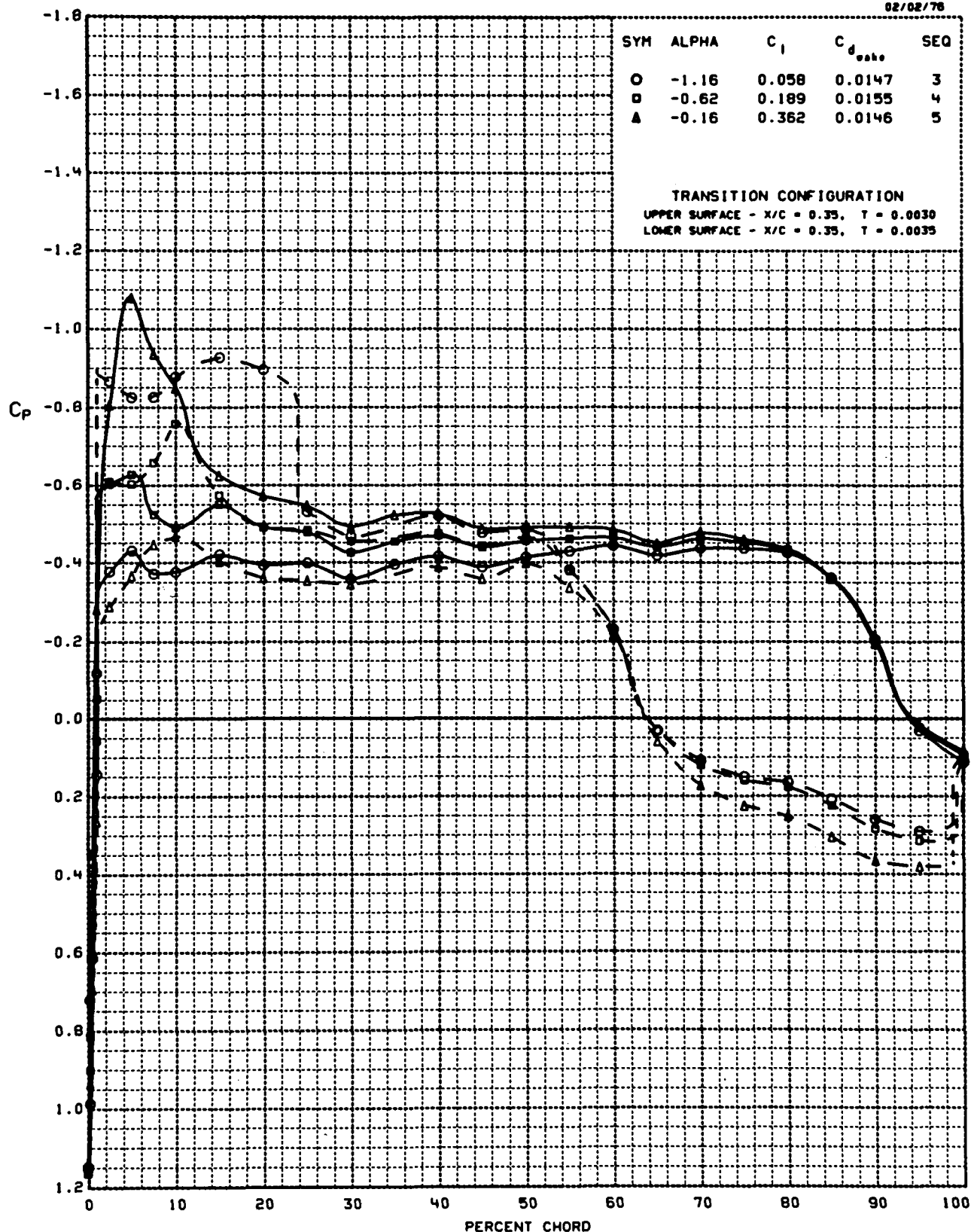
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REYNOLDS NUMBER =  $4.04 \times 10^6$

RUN = 60

AMES 22-060-5

02/02/76



# WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

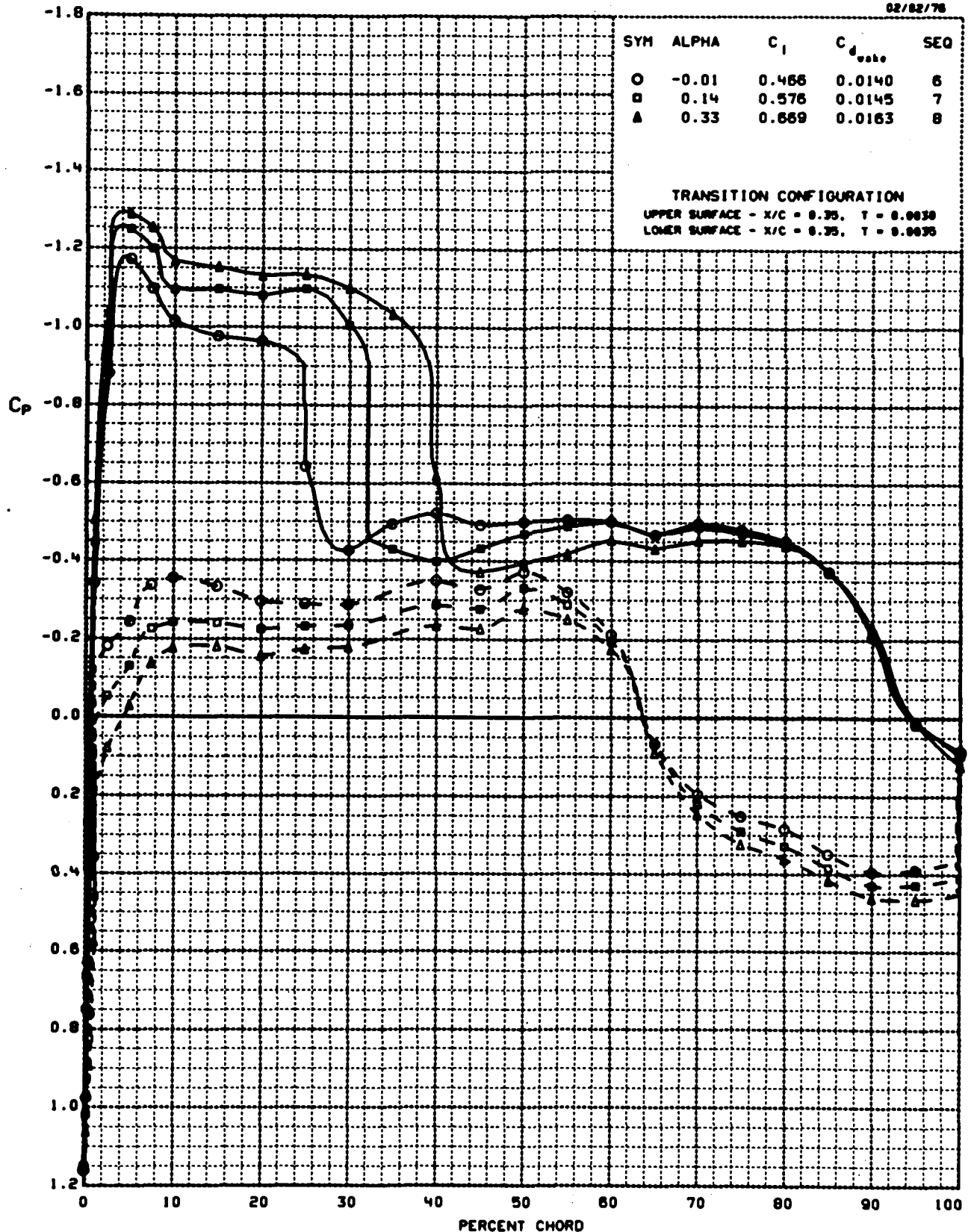
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REYNOLDS NUMBER =  $3.97 \times 10^6$

RUN = 60

AMES 22-060-5

02/02/76



# WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

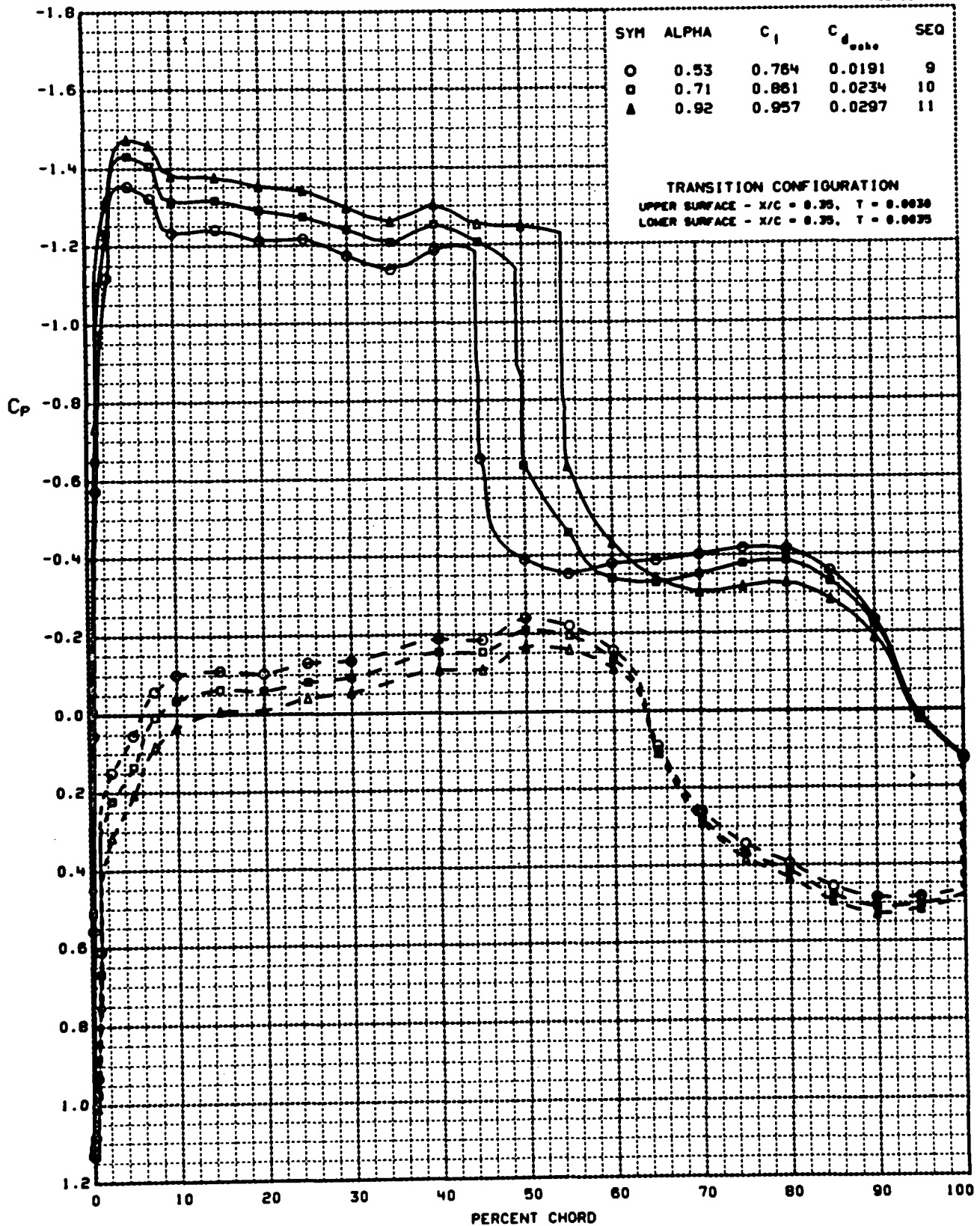
MACH NUMBER = 0.760

REYNOLDS NUMBER =  $3.92 \times 10^6$

RUN = 60

AMES 22-060-5

02/02/76



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

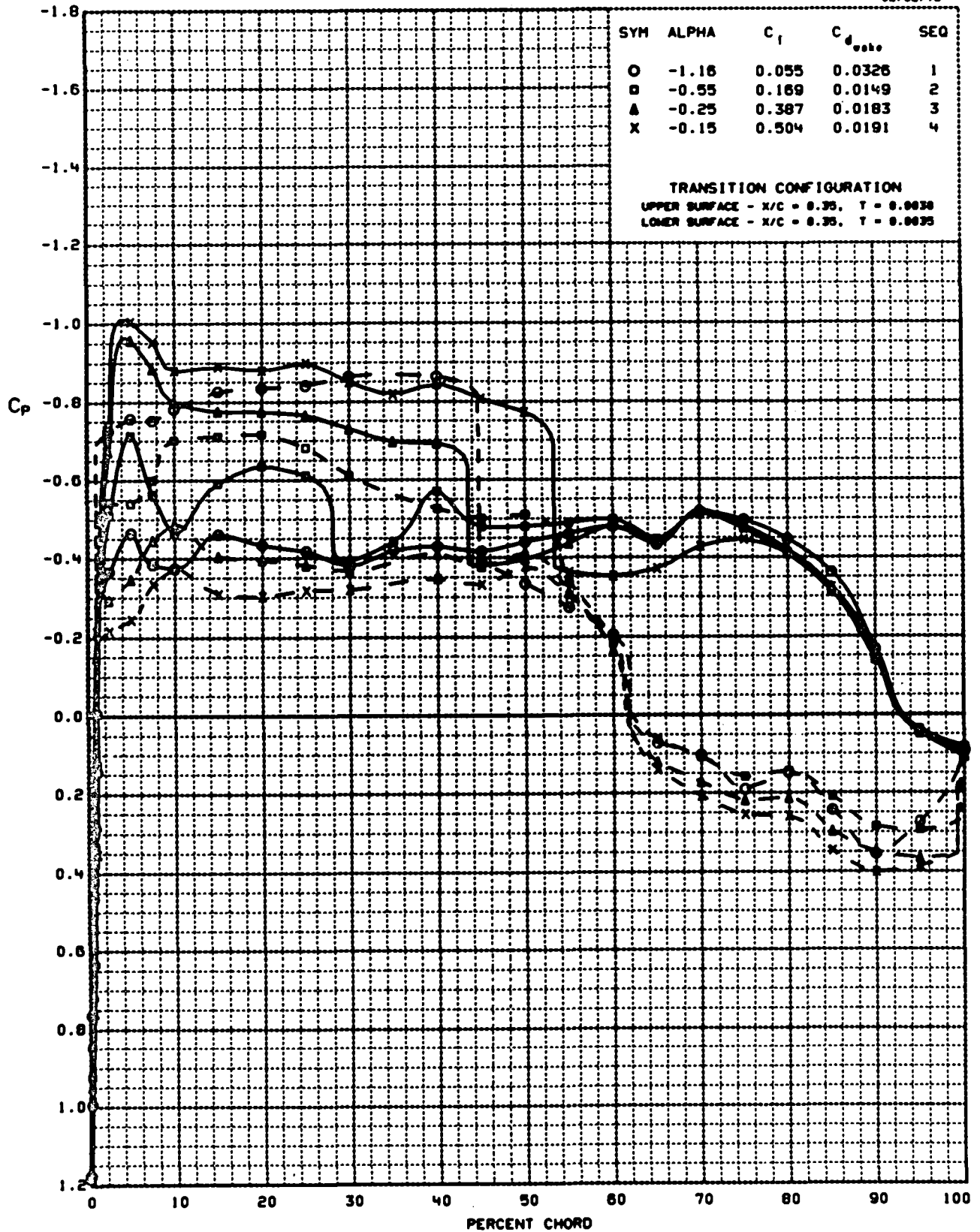
MACH NUMBER = 0.801

REYNOLDS NUMBER =  $3.01 \times 10^6$

RUN = 61

AMES 22-060-5

02/02/76





# WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

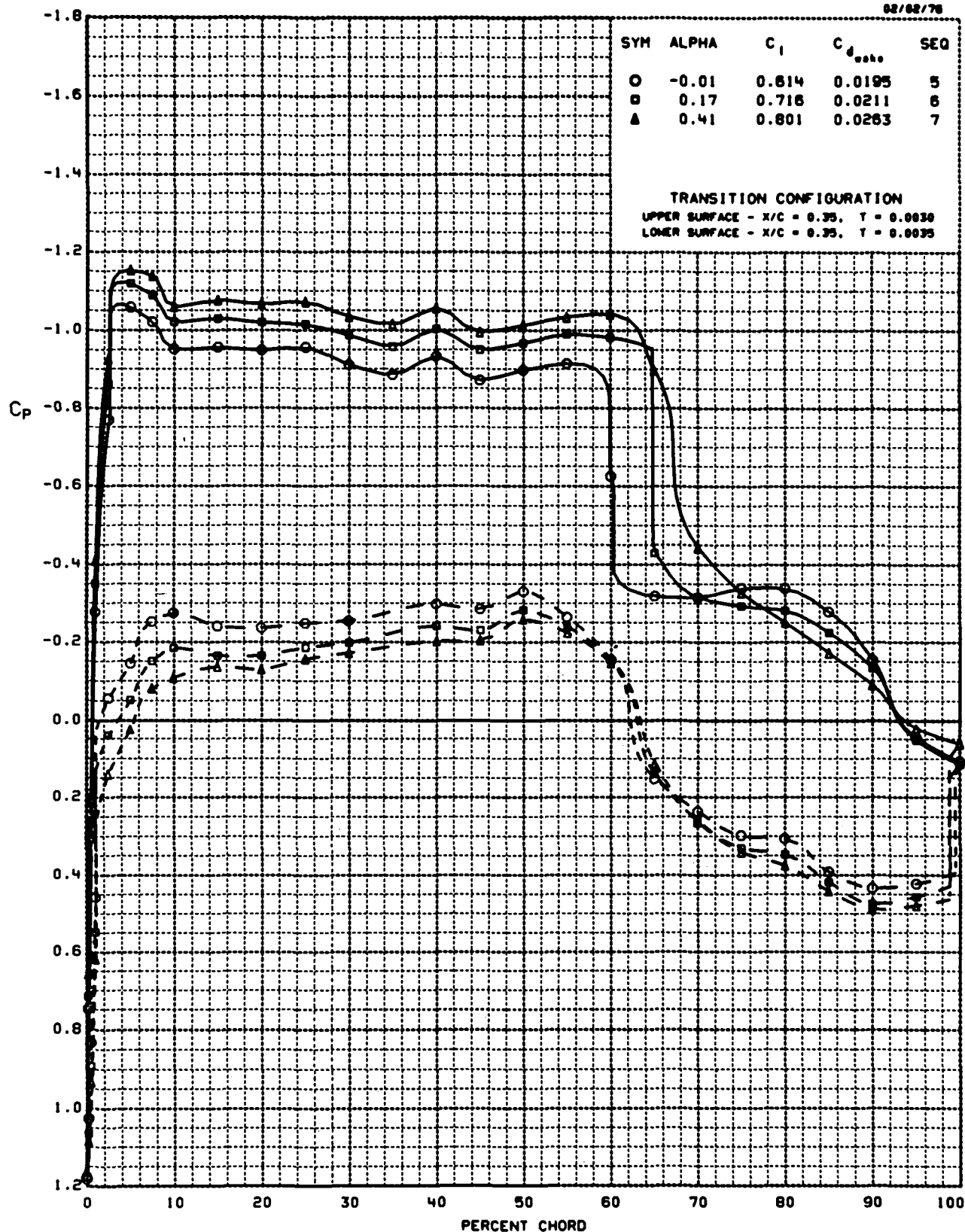
MACH NUMBER = 0.802

REYNOLDS NUMBER =  $2.98 \times 10^6$

RUN = 61

AMES 22-060-5

02/02/76





# WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

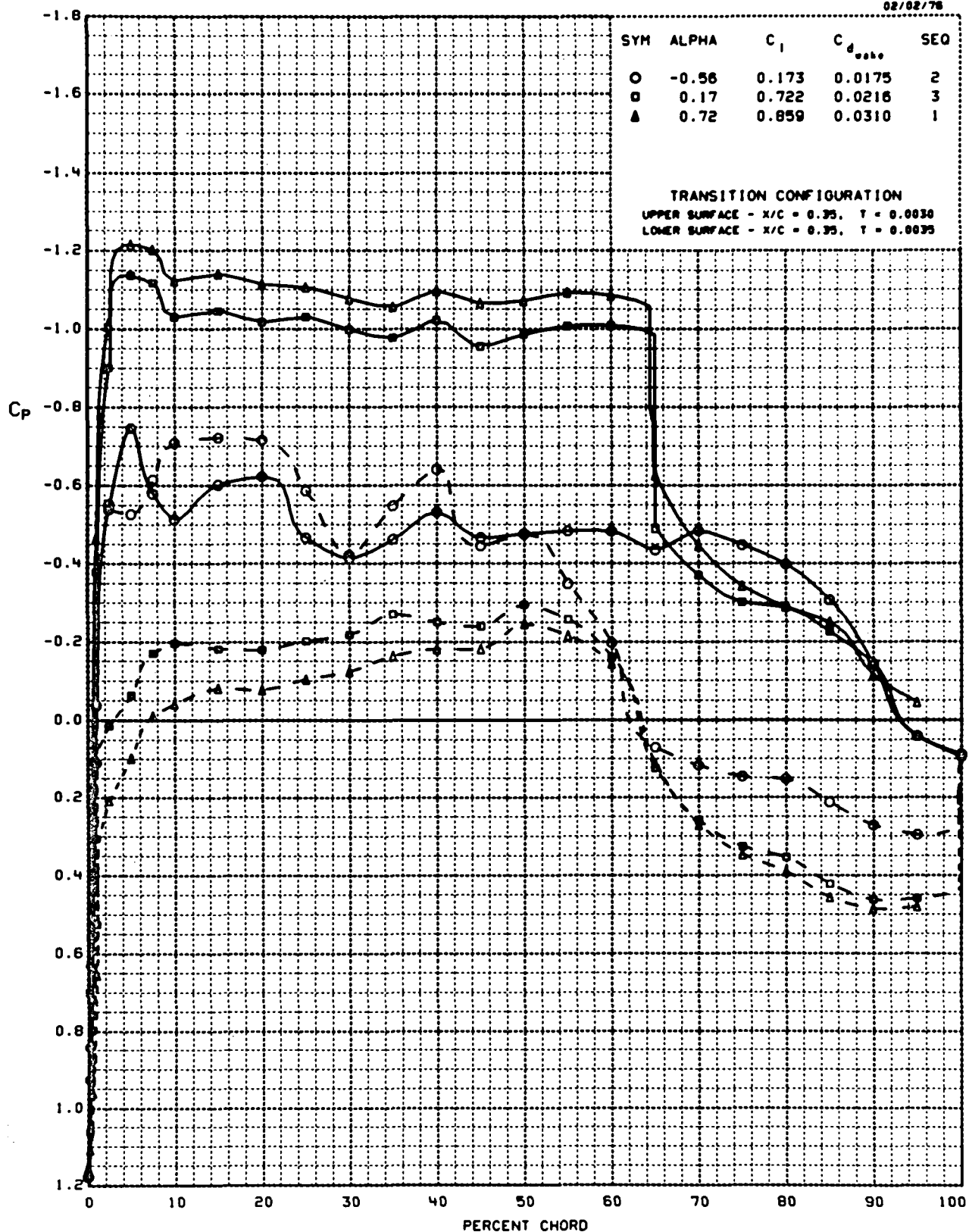
MACH NUMBER = 0.798

REYNOLDS NUMBER =  $2.99 \times 10^6$

RUN = 62

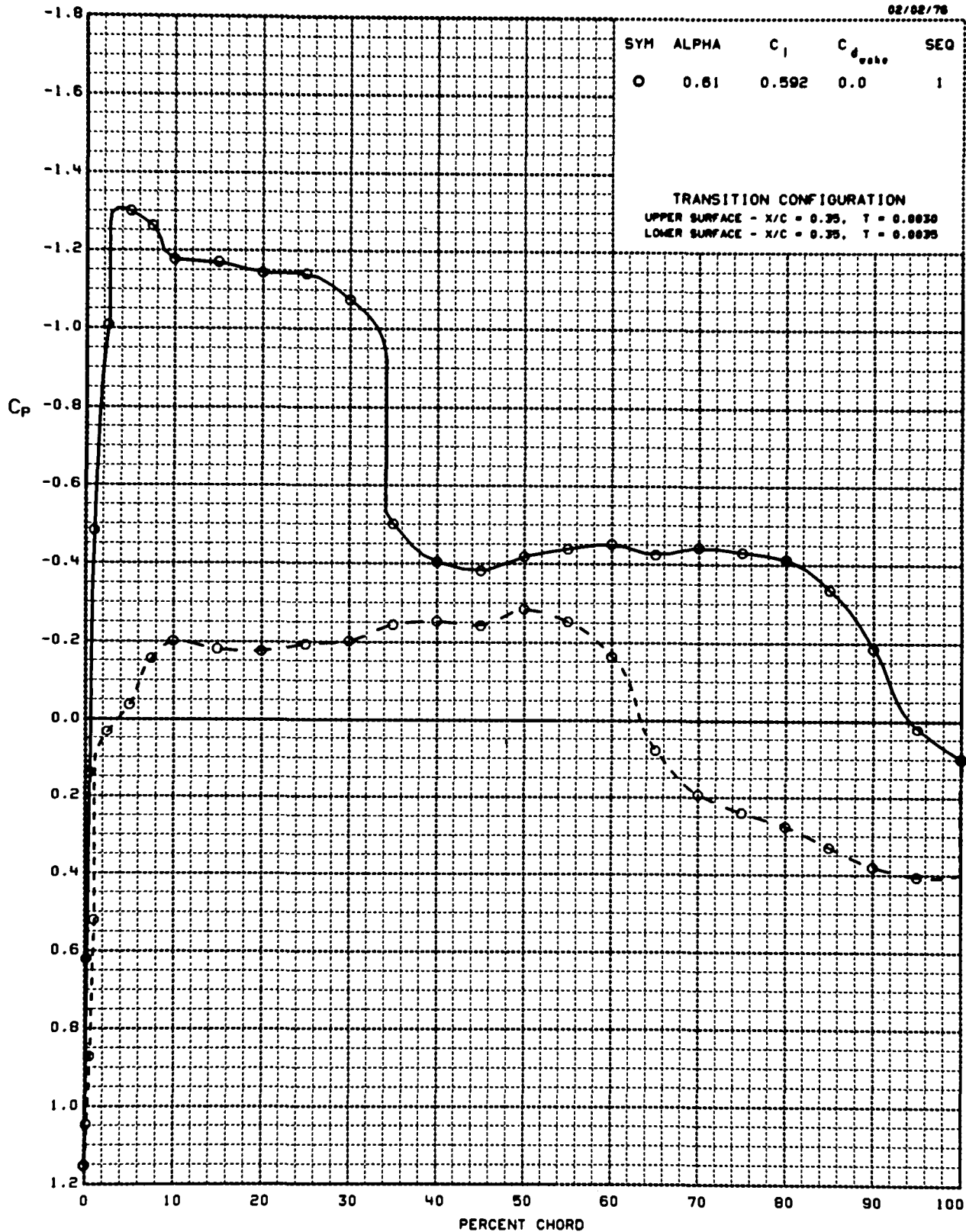
AMES 22-060-5

02/02/78



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS  
 MACH NUMBER = 0.759      REYNOLDS NUMBER =  $4.02 \times 10^6$       RUN = 65      AMES 22-060-5

02/02/76



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

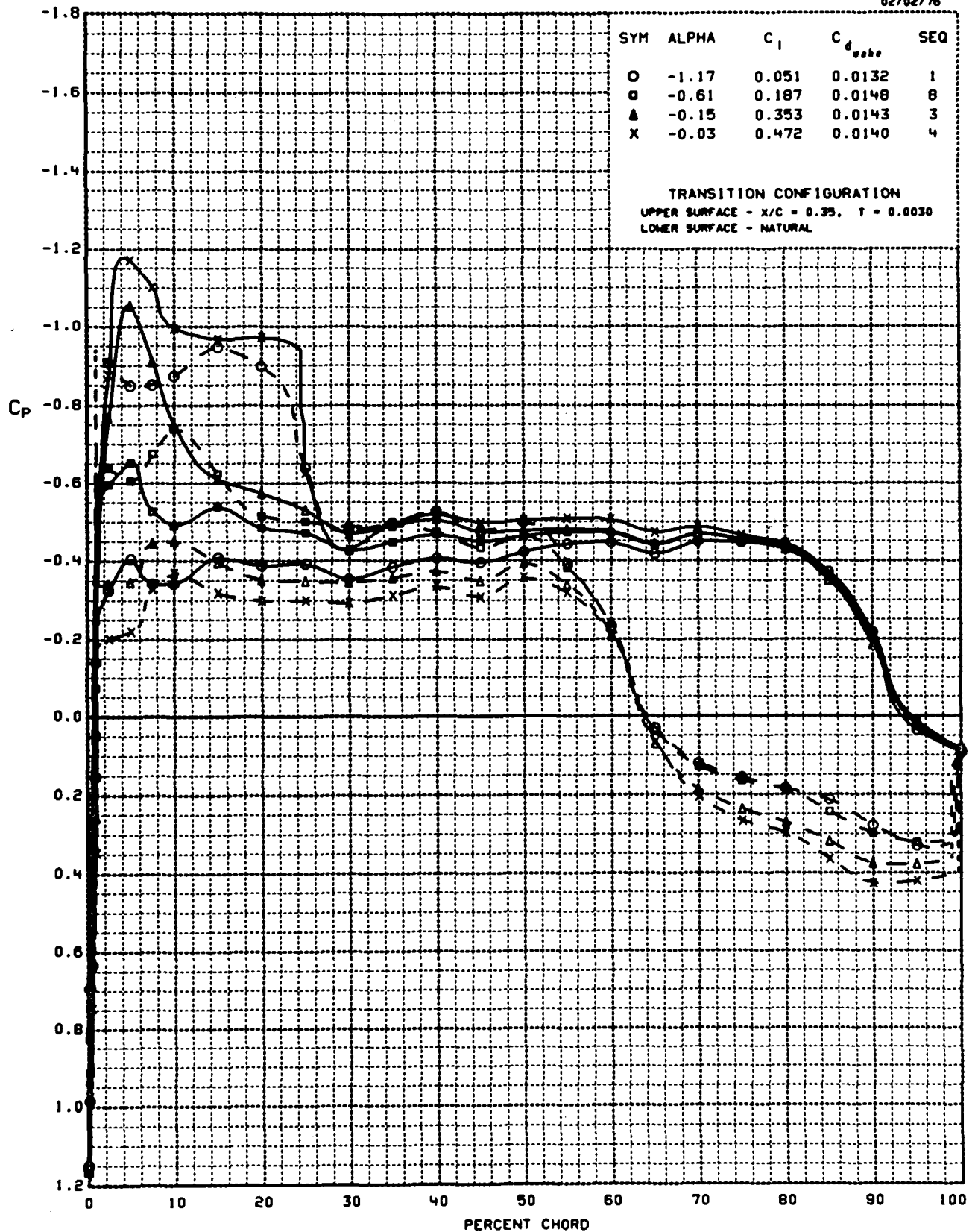
MACH NUMBER = 0.761

REYNOLDS NUMBER =  $3.98 \times 10^6$

RUN = 66

AMES 22-060-5

02/02/76



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

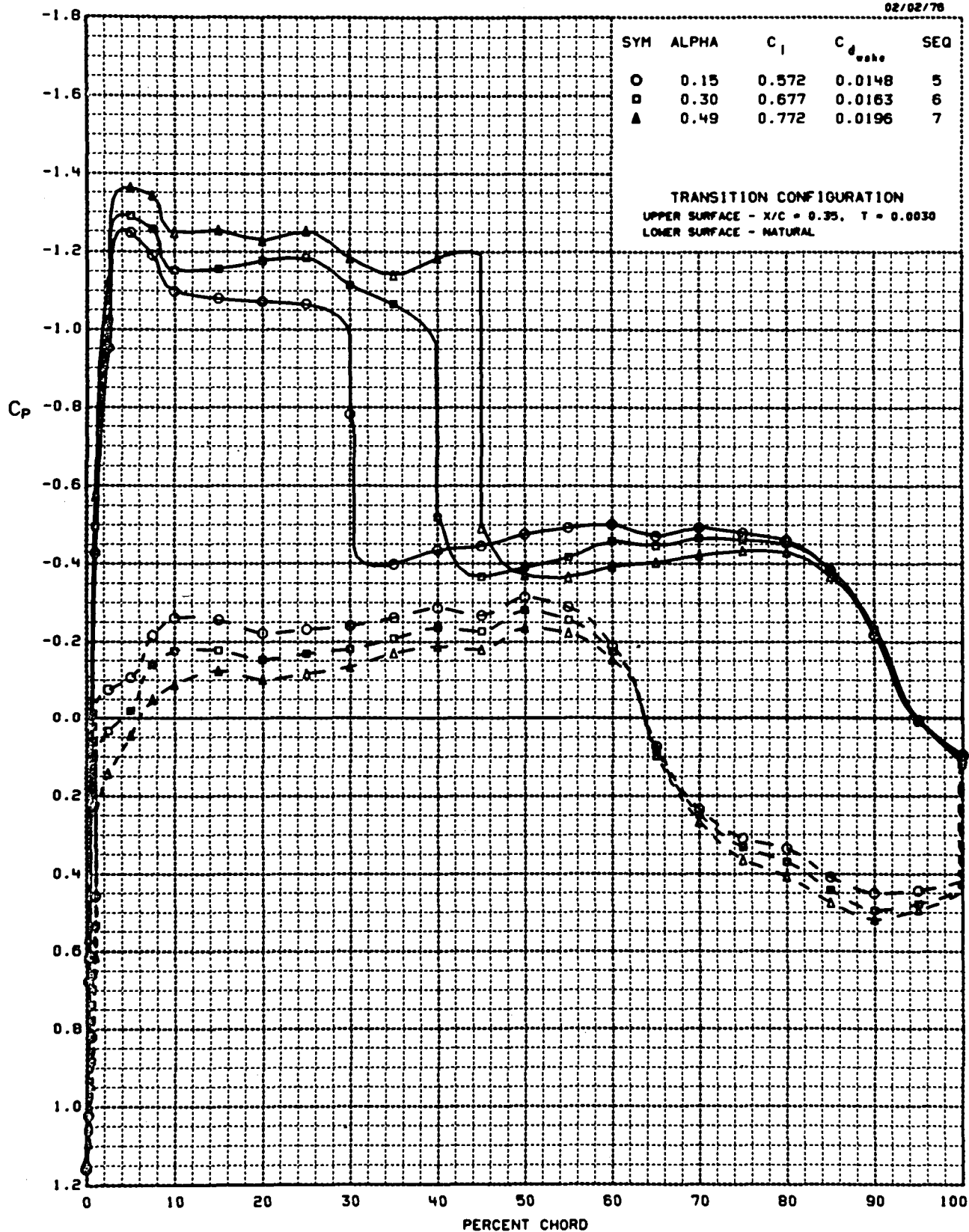
MACH NUMBER = 0.759

REYNOLDS NUMBER =  $3.96 \times 10^6$

RUN = 66

AMES 22-060-5

02/02/78



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

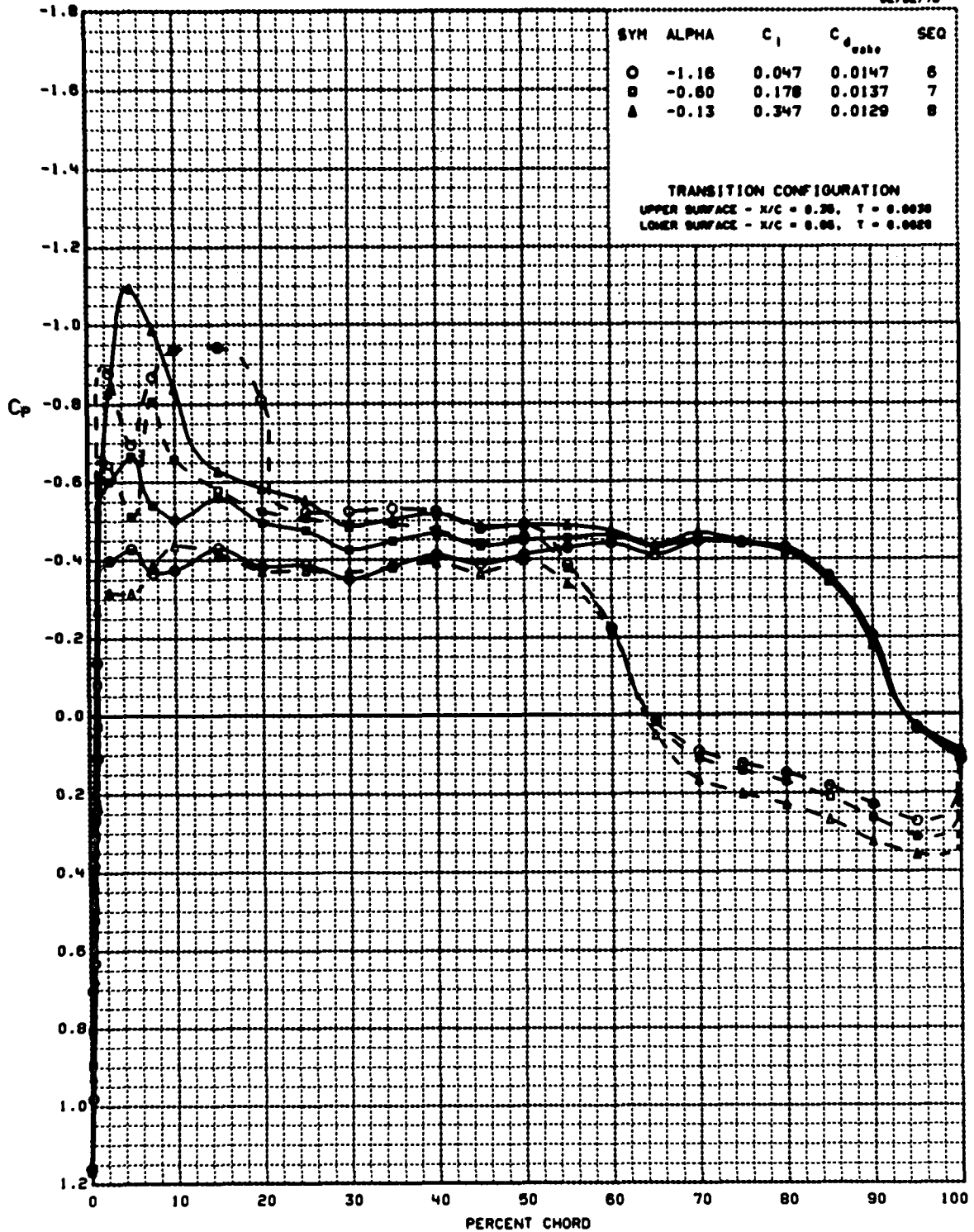
MACH NUMBER = 0.759

REYNOLDS NUMBER =  $3.98 \times 10^6$

RUN = 67

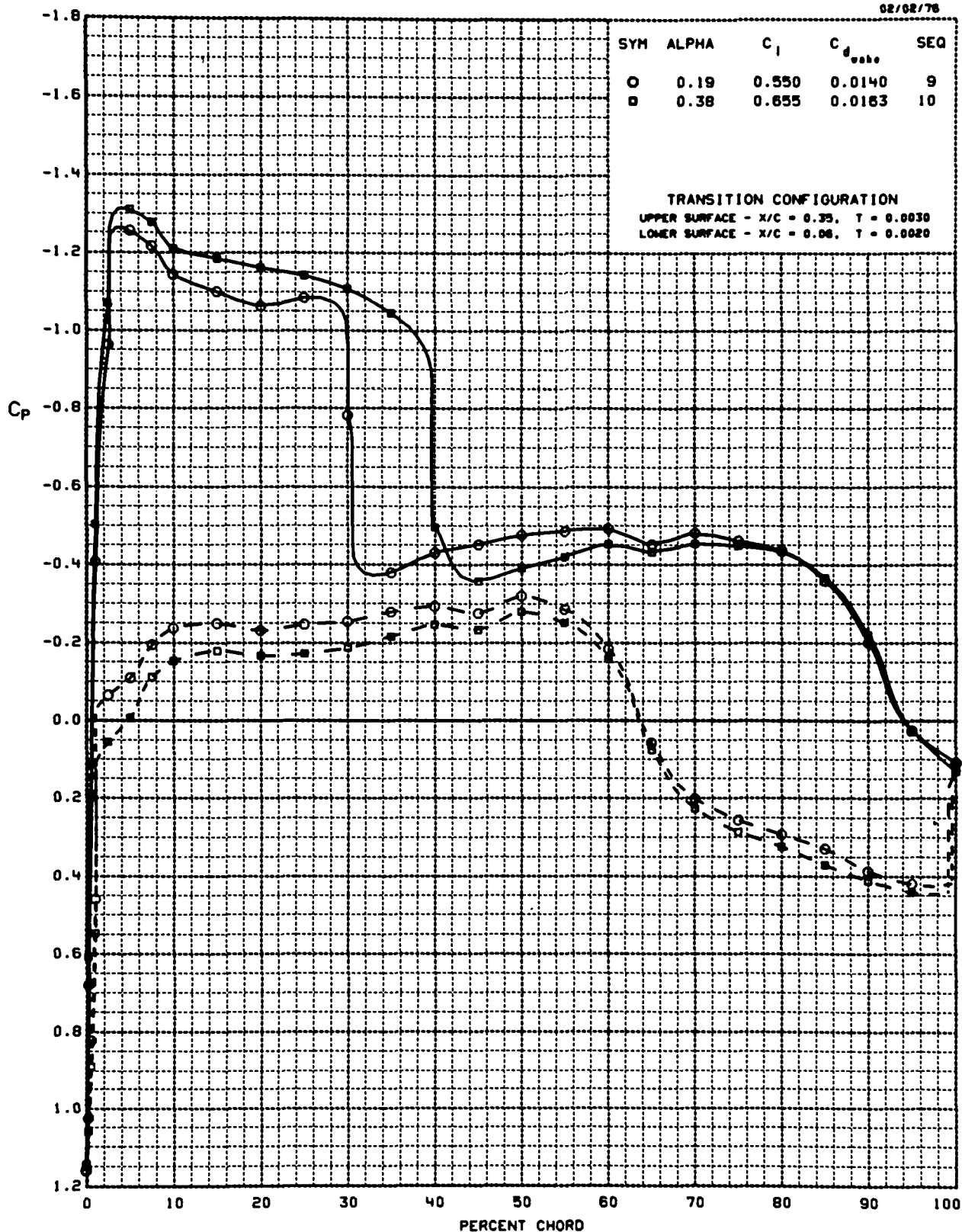
AMES 22-060-5

02/02/78



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS  
 MACH NUMBER = 0.758 REYNOLDS NUMBER =  $3.94 \times 10^6$  RUN = 67 AMES 22-060-5

02/02/76



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

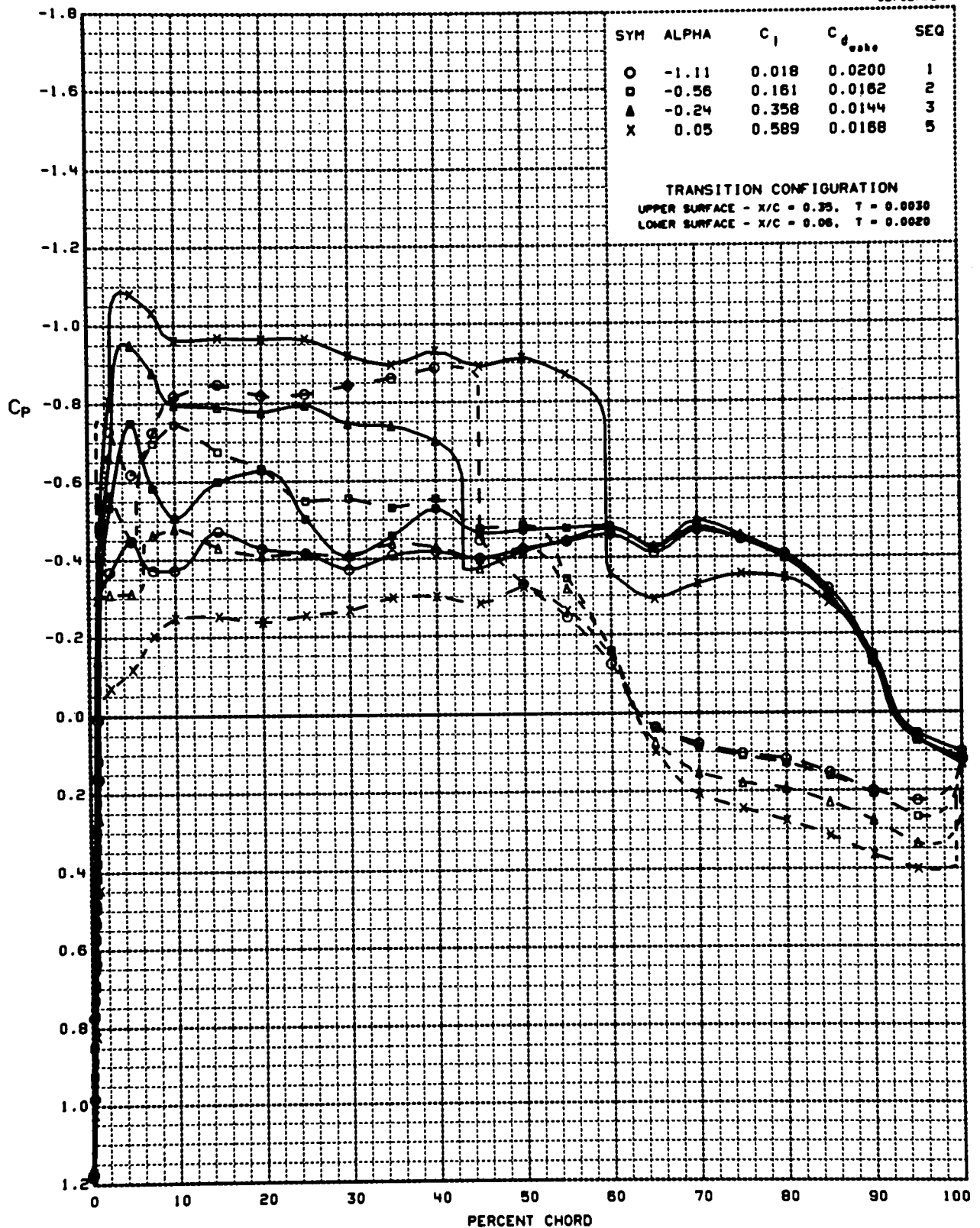
MACH NUMBER = 0.800

REYNOLDS NUMBER =  $2.99 \times 10^6$

RUN = 68

AMES 22-080-5

02/02/78



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

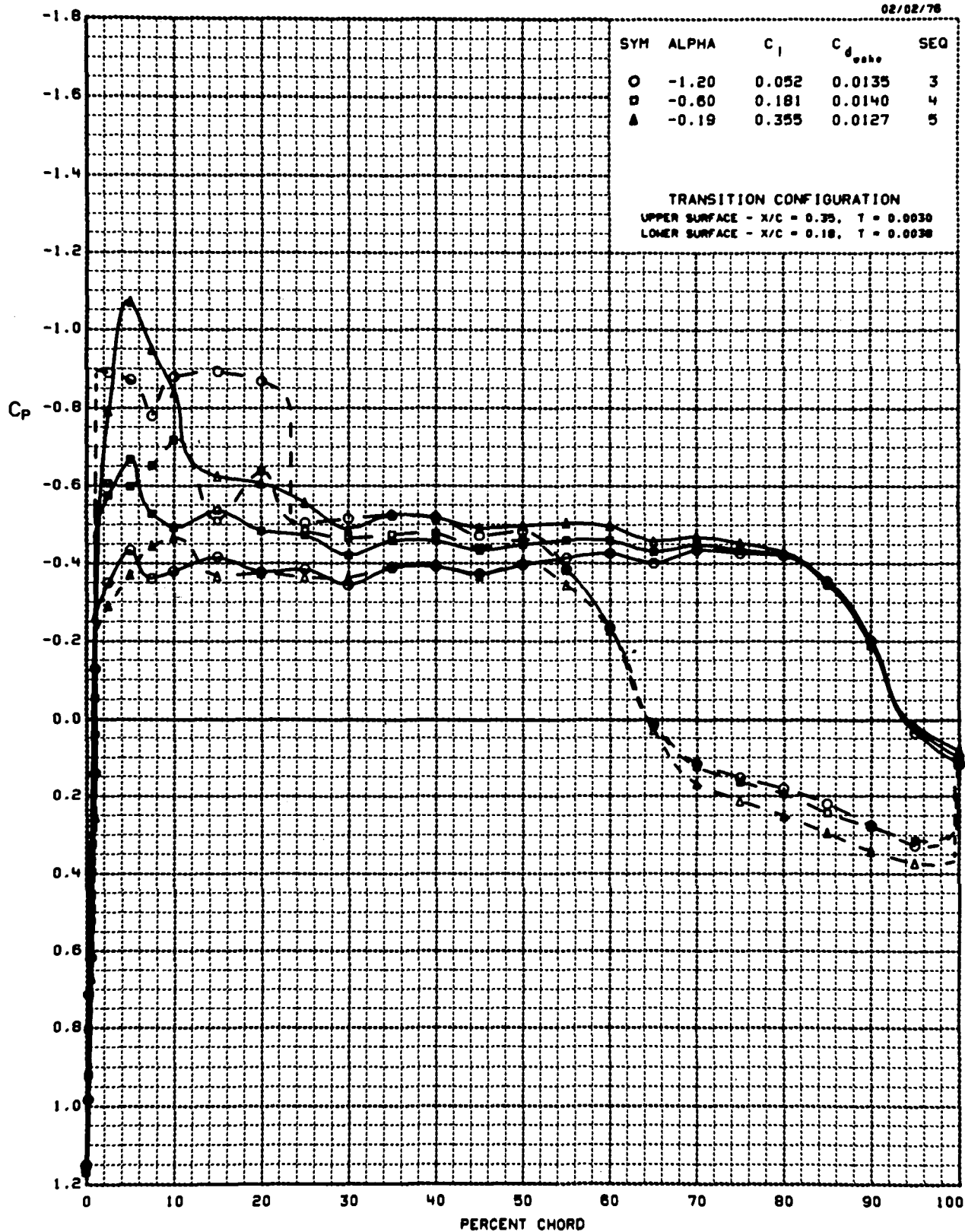
MACH NUMBER = 0.758

REYNOLDS NUMBER =  $3.98 \times 10^6$

RUN = 69

AMES 22-060-5

02/02/76





WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

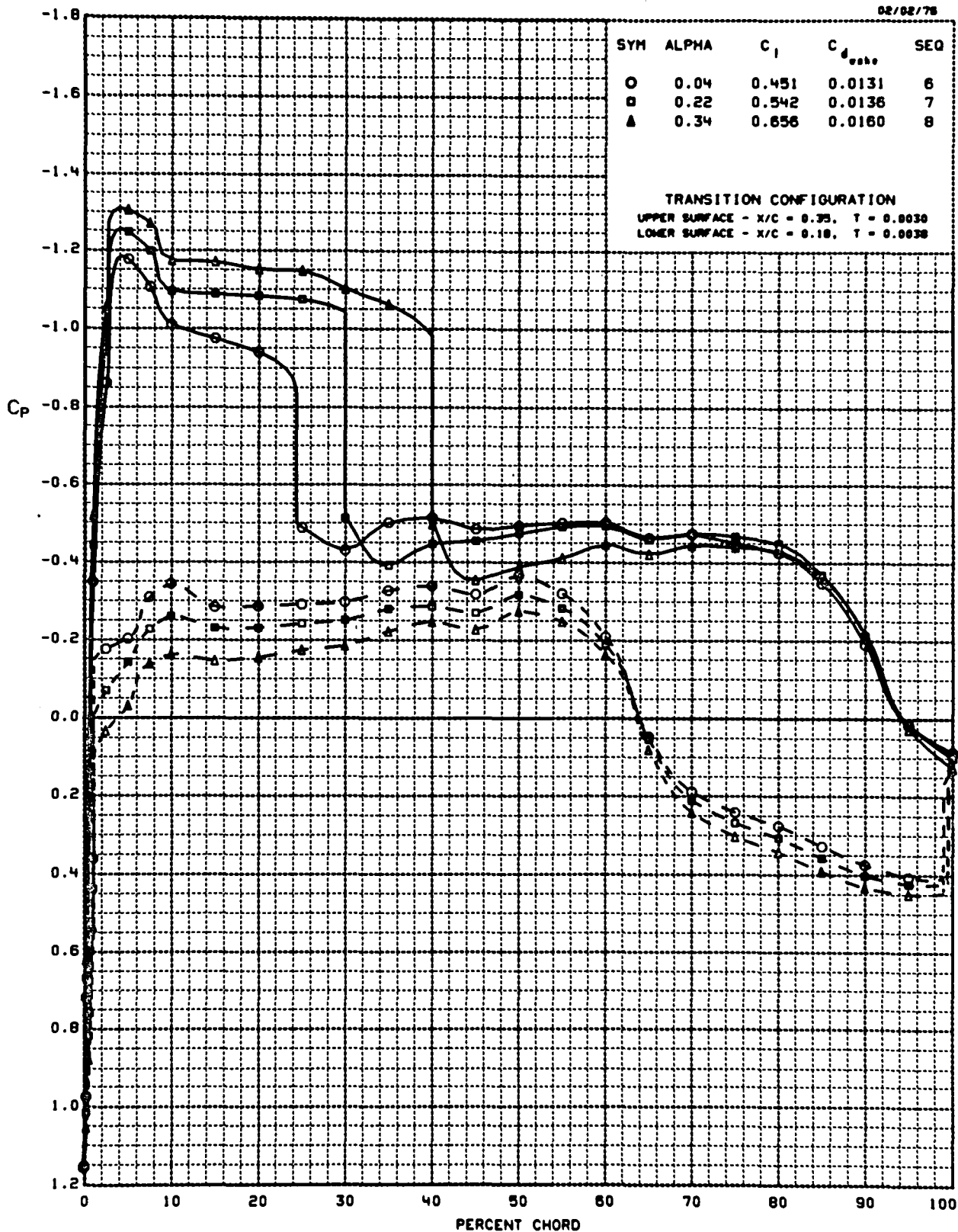
MACH NUMBER = 0.759

REYNOLDS NUMBER =  $3.91 \times 10^6$

RUN = 69

AMES 22-060-5

02/02/76



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

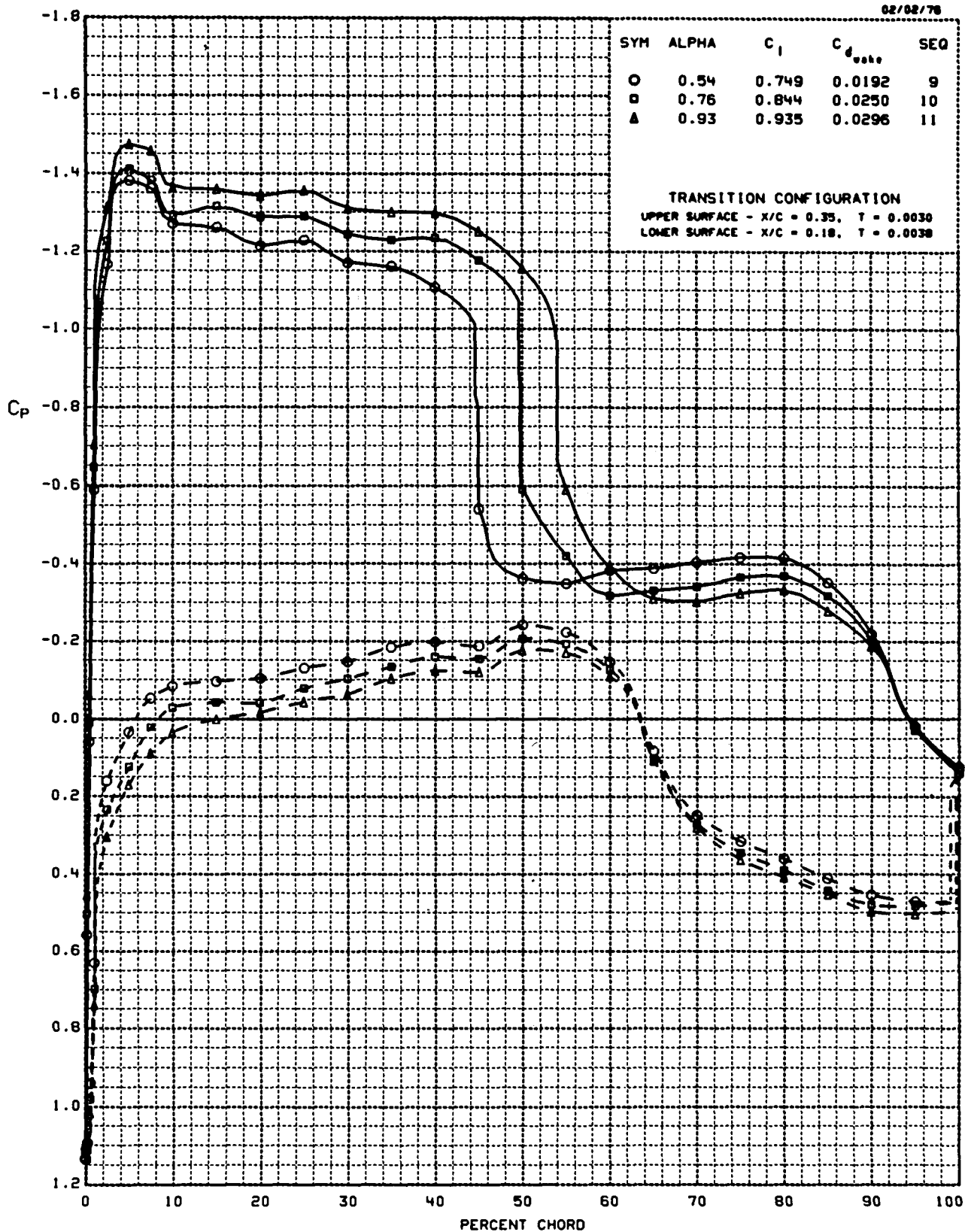
MACH NUMBER = 0.759

REYNOLDS NUMBER =  $3.93 \times 10^8$

RUN = 69

AMES 22-060-5

02/02/78



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

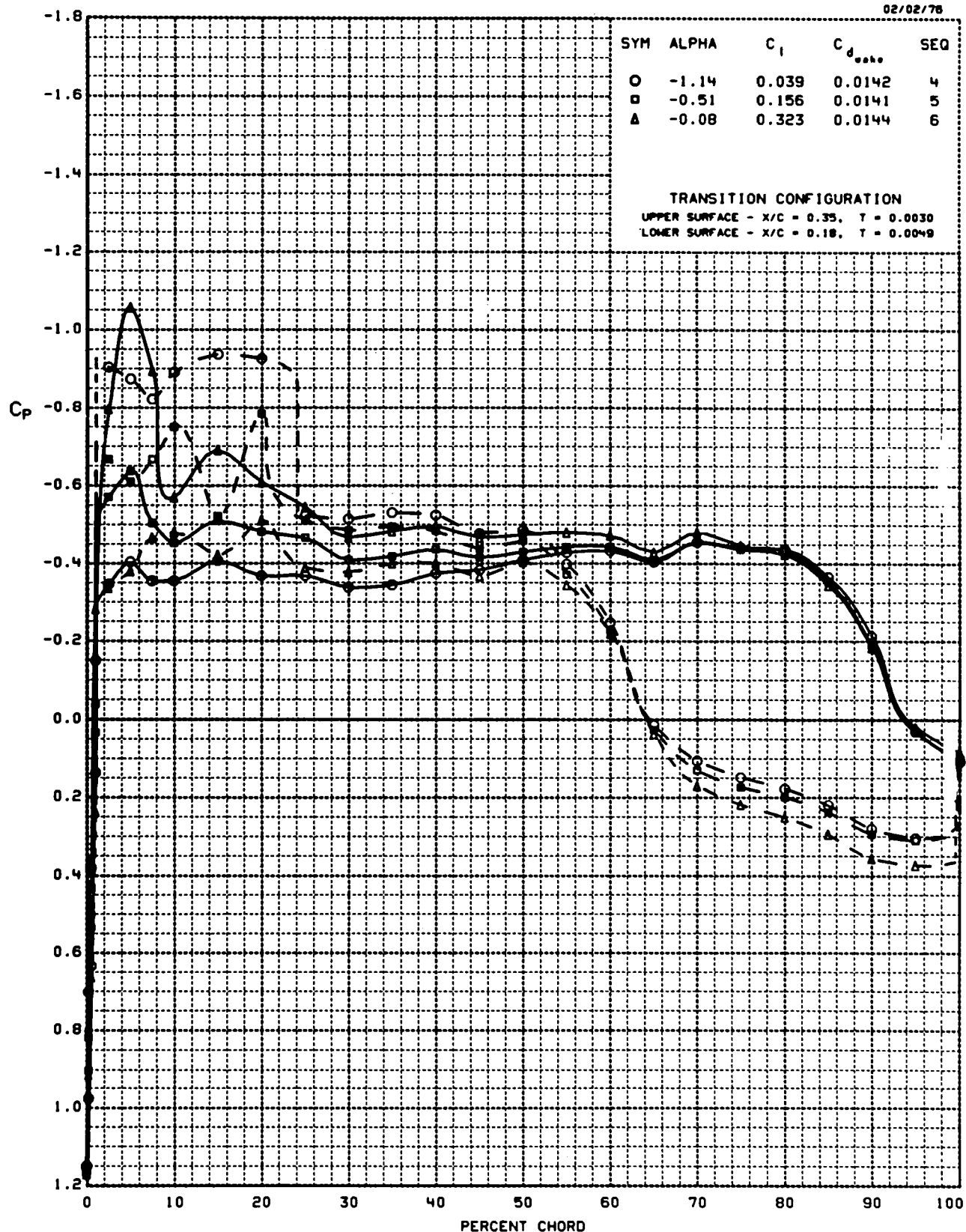
MACH NUMBER = 0.760

REYNOLDS NUMBER =  $4.01 \times 10^6$

RUN = 70

AMES 22-060-5

02/02/76



# WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

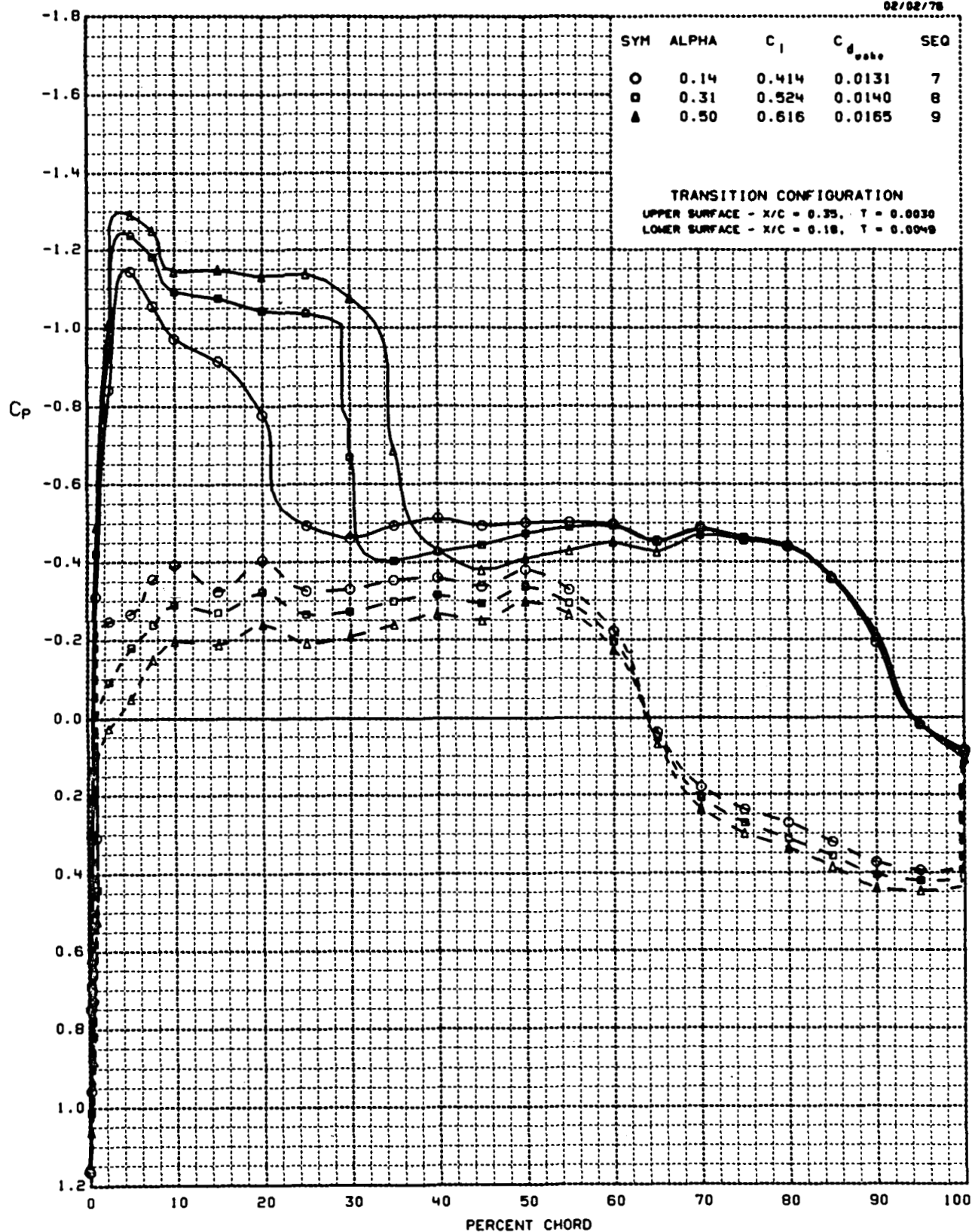
MACH NUMBER = 0.760

REYNOLDS NUMBER =  $3.99 \times 10^6$

RUN = 70

AMES 22-060-5

02/02/78



# WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523

## TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

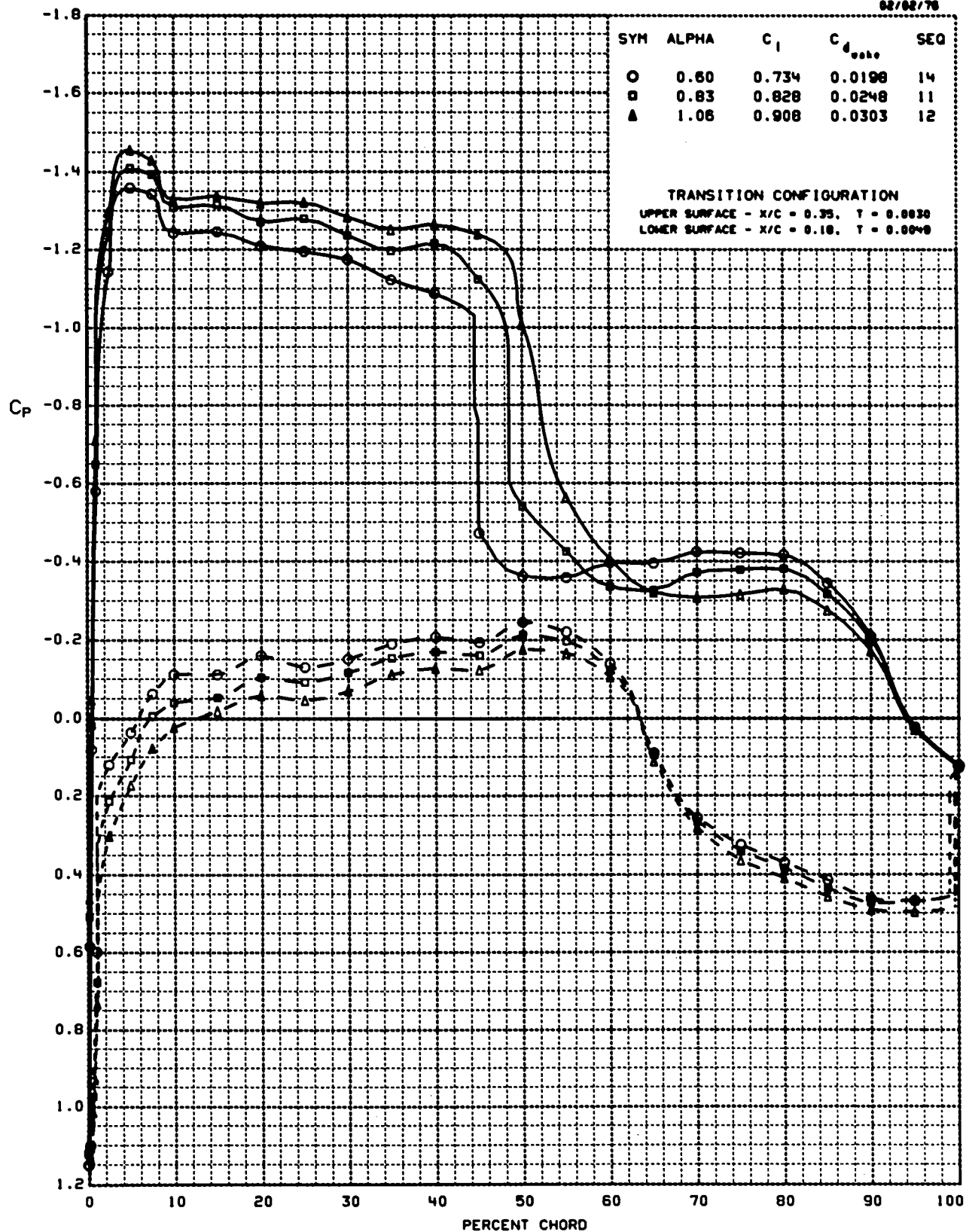
MACH NUMBER = 0.760

REYNOLDS NUMBER =  $3.93 \times 10^6$

RUN = 70

AMES 22-060-5

02/02/78



# WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

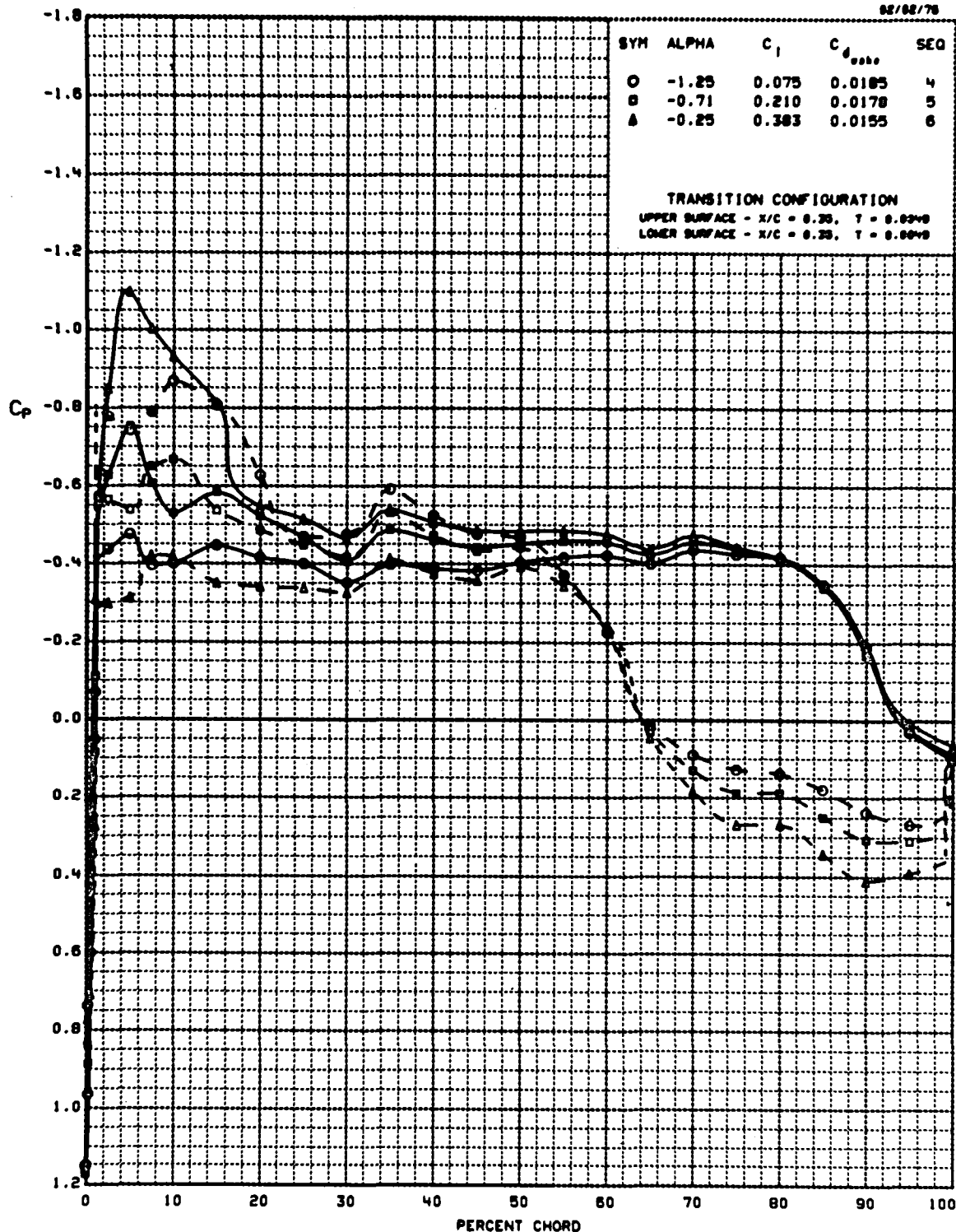
MACH NUMBER = 0.759

REYNOLDS NUMBER =  $2.03 \times 10^6$

RUN = 71

AMES 22-060-5

02/02/78



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

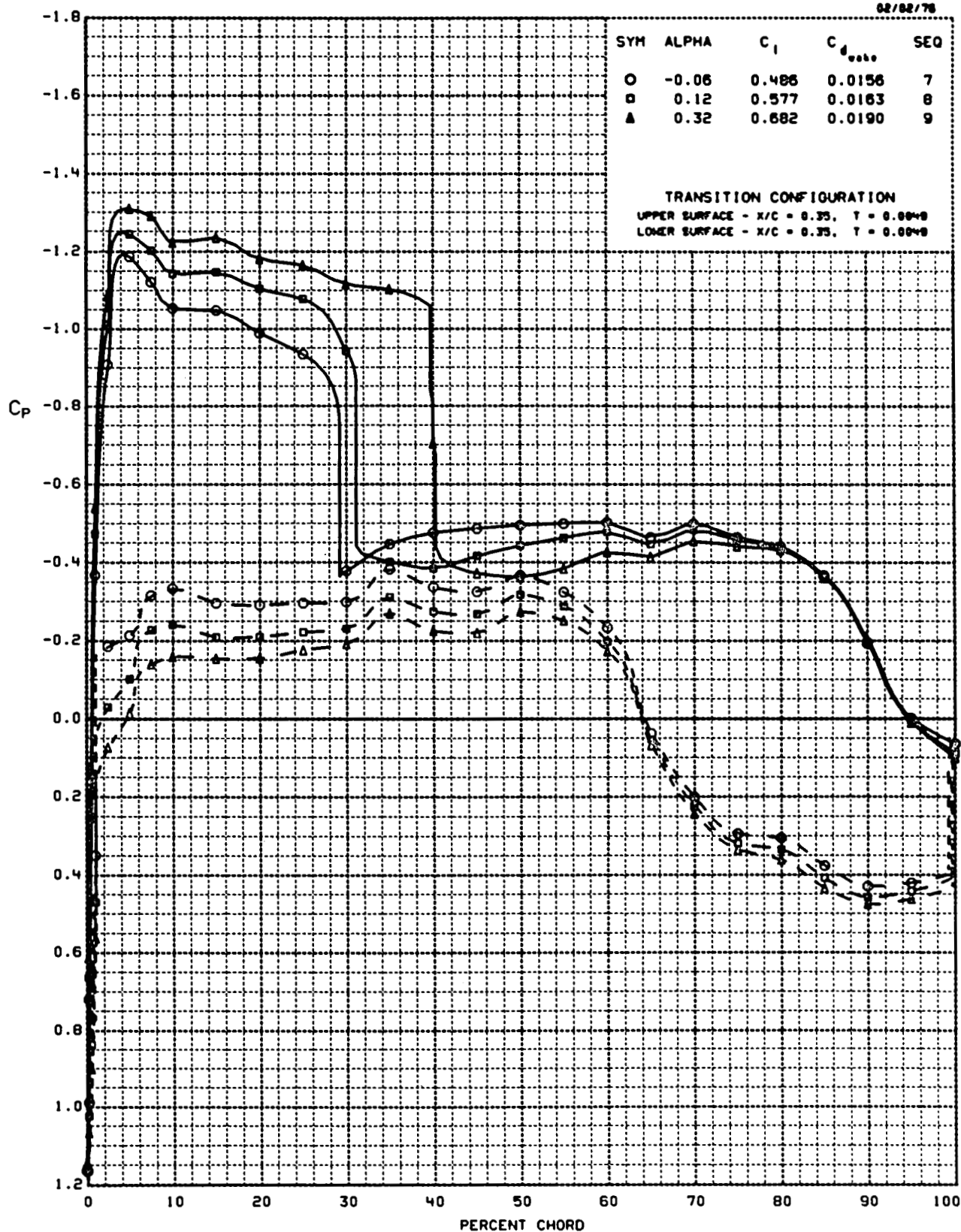
MACH NUMBER = 0.759

REYNOLDS NUMBER =  $1.98 \times 10^6$

RUN = 71

AMES 22-060-5

02/02/78





WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

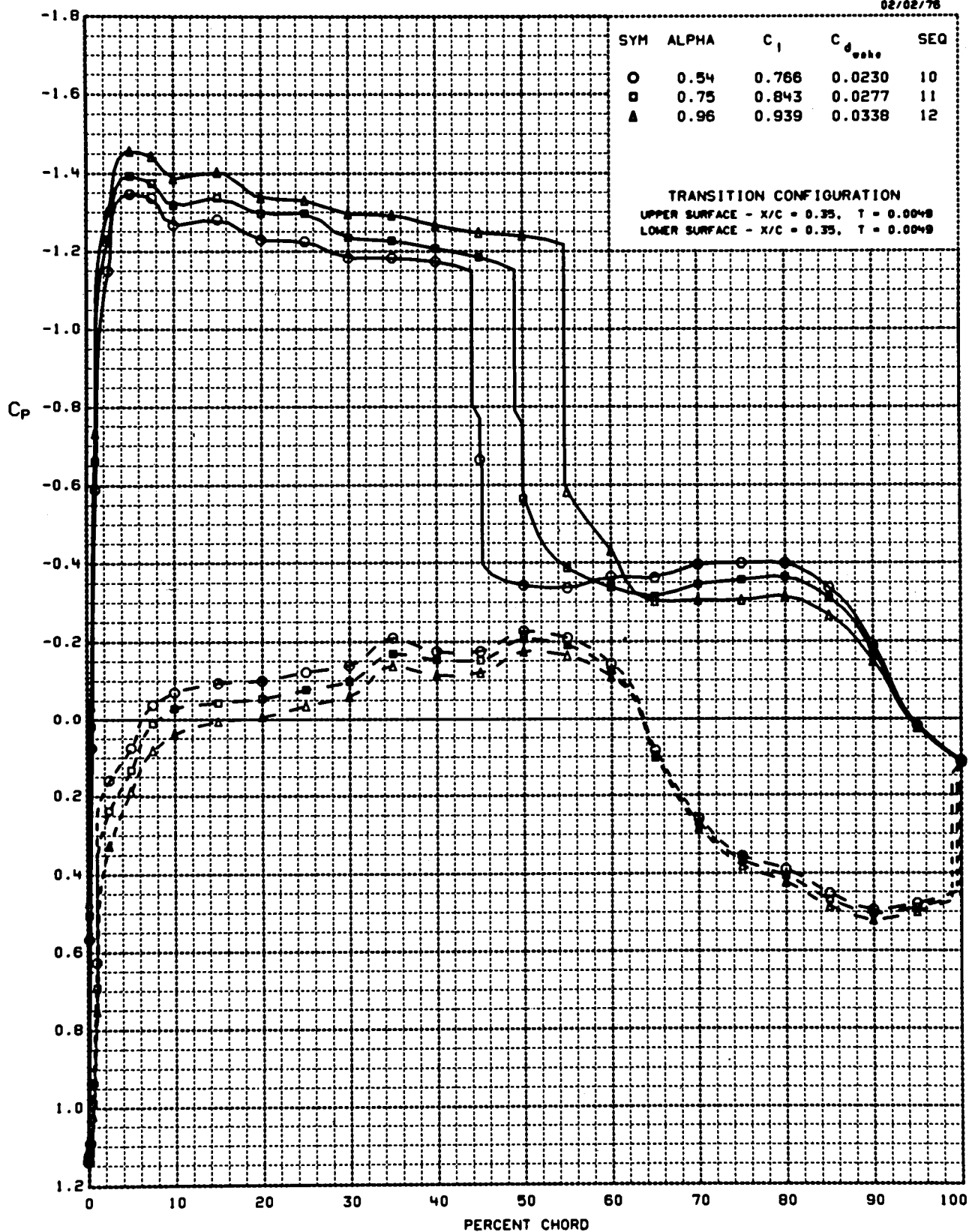
MACH NUMBER = 0.761

REYNOLDS NUMBER =  $1.98 \times 10^6$

RUN = 71

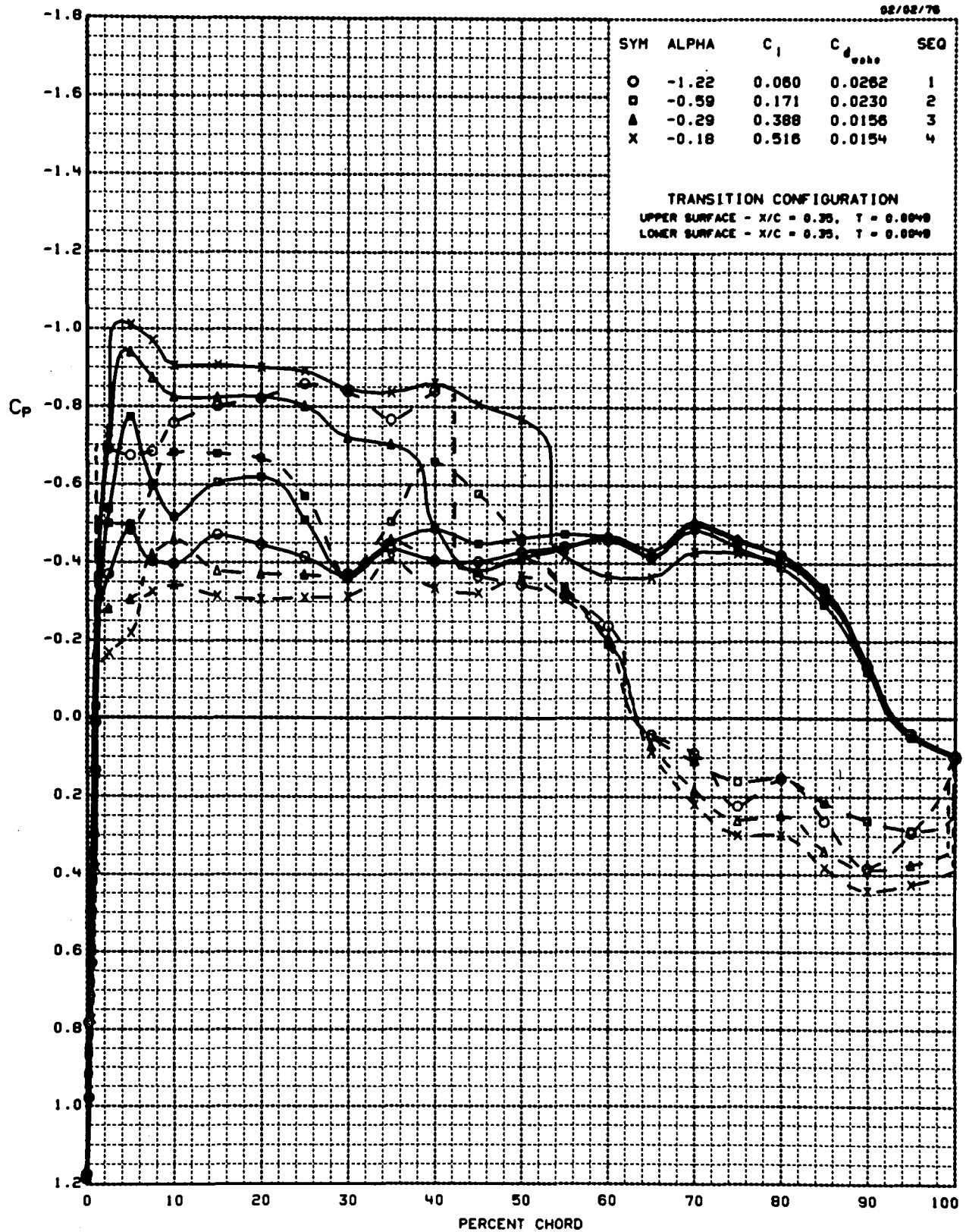
AMES 22-060-5

02/02/76





WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS  
 MACH NUMBER = 0.800 REYNOLDS NUMBER =  $1.99 \times 10^6$  RUN = 72 AMES 22-060-5



# WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

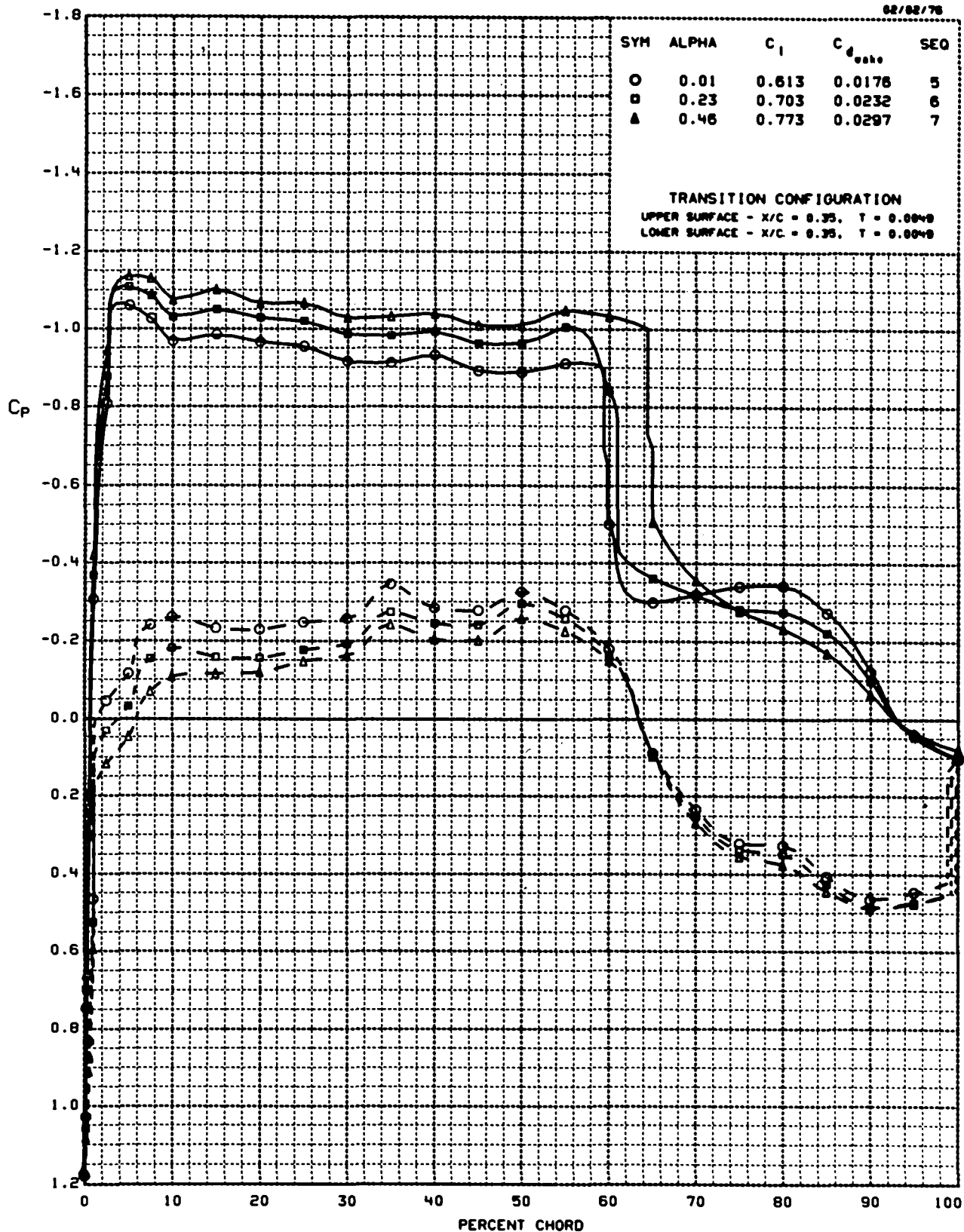
MACH NUMBER = 0.801

REYNOLDS NUMBER =  $1.98 \times 10^8$

RUN = 72

AMES 22-060-5

02/02/76



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

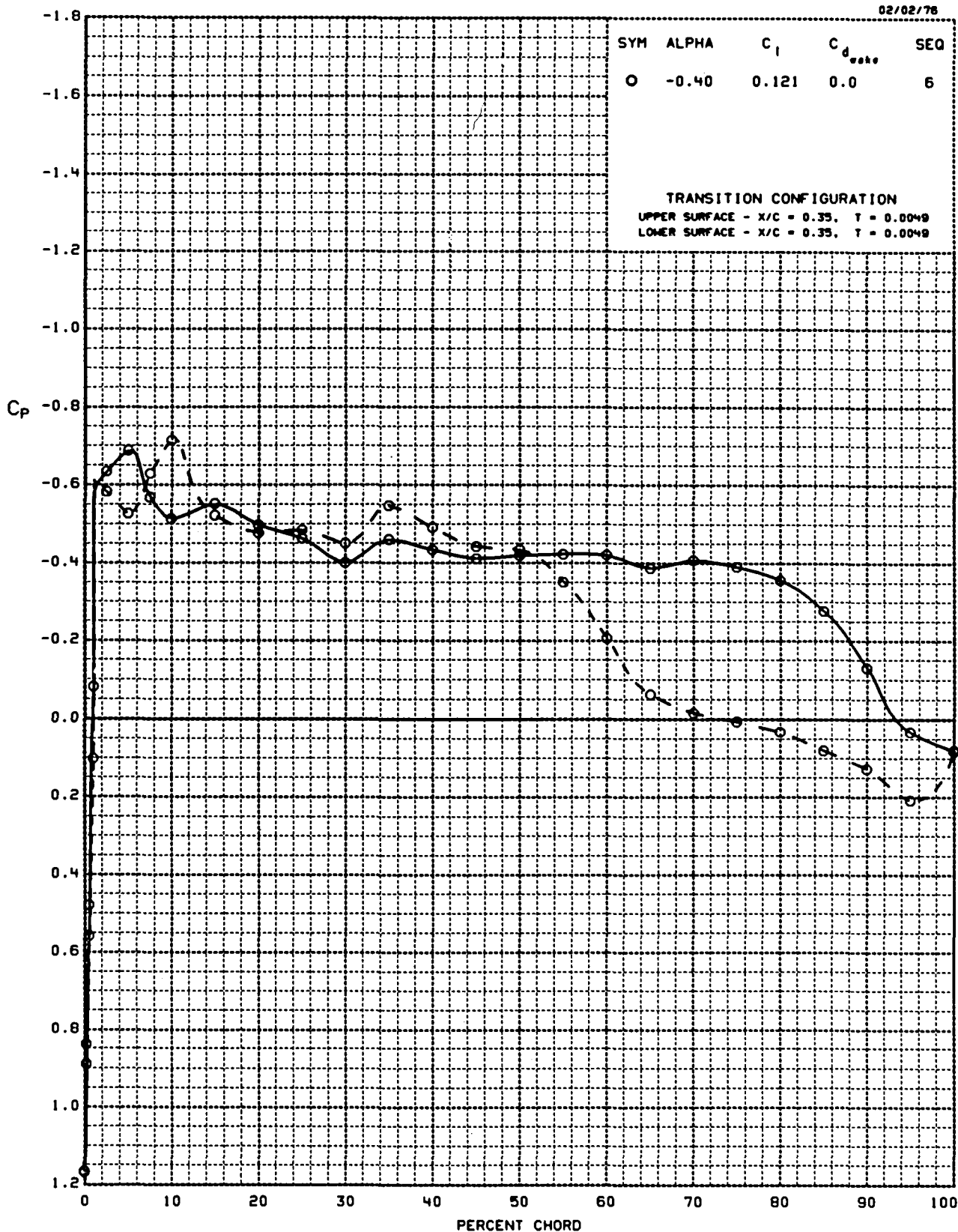
MACH NUMBER = 0.764

REYNOLDS NUMBER =  $2.05 \times 10^6$

RUN = 73

AMES 22-060-5

02/02/78



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

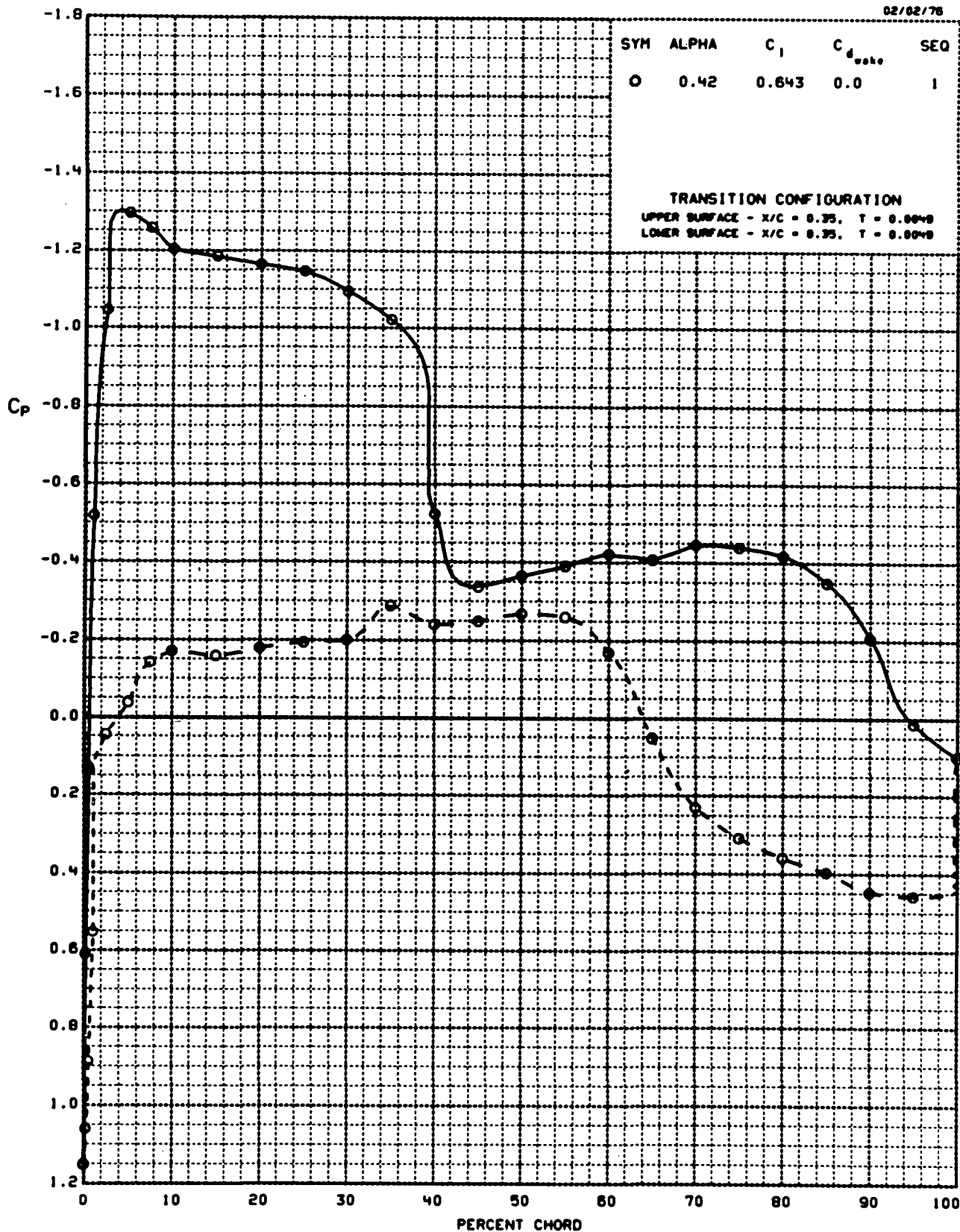
MACH NUMBER = 0.761

REYNOLDS NUMBER =  $1.97 \times 10^6$

RUN = 74

AMES 22-060-5

02/02/76



# WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

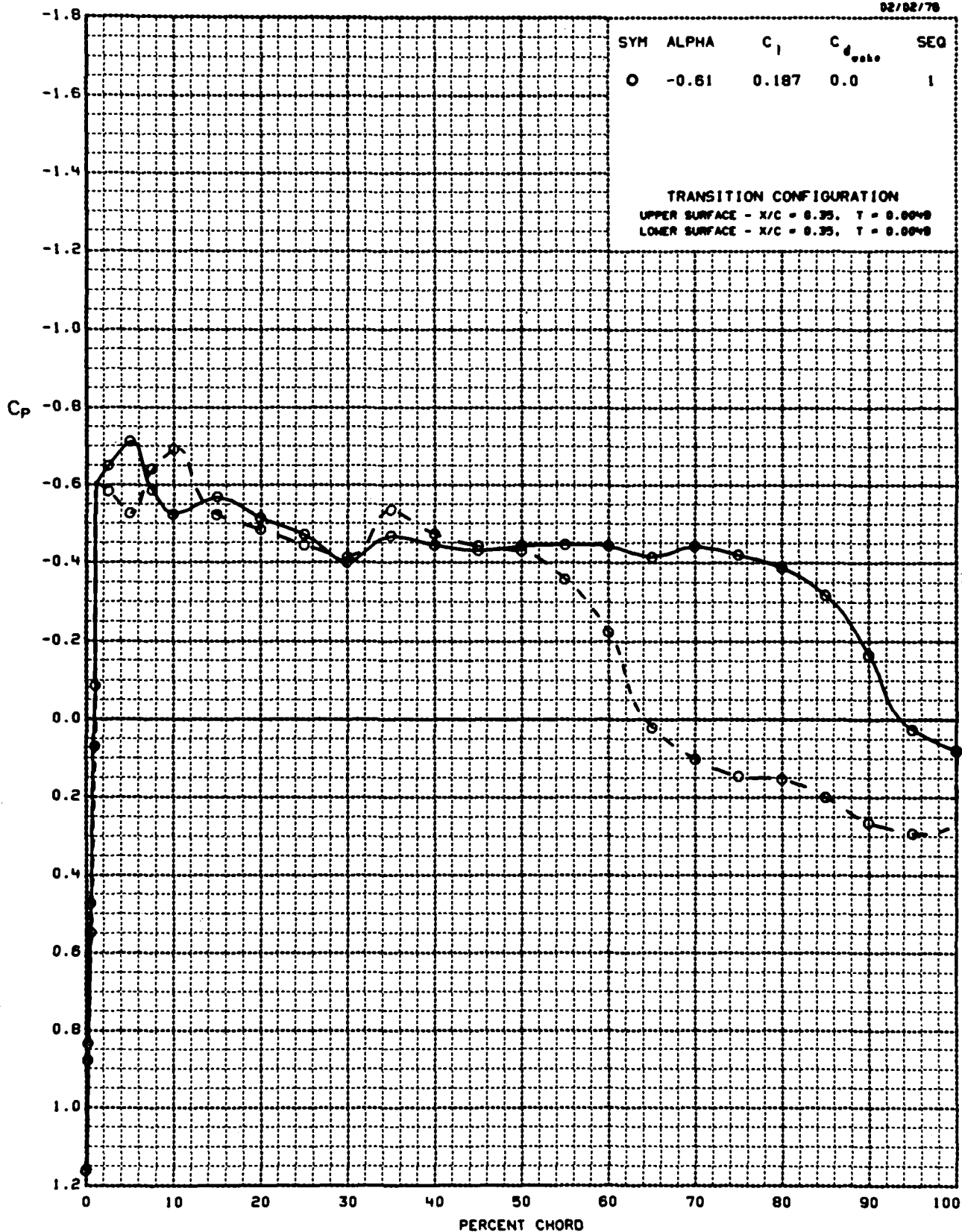
MACH NUMBER = 0.758

REYNOLDS NUMBER =  $1.99 \times 10^6$

RUN = 75

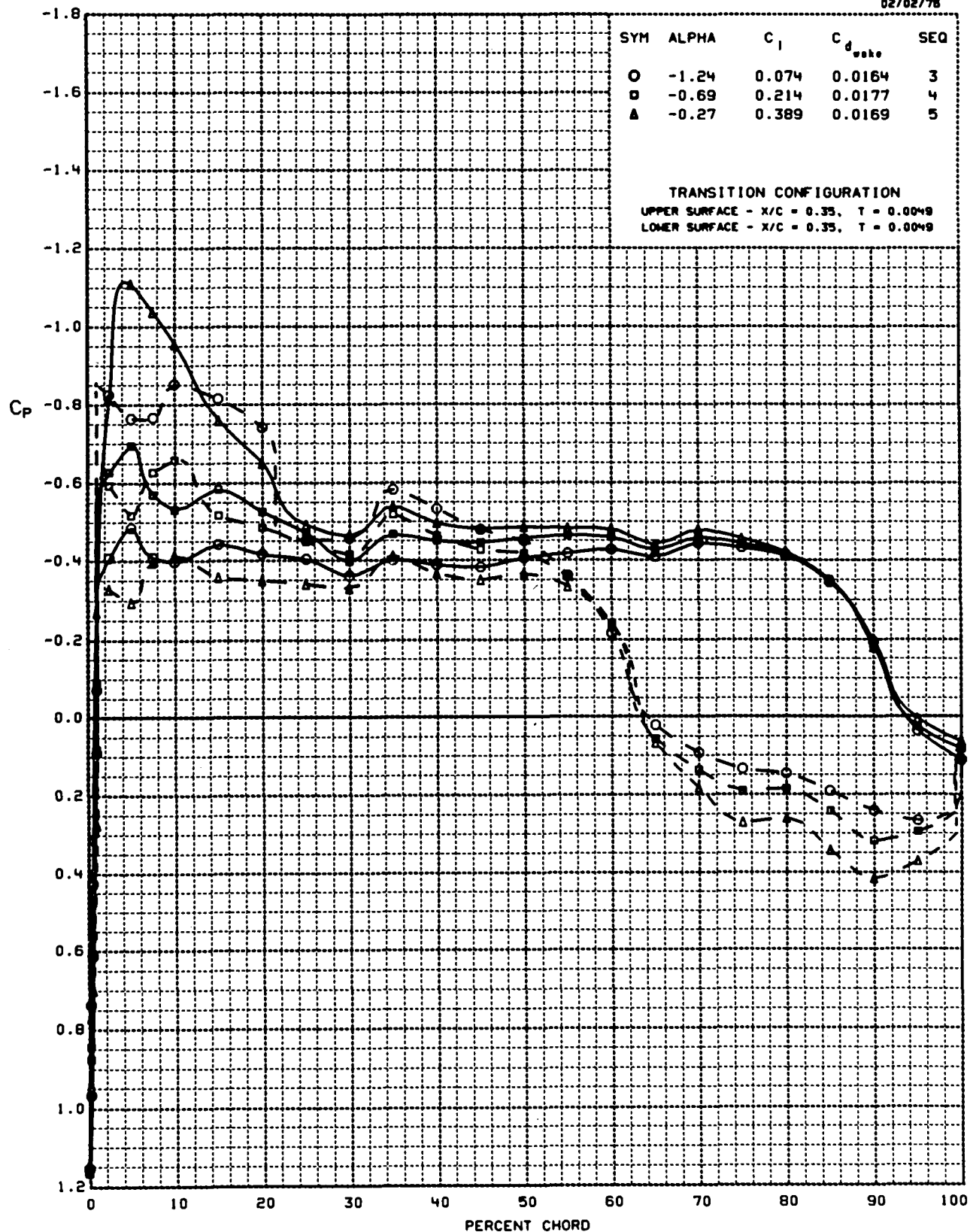
AMES 22-060-5

02/02/78



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS  
MACH NUMBER = 0.761 REYNOLDS NUMBER =  $2.01 \times 10^6$  RUN = 76 AMES 22-060-5

02/02/78



# WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

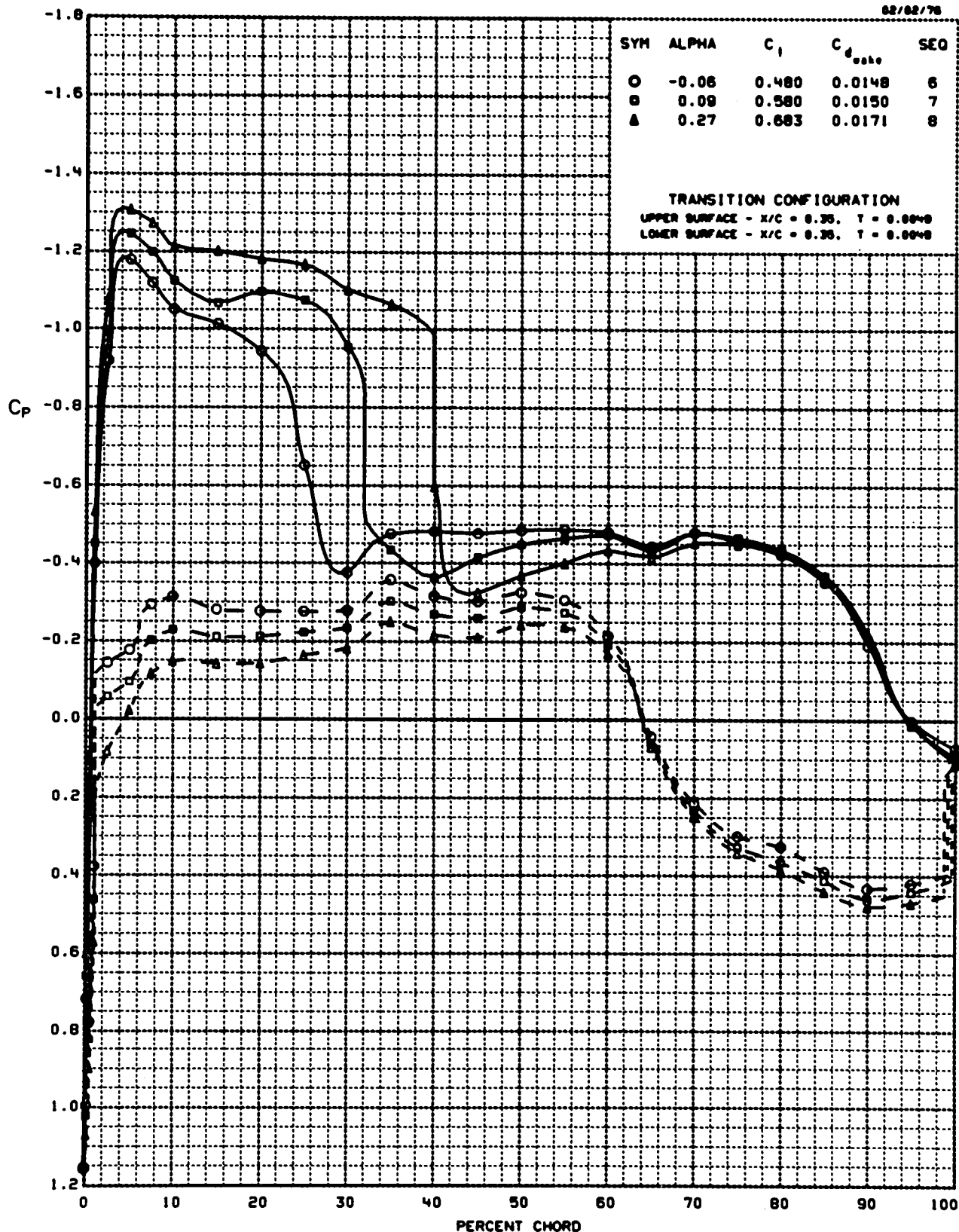
MACH NUMBER = 0.759

REYNOLDS NUMBER =  $1.99 \times 10^6$

RUN = 76

AMES 22-060-5

02/02/76



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

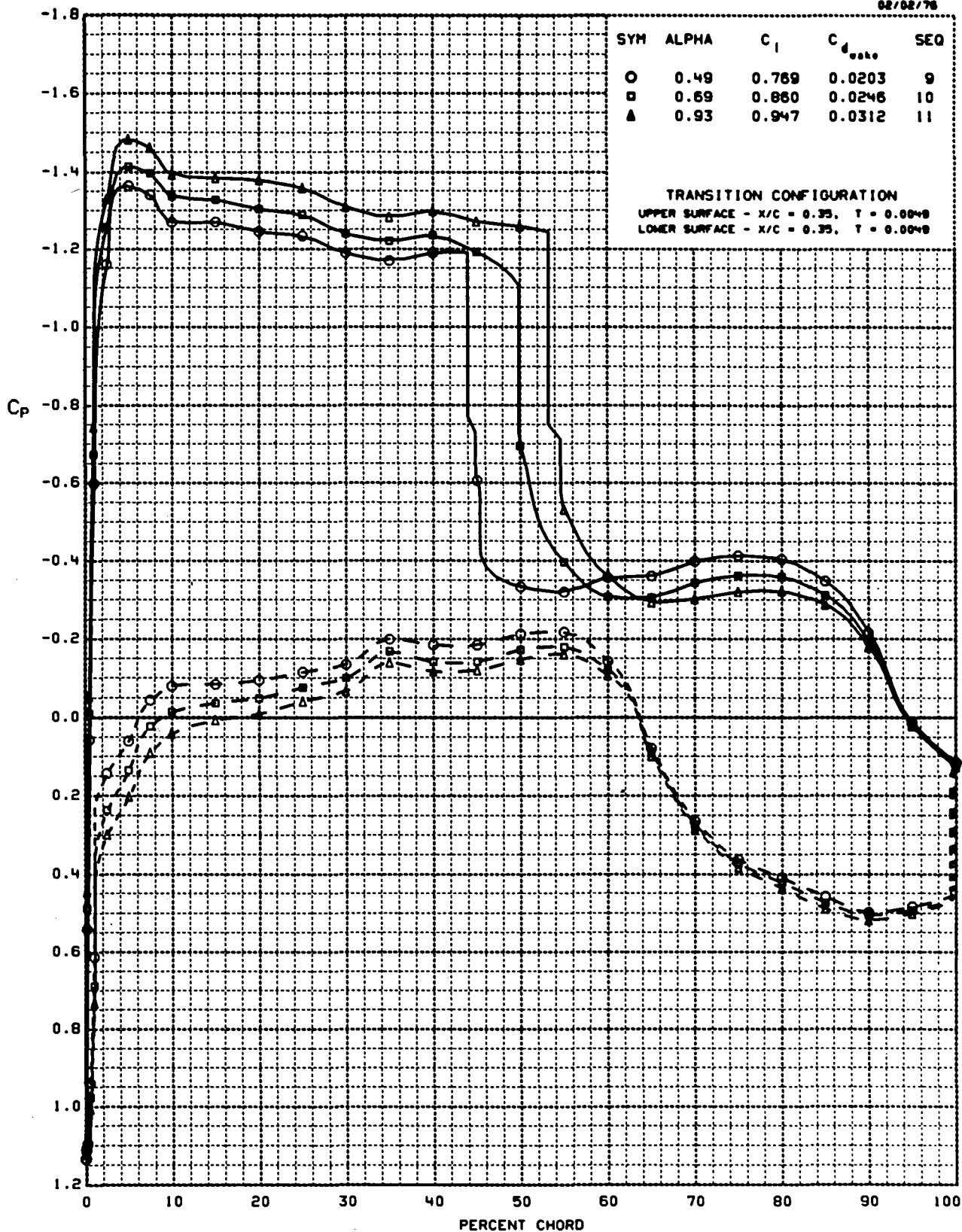
MACH NUMBER = 0.759

REYNOLDS NUMBER =  $1.98 \times 10^6$

RUN = 76

AMES 22-060-5

02/02/76





# WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

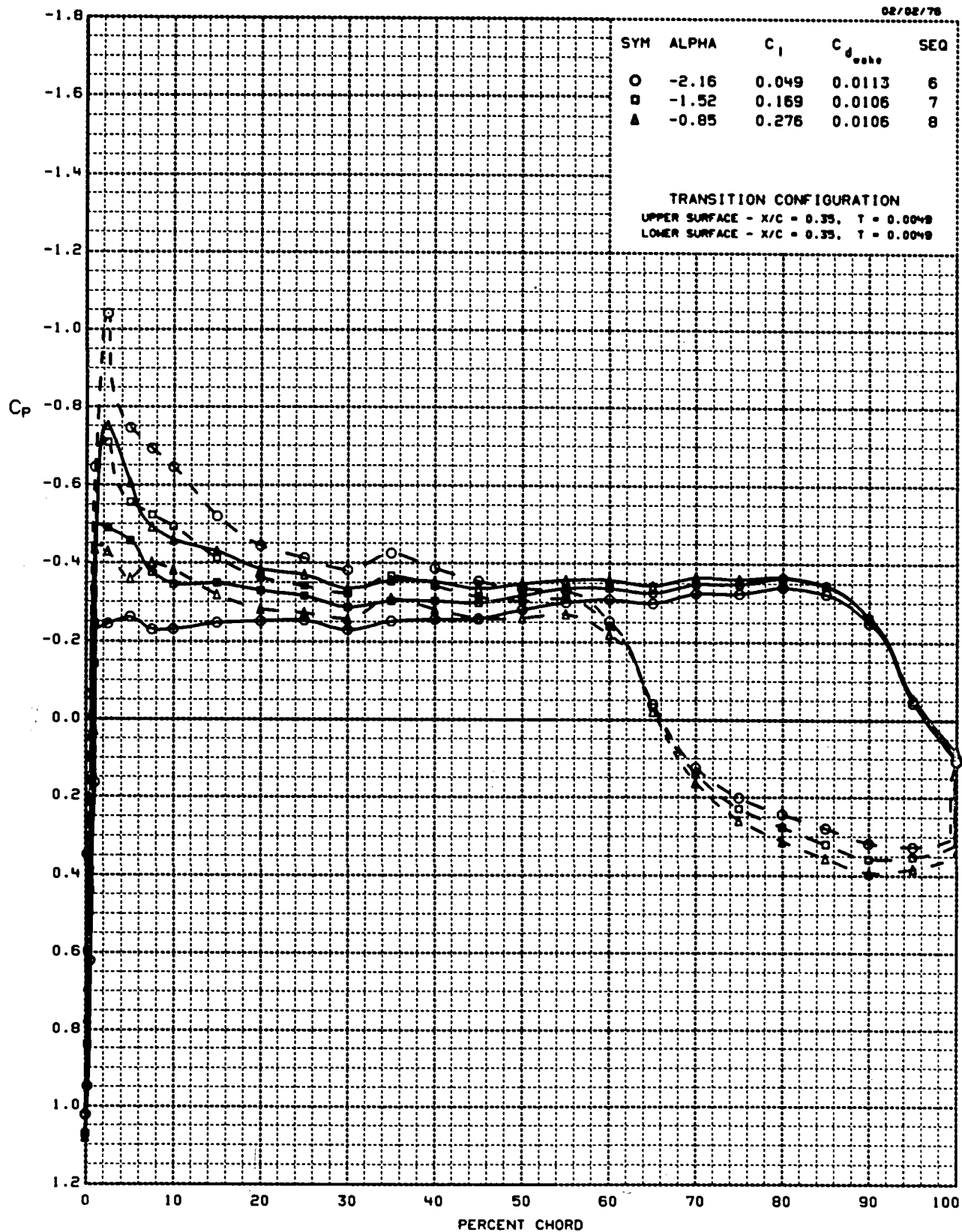
MACH NUMBER = 0.498

REYNOLDS NUMBER =  $2.00 \times 10^6$

RUN = 77

AMES 22-060-5

02/02/78



# WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

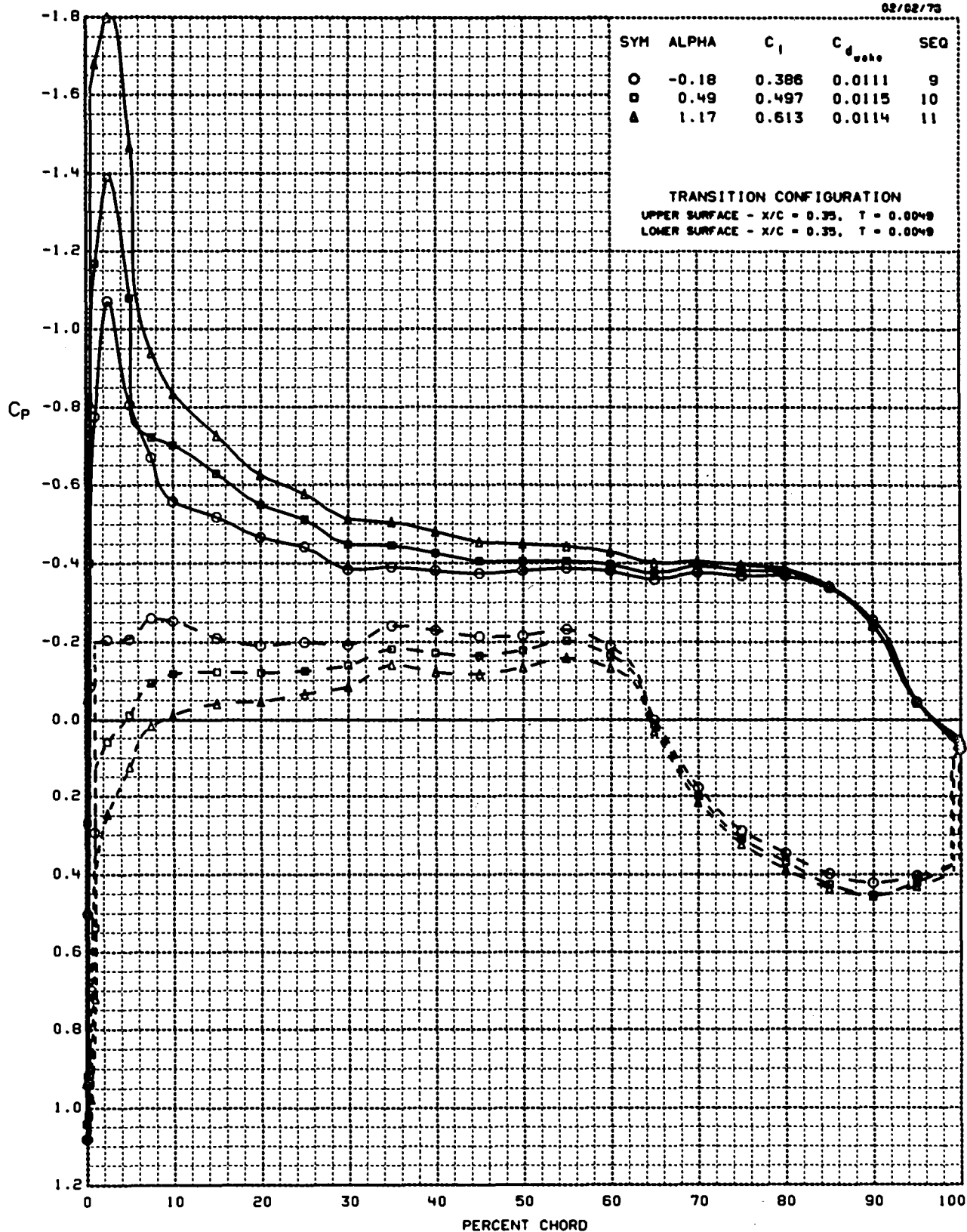
MACH NUMBER = 0.501

REYNOLDS NUMBER =  $2.01 \times 10^6$

RUN = 77

AMES 22-060-5

02/02/73



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

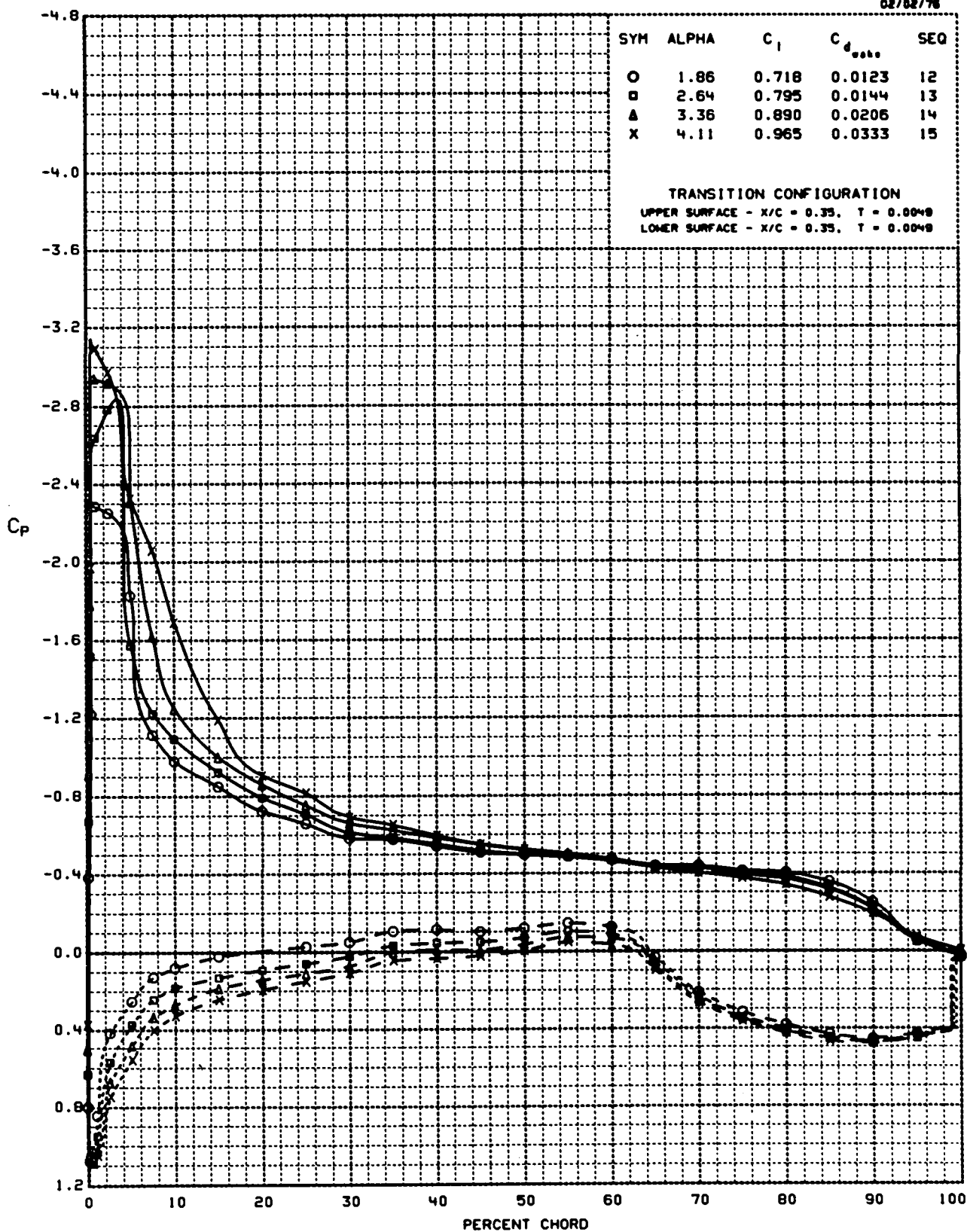
MACH NUMBER = 0.498

REYNOLDS NUMBER =  $1.99 \times 10^6$

RUN = 77

AMES 22-060-5

02/02/78



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

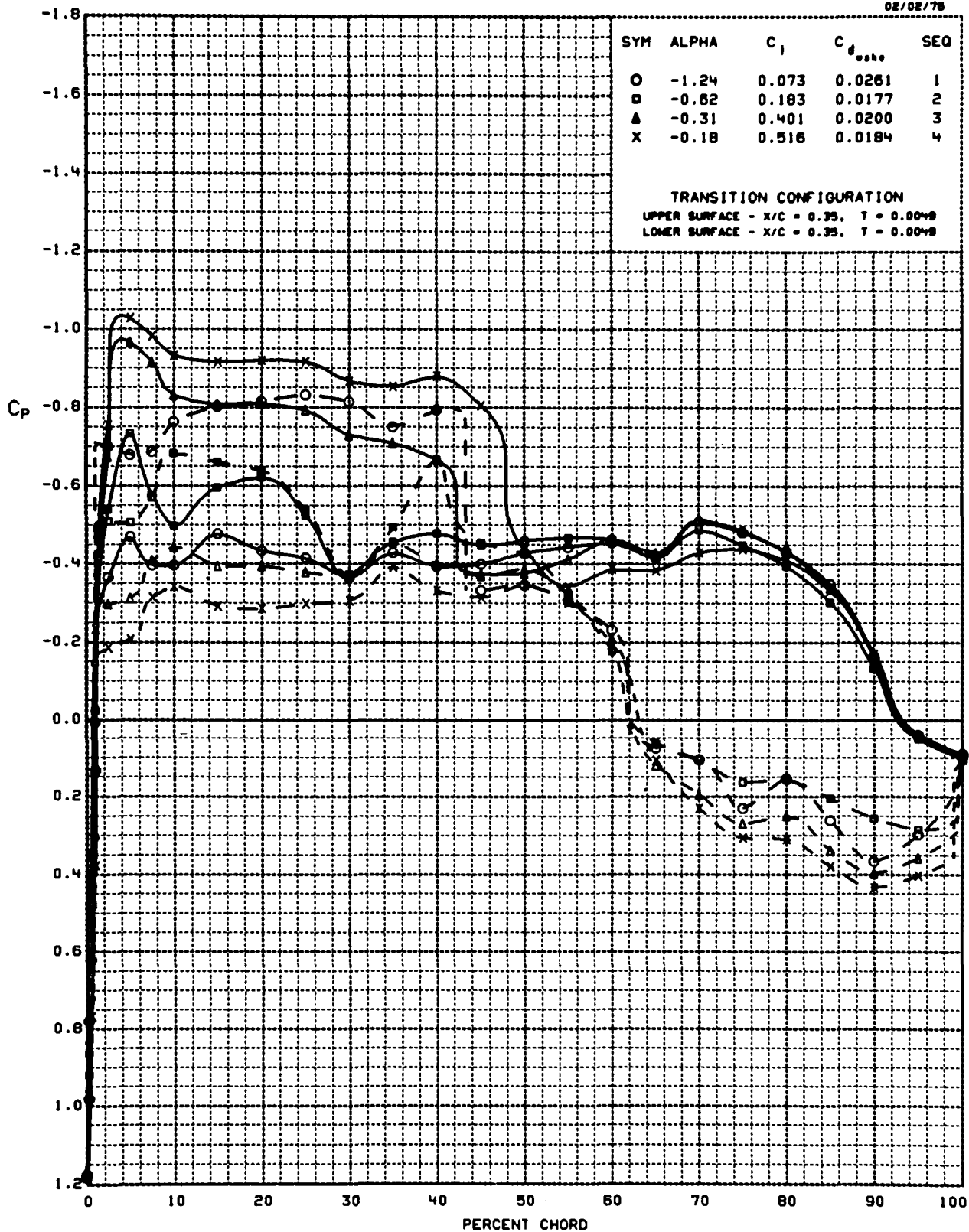
MACH NUMBER = 0.799

REYNOLDS NUMBER =  $1.98 \times 10^6$

RUN = 78

AMES 22-060-5

02/02/78



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

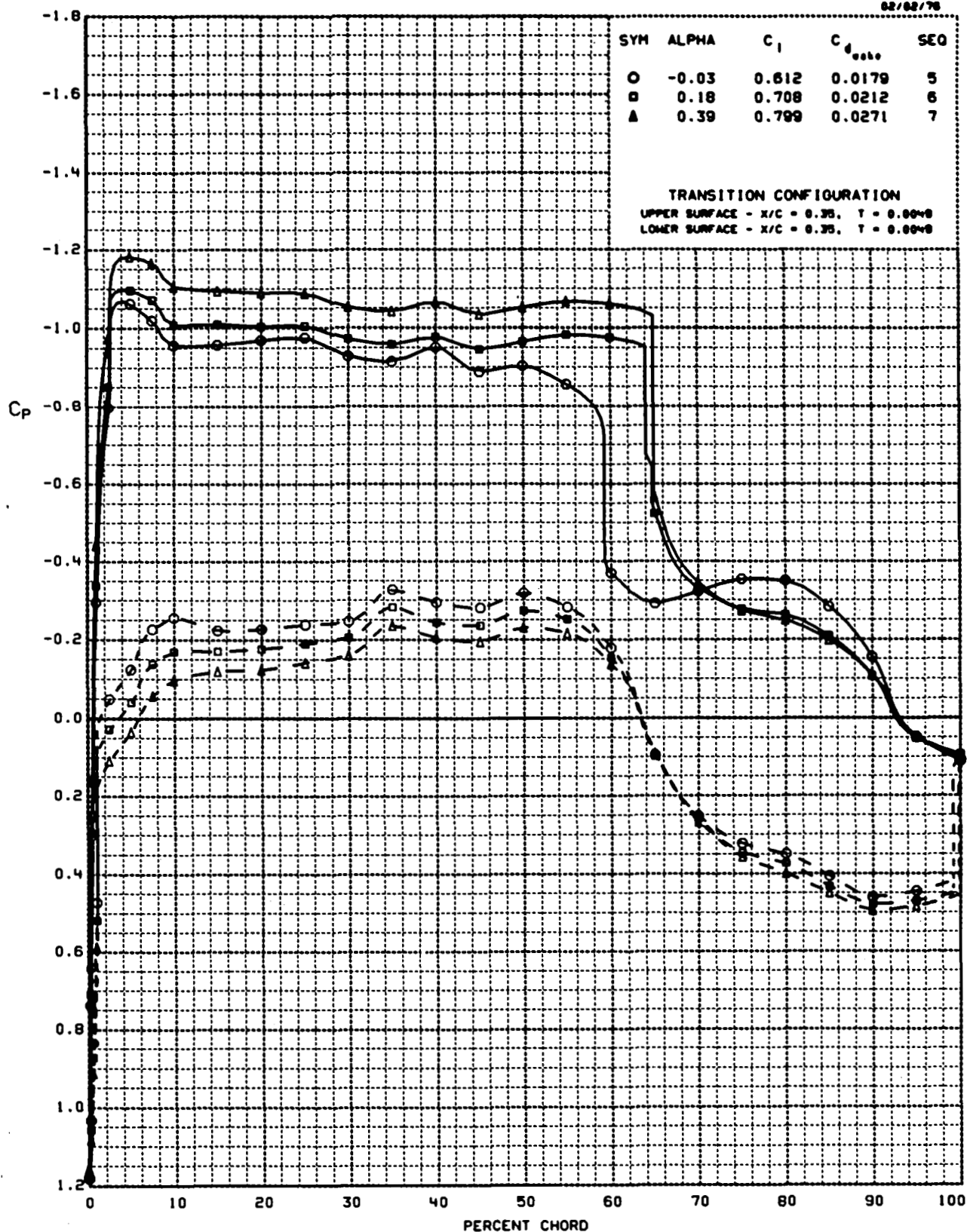
MACH NUMBER = 0.801

REYNOLDS NUMBER =  $1.96 \times 10^6$

RUN = 78

AMES 22-060-5

02/02/78



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

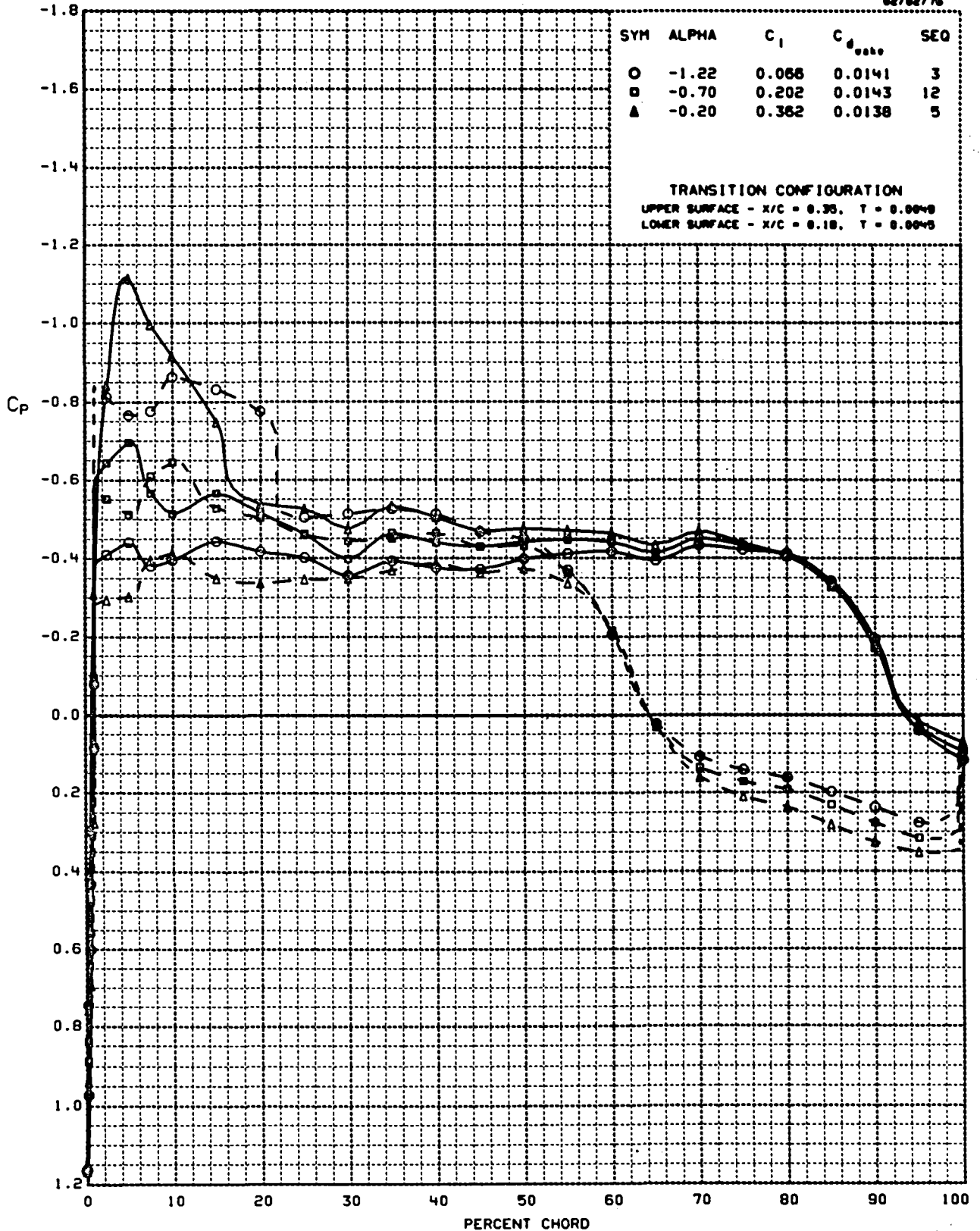
MACH NUMBER = 0.759

REYNOLDS NUMBER =  $2.00 \times 10^8$

RUN = 79

AMES 22-060-5

02/02/70



# WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

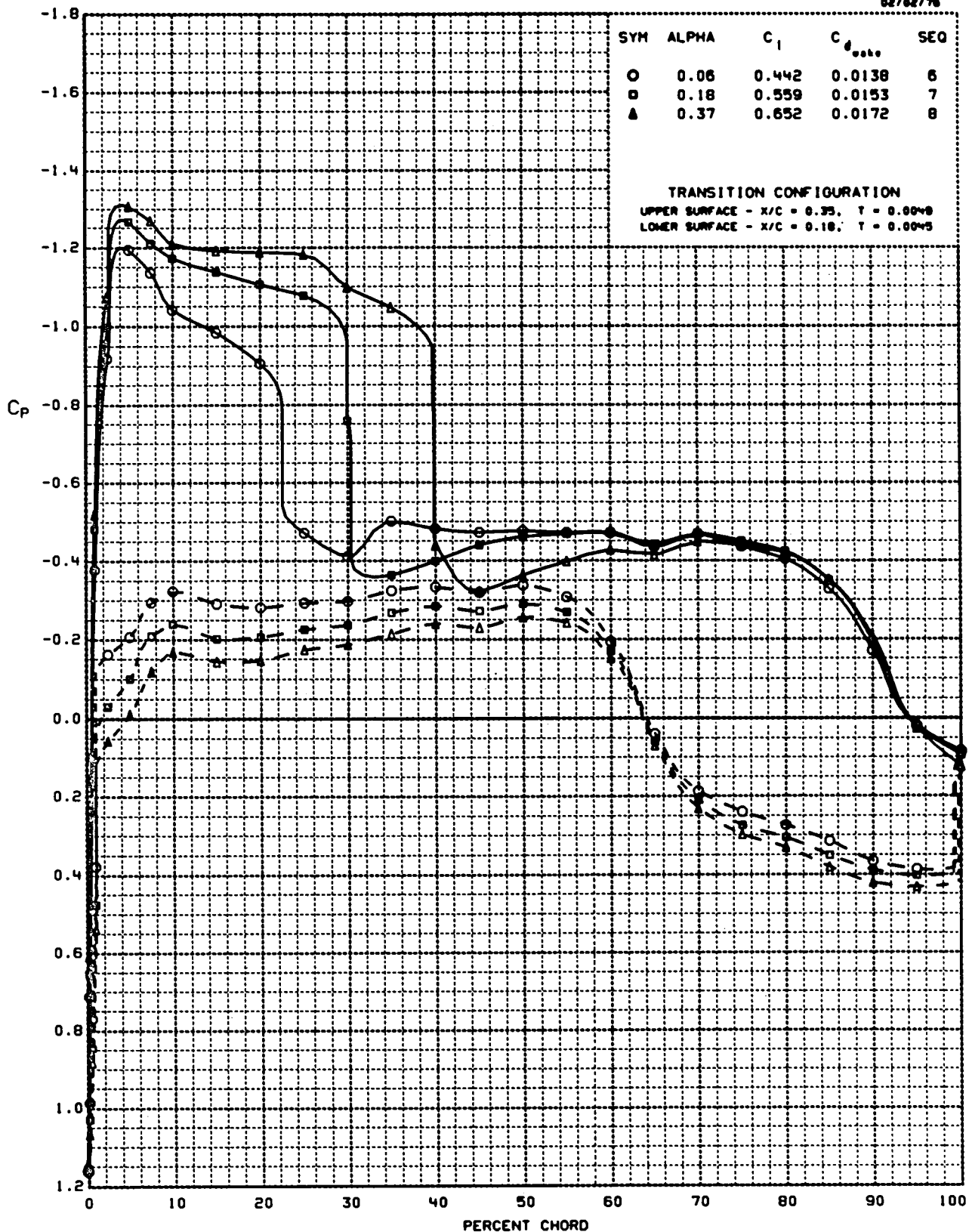
MACH NUMBER = 0.757

REYNOLDS NUMBER =  $1.98 \times 10^6$

RUN = 79

AMES 22-080-5

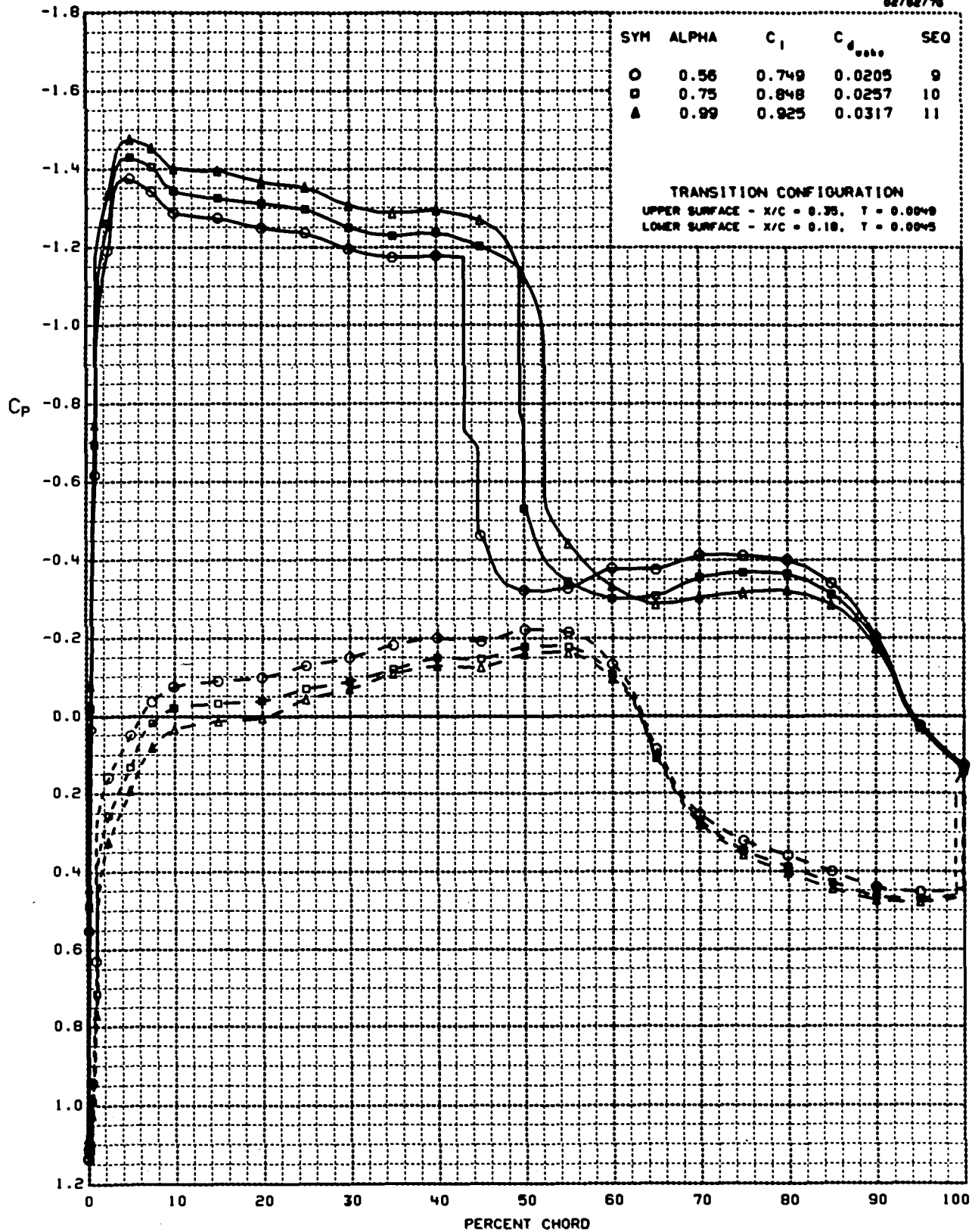
02/02/76





WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS  
 MACH NUMBER = 0.758 REYNOLDS NUMBER =  $1.97 \times 10^6$  RUN = 79 AMES 22-060-5

02/02/78

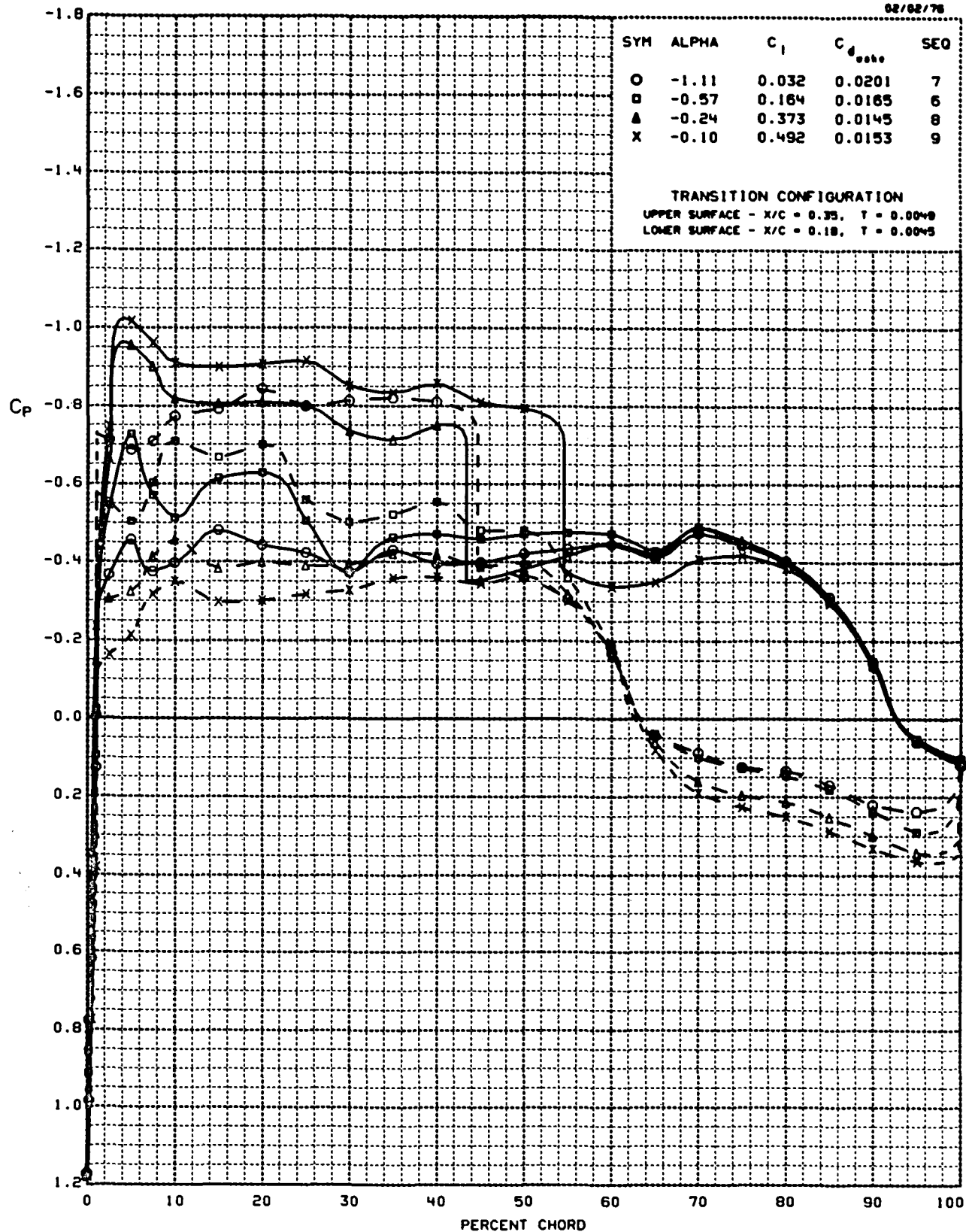




WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

MACH NUMBER = 0.799      REYNOLDS NUMBER =  $1.99 \times 10^6$       RUN = 80      AMES 22-060-5

02/02/76



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

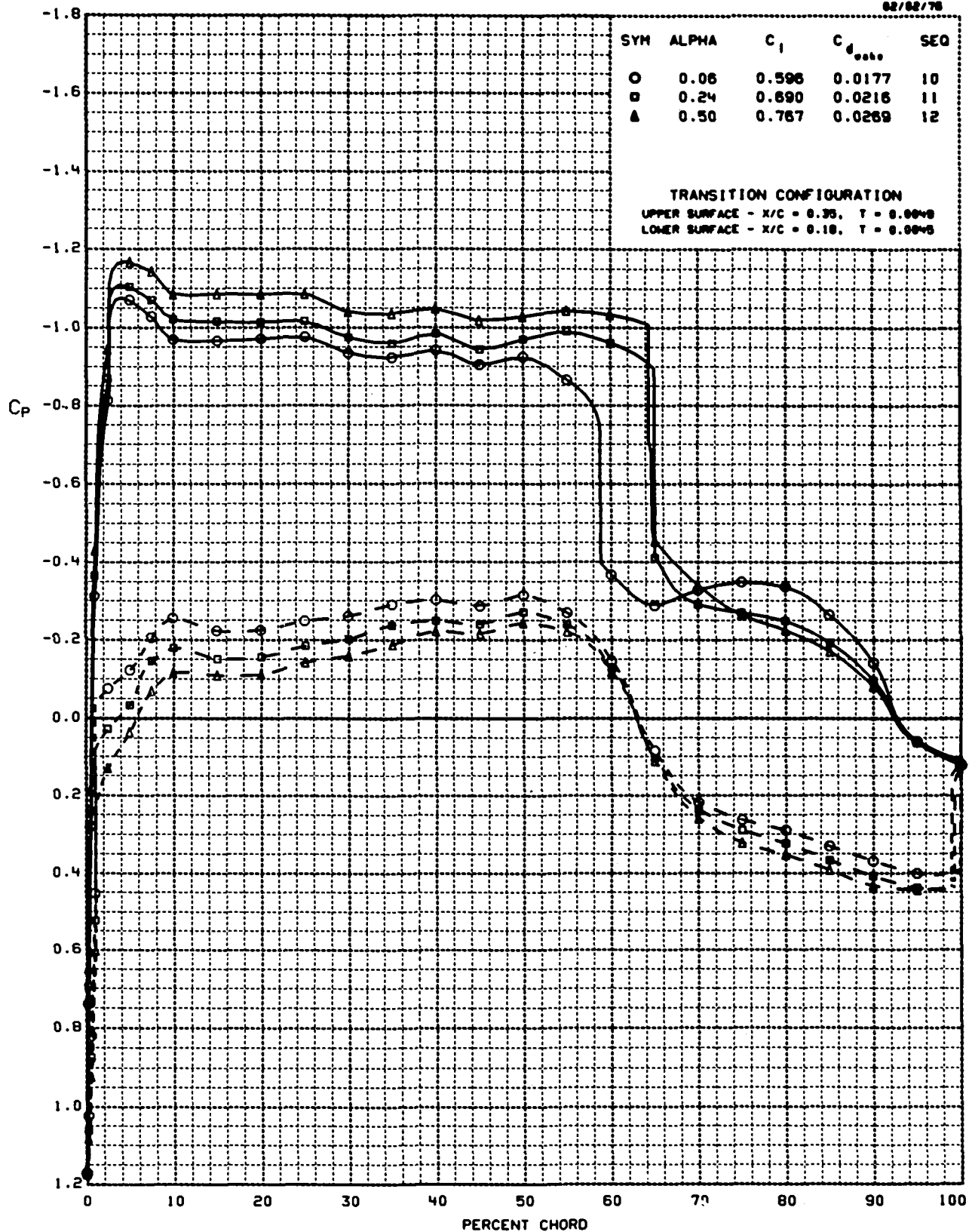
MACH NUMBER = 0.801

REYNOLDS NUMBER =  $1.98 \times 10^6$

RUN = 80

AMES 22-060-5

02/02/78



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

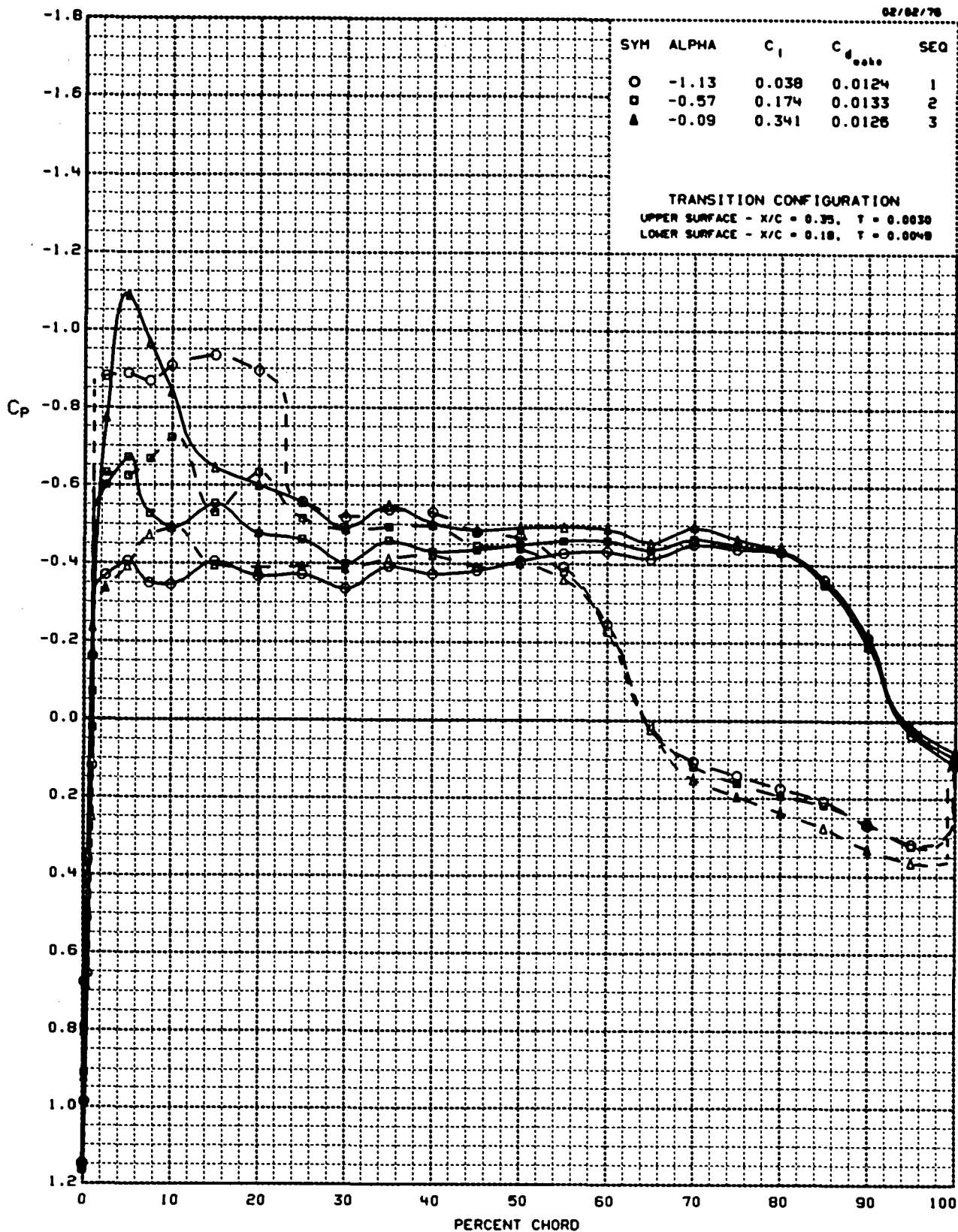
MACH NUMBER = 0.759

REYNOLDS NUMBER =  $3.97 \times 10^6$

RUN = 81

AMES 22-060-5

02/02/76



# WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

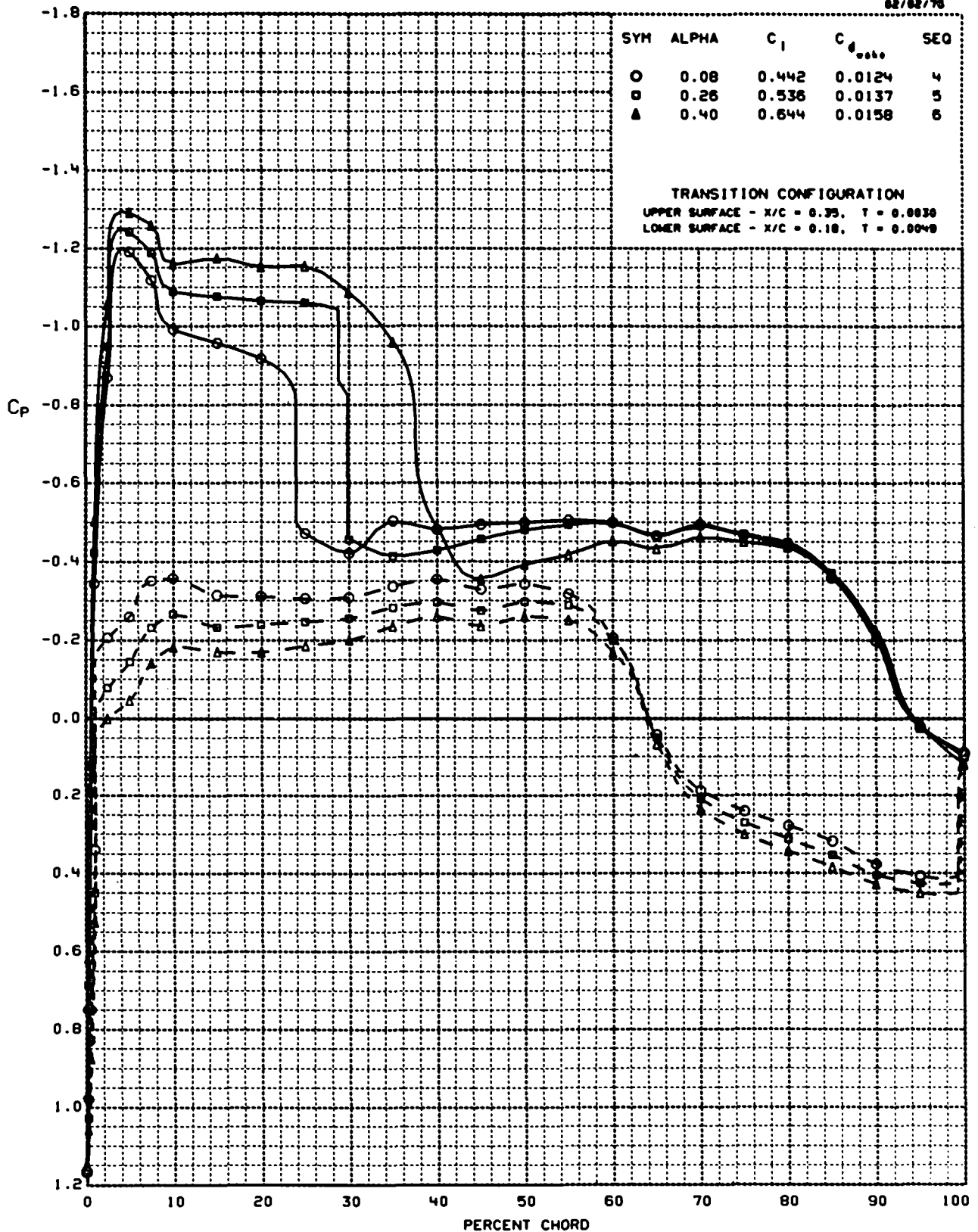
MACH NUMBER = 0.759

REYNOLDS NUMBER =  $3.99 \times 10^6$

RUN = 81

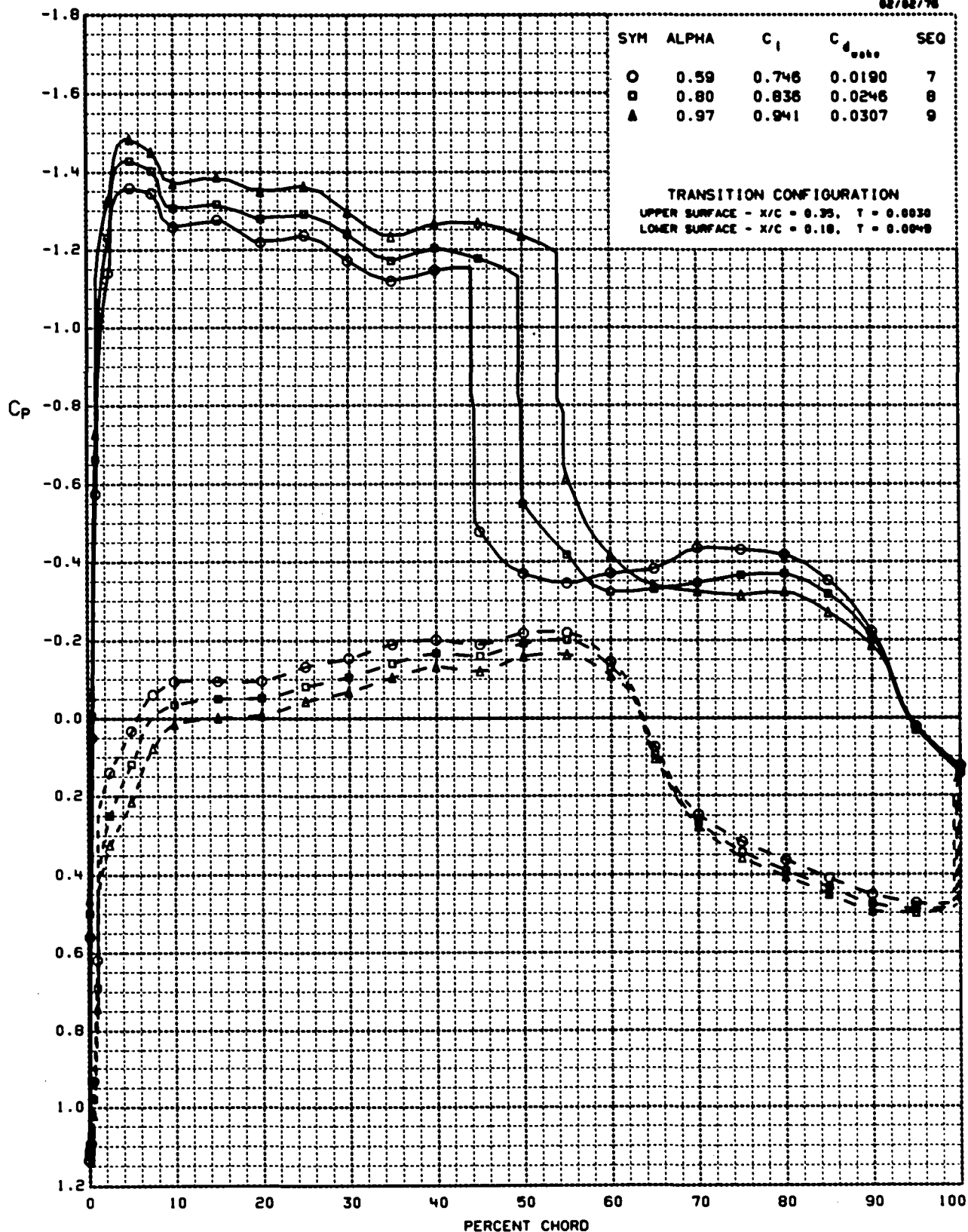
AMES 22-060-5

82/82/78



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS  
 MACH NUMBER = 0.758 REYNOLDS NUMBER =  $3.93 \times 10^6$  RUN = 81 AMES 22-060-5

02/02/78



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

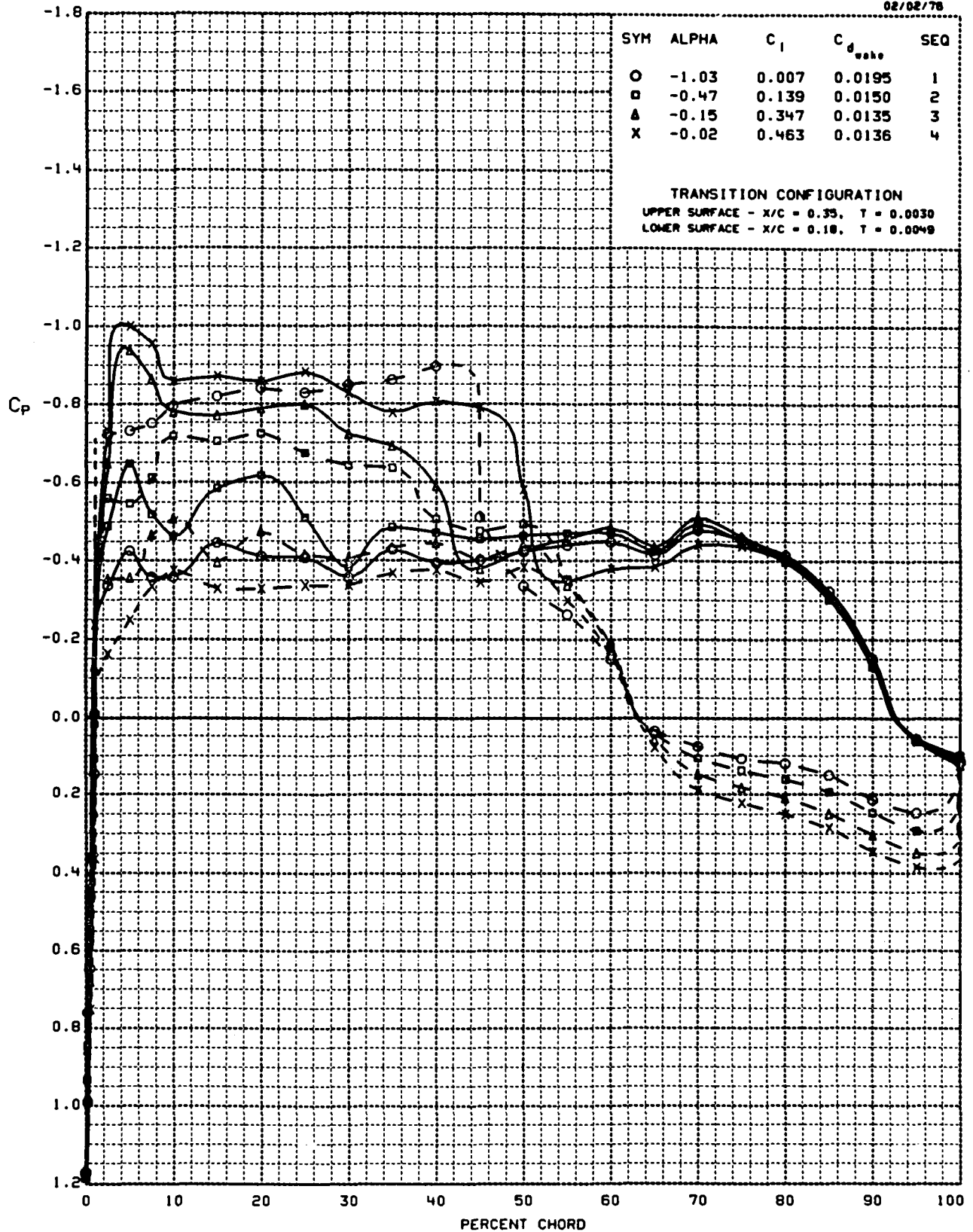
MACH NUMBER = 0.800

REYNOLDS NUMBER =  $2.99 \times 10^6$

RUN = 82

AMES 22-060-5

02/02/76





WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

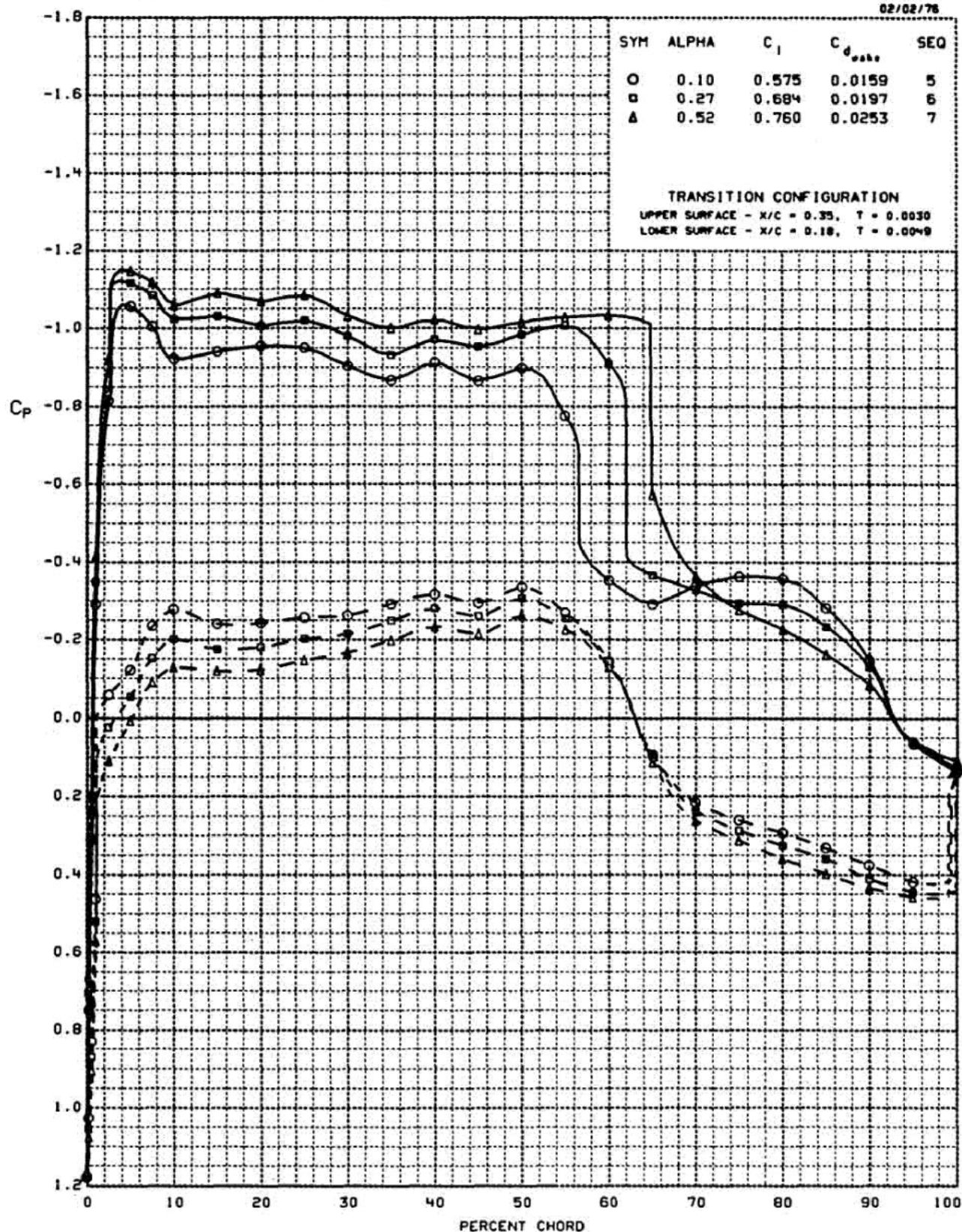
MACH NUMBER = 0.801

REYNOLDS NUMBER =  $2.97 \times 10^6$

RUN = 82

AMES 22-060-5

02/02/78



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

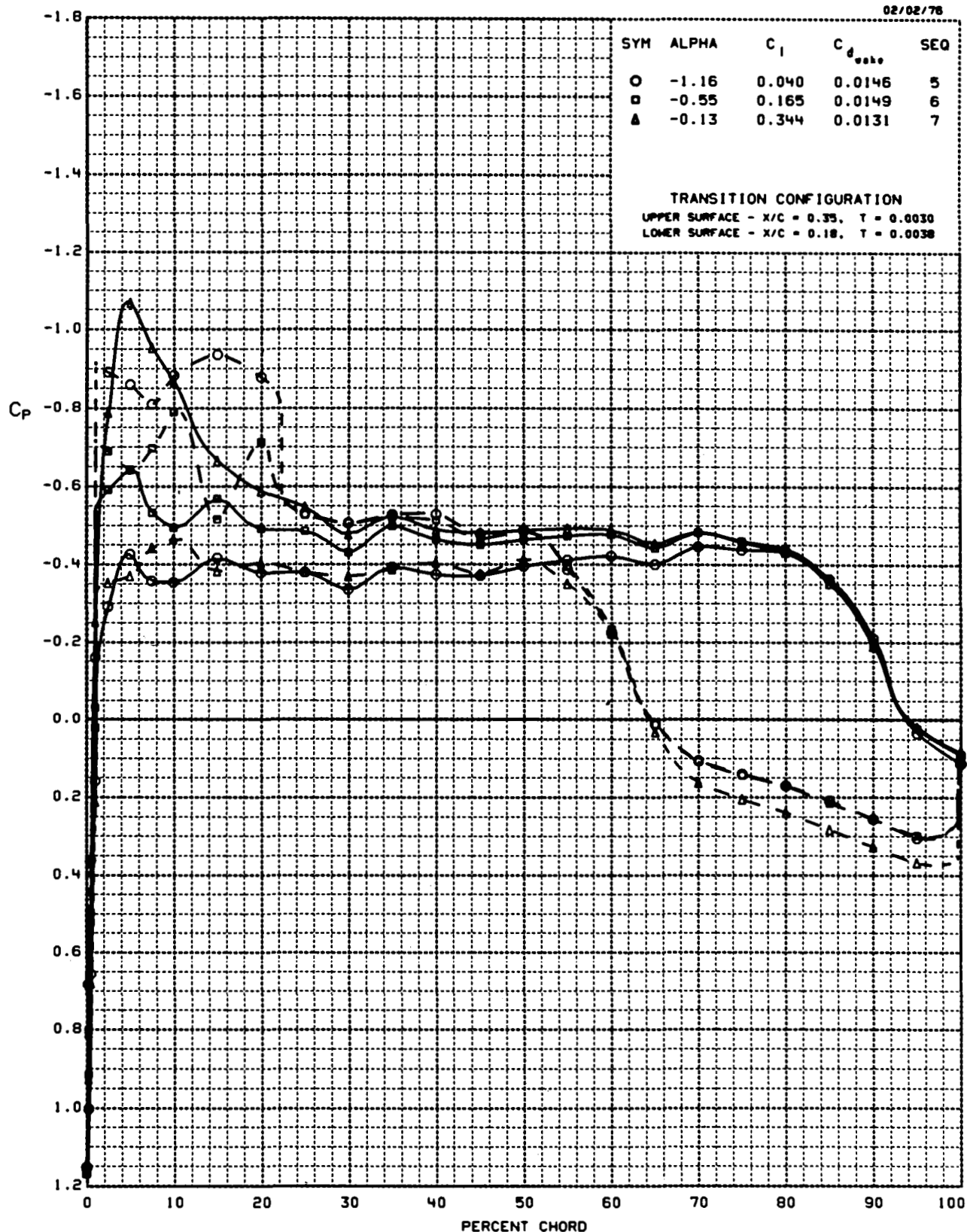
MACH NUMBER = 0.760

REYNOLDS NUMBER =  $3.97 \times 10^6$

RUN = 83

AMES 22-060-5

02/02/78





# WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

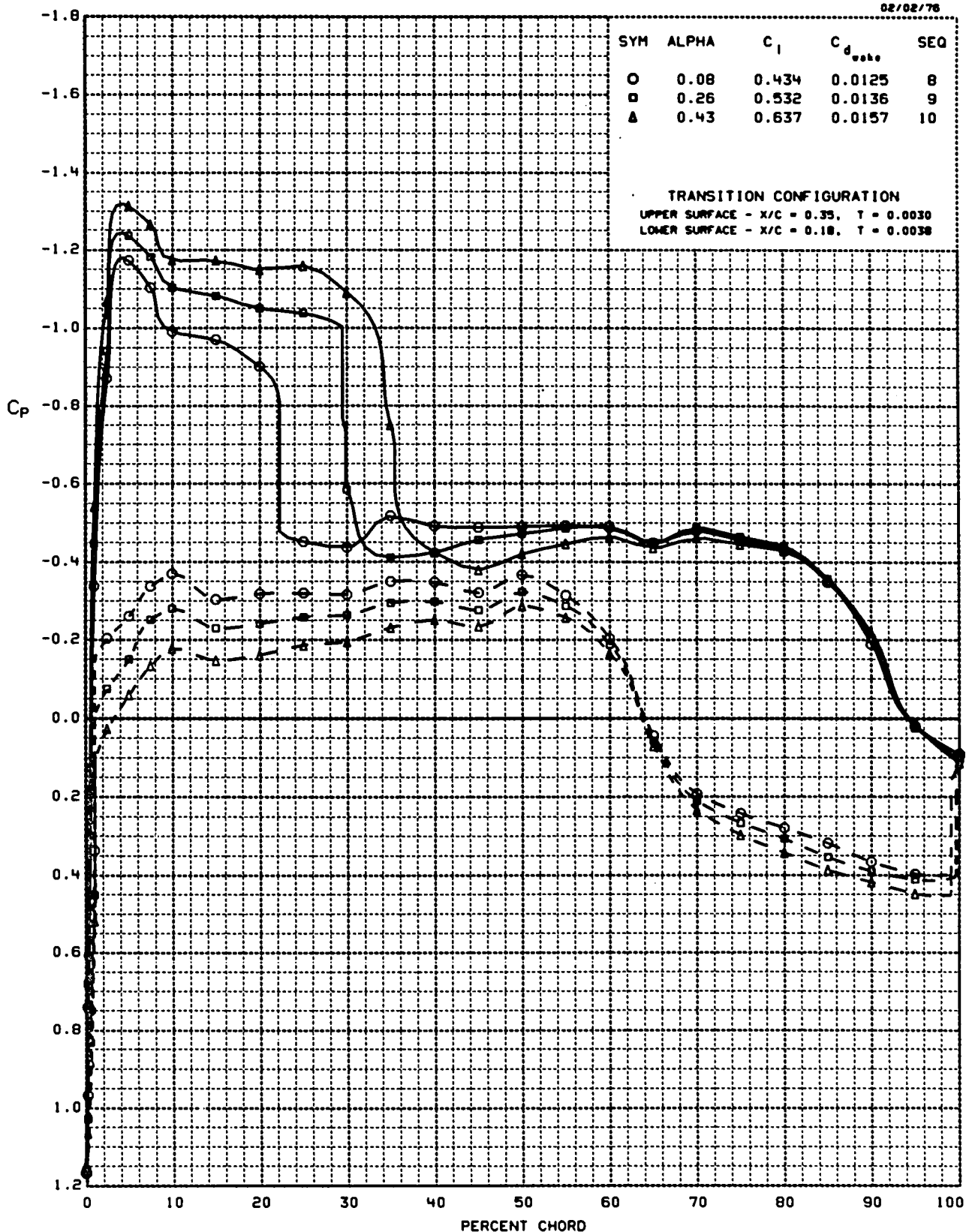
MACH NUMBER = 0.759

REYNOLDS NUMBER =  $3.97 \times 10^6$

RUN = 83

AMES 22-060-5

02/02/78



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

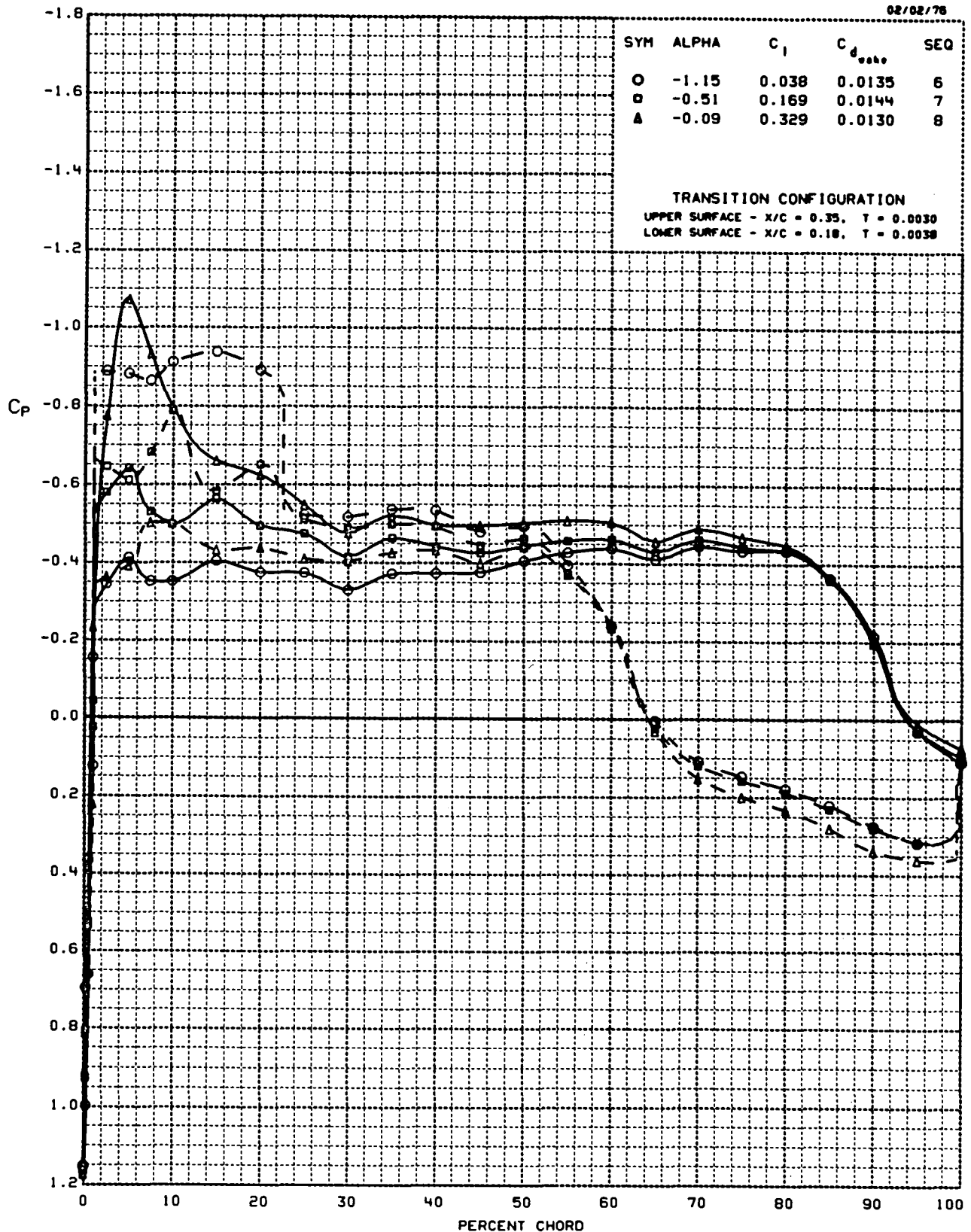
MACH NUMBER = 0.759

REYNOLDS NUMBER =  $3.98 \times 10^6$

RUN = 84

AMES 22-060-5

02/02/78



# WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

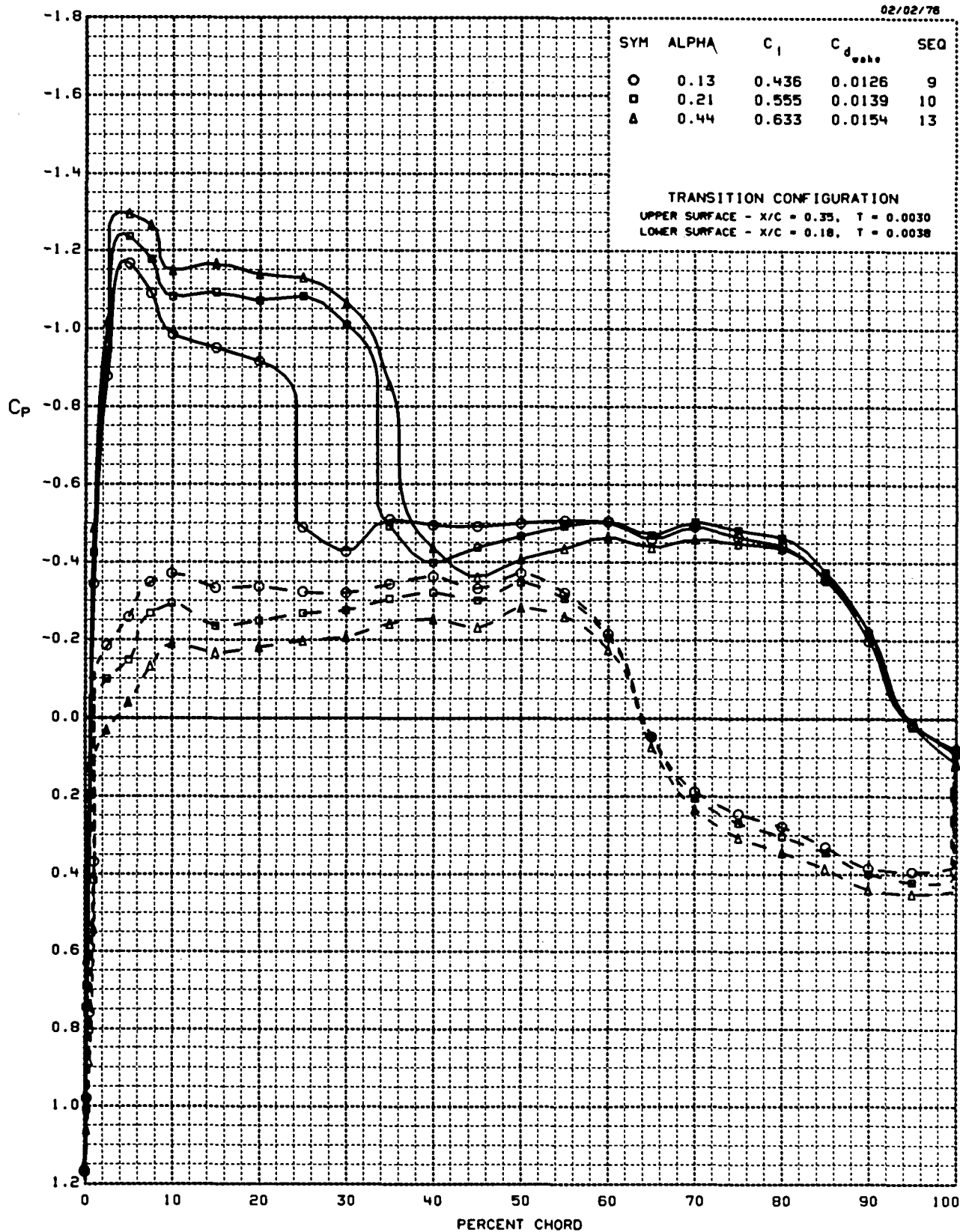
MACH NUMBER = 0.760

REYNOLDS NUMBER =  $3.96 \times 10^6$

RUN = 84

AMES 22-060-5

02/02/78



# WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

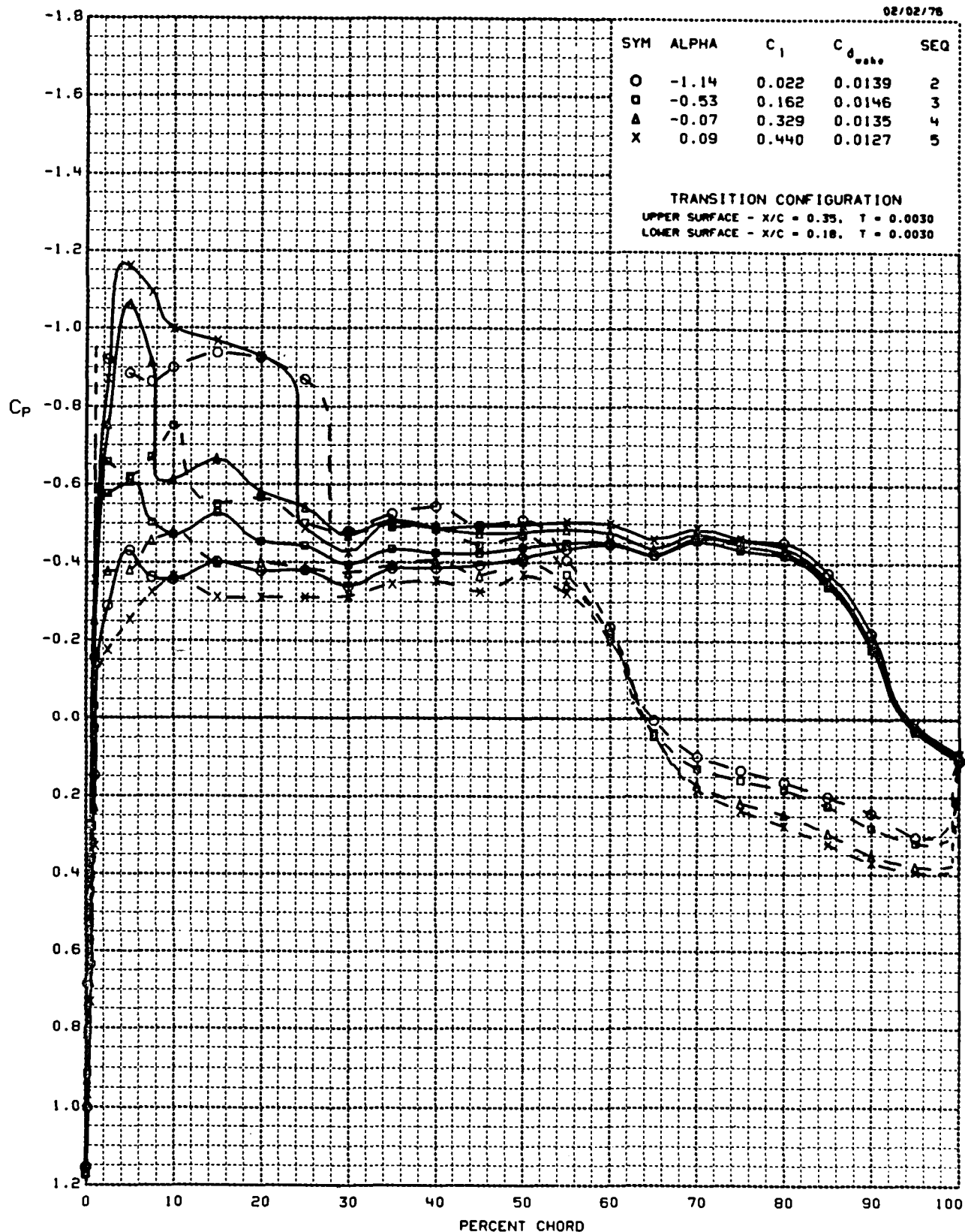
MACH NUMBER = 0.760

REYNOLDS NUMBER =  $3.94 \times 10^6$

RUN = 85

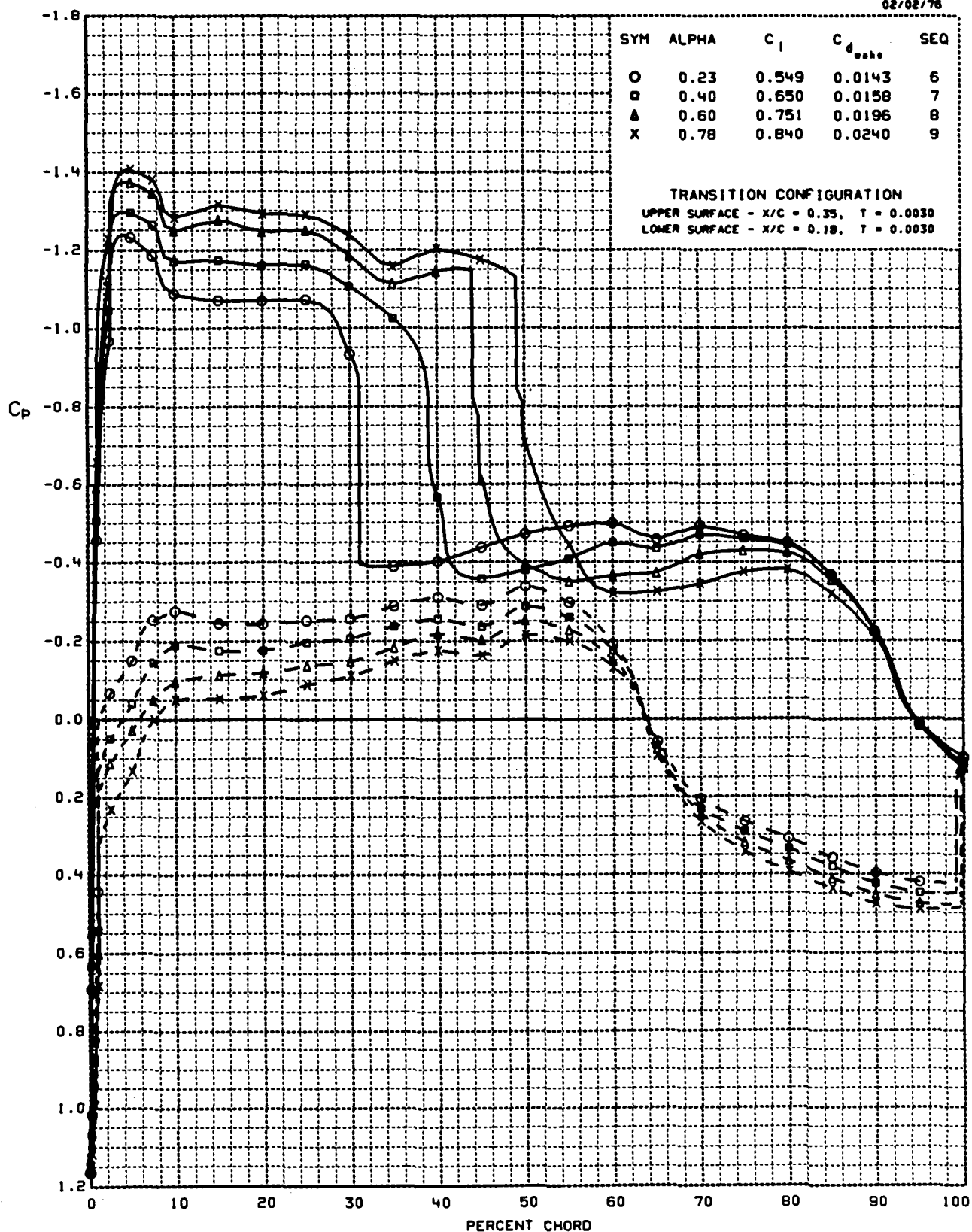
AMES 22-060-5

02/02/78



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS  
 MACH NUMBER = 0.759 REYNOLDS NUMBER =  $3.91 \times 10^6$  RUN = 85 AMES 22-060-5

02/02/78



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

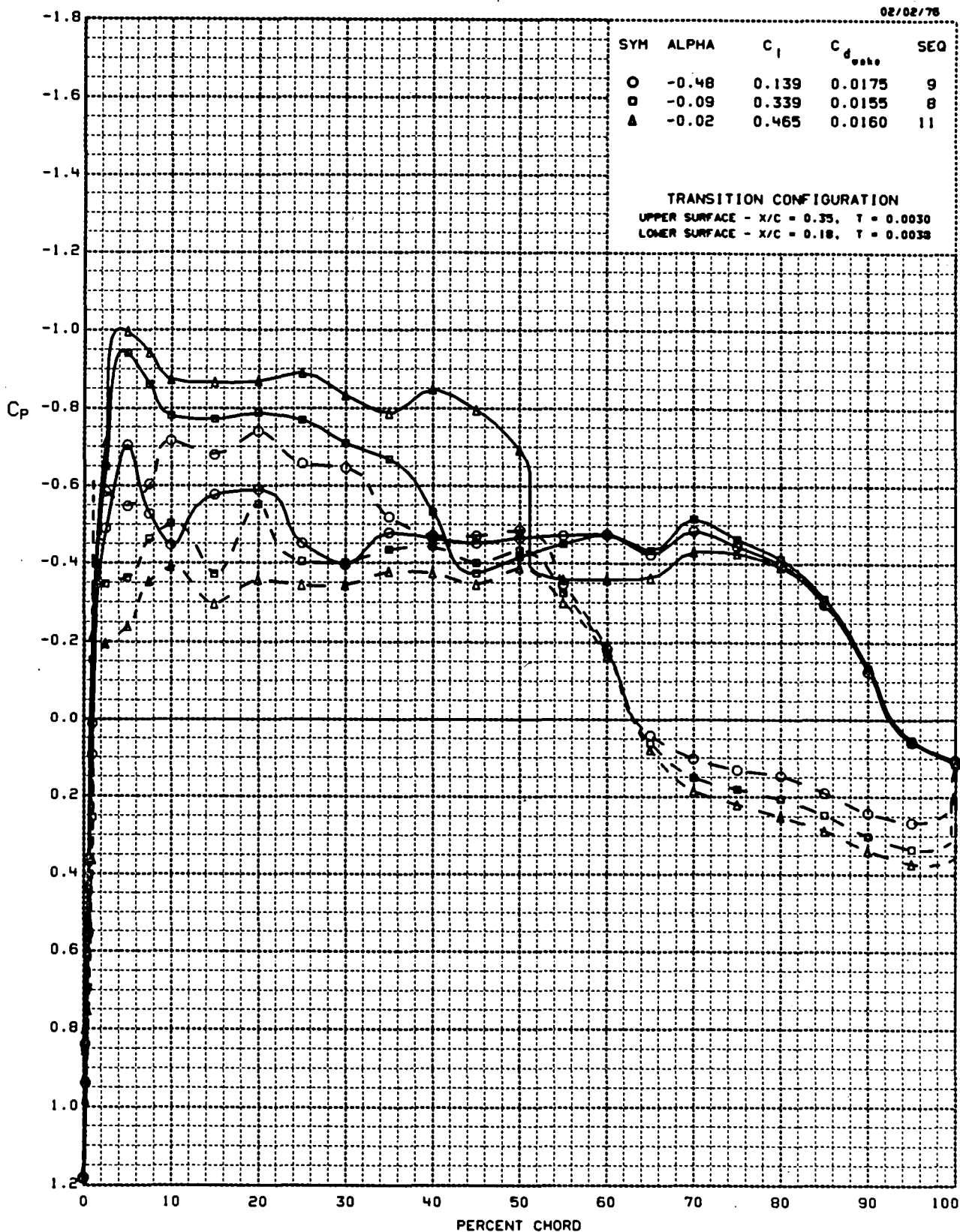
MACH NUMBER = 0.801

REYNOLDS NUMBER =  $2.99 \times 10^6$

RUN = 86

AMES 22-060-5

02/02/78



# WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523

## TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

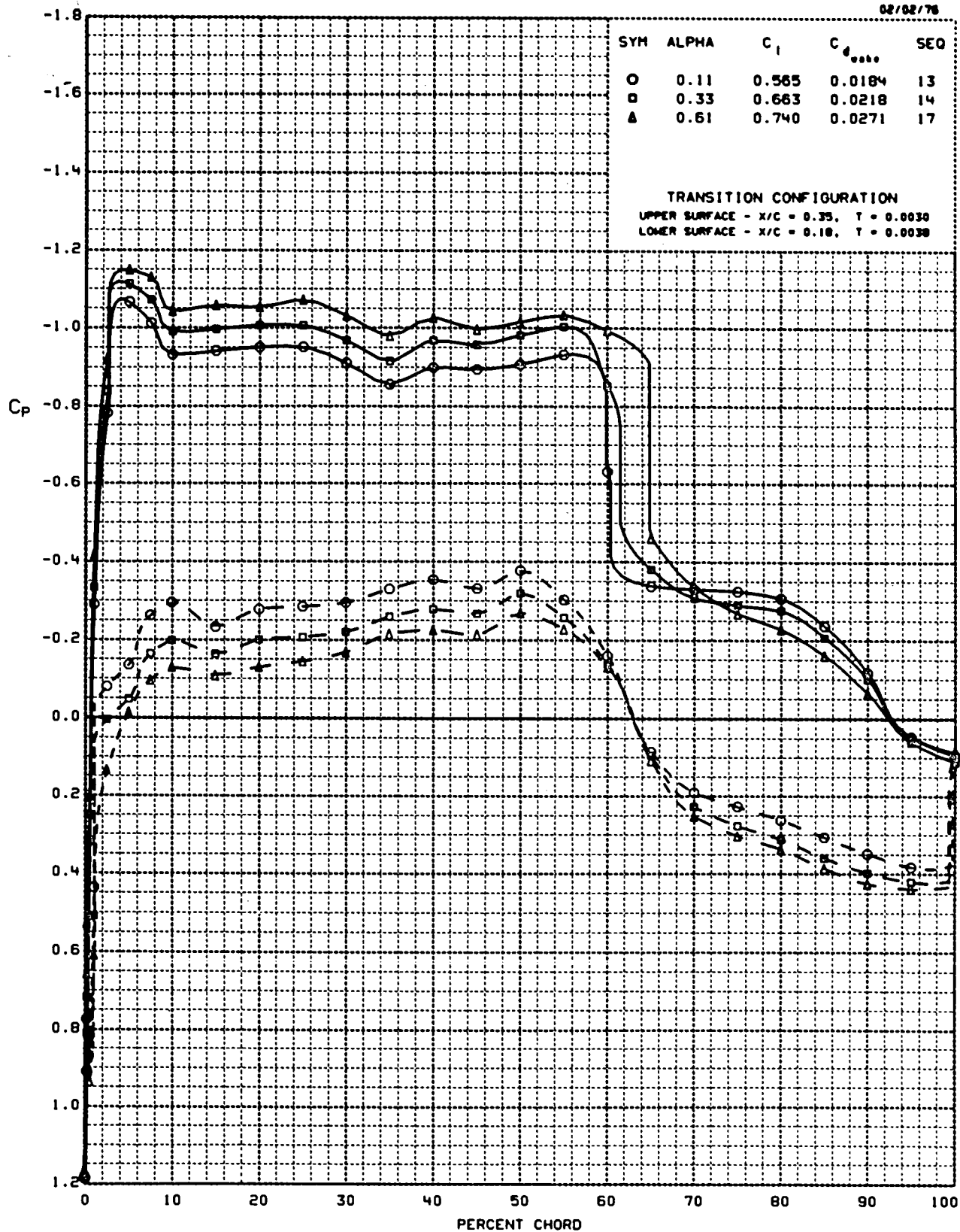
MACH NUMBER = 0.800

REYNOLDS NUMBER =  $3.01 \times 10^6$

RUN = 86

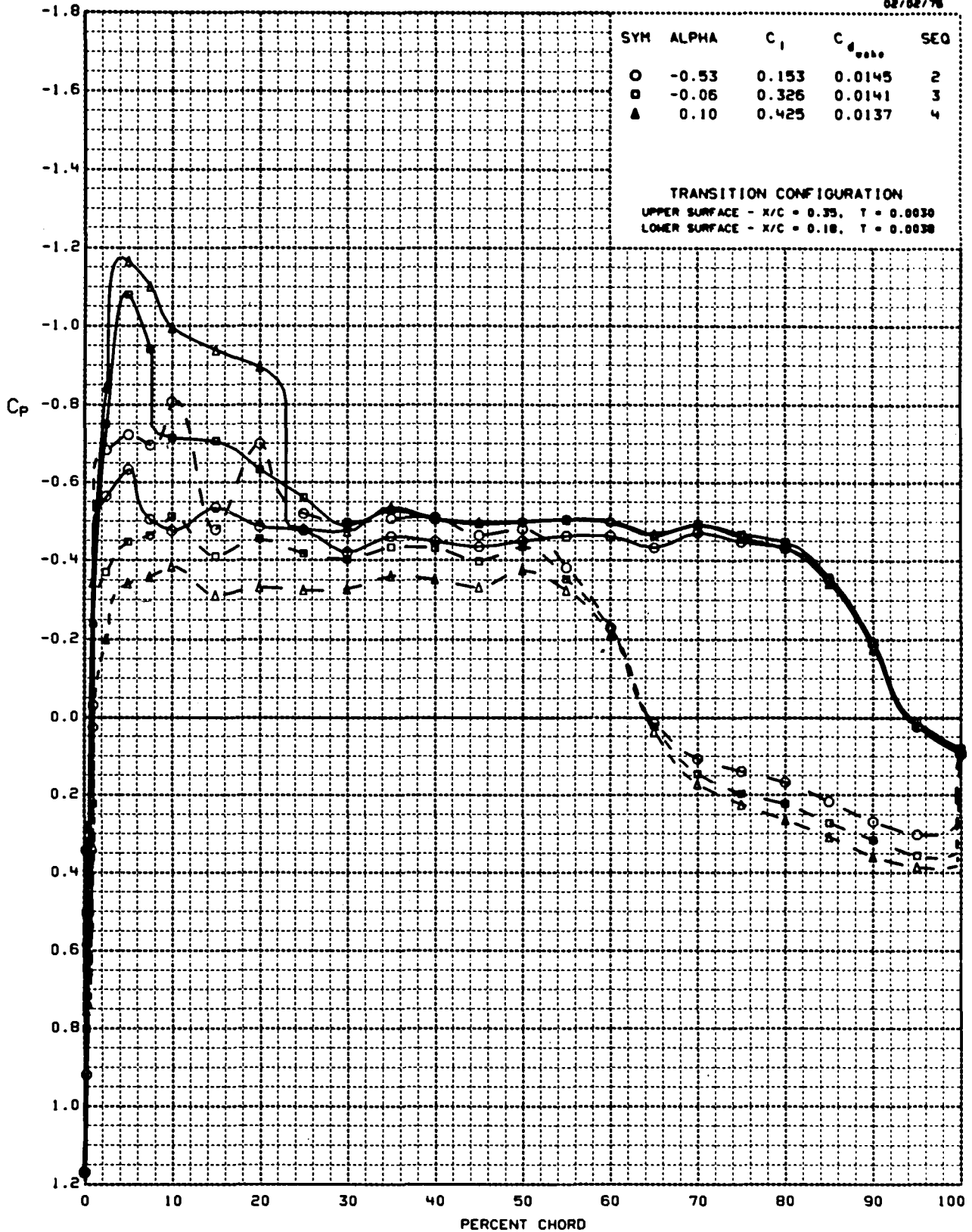
AMES 22-080-5

02/02/76



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS  
MACH NUMBER = 0.758 REYNOLDS NUMBER =  $3.96 \times 10^6$  RUN = 87 AMES 22-060-5

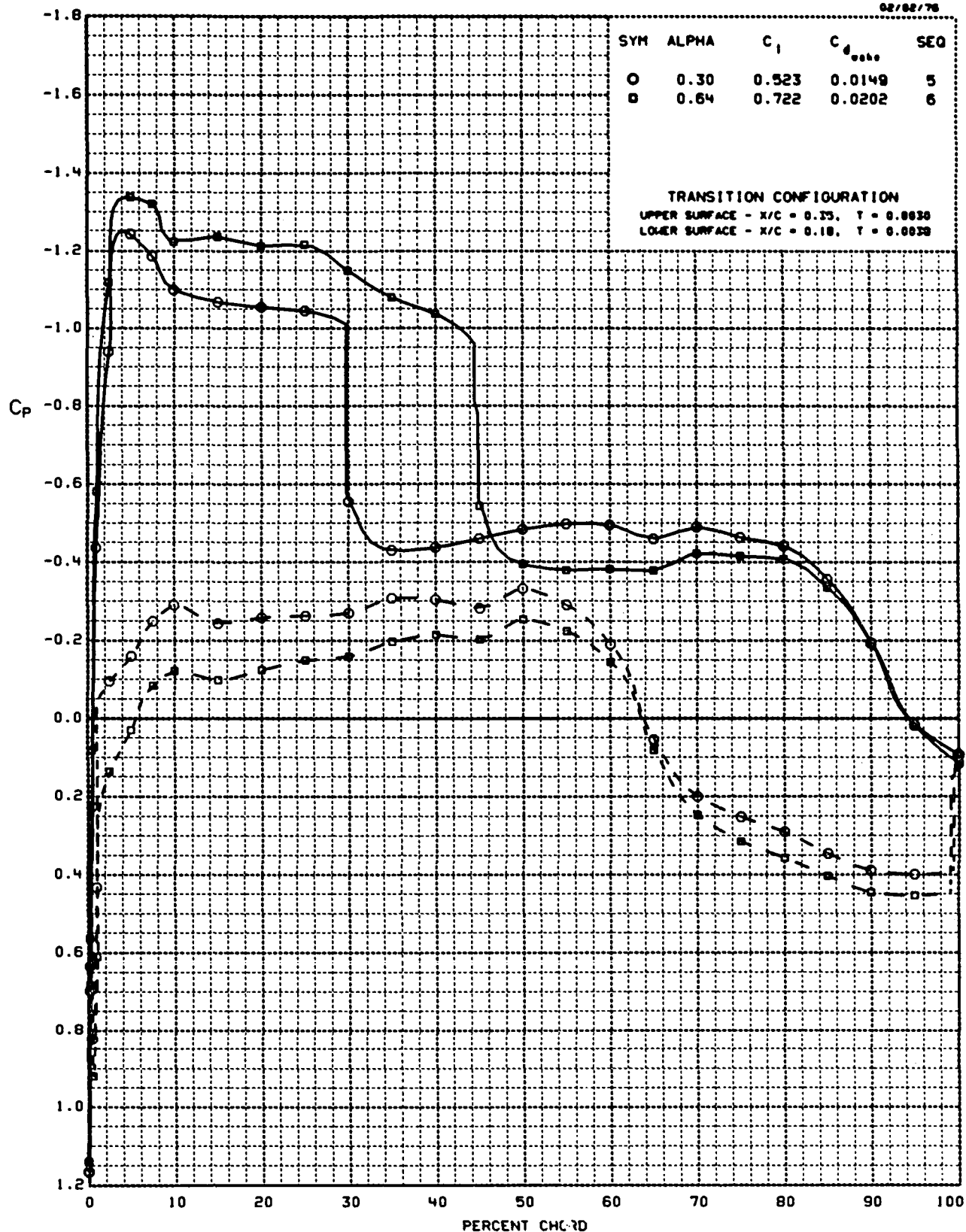
02/02/78





WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS  
MACH NUMBER = 0.758 REYNOLDS NUMBER =  $3.93 \times 10^6$  RUN = 87 AMES 22-060-5

02/02/76



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

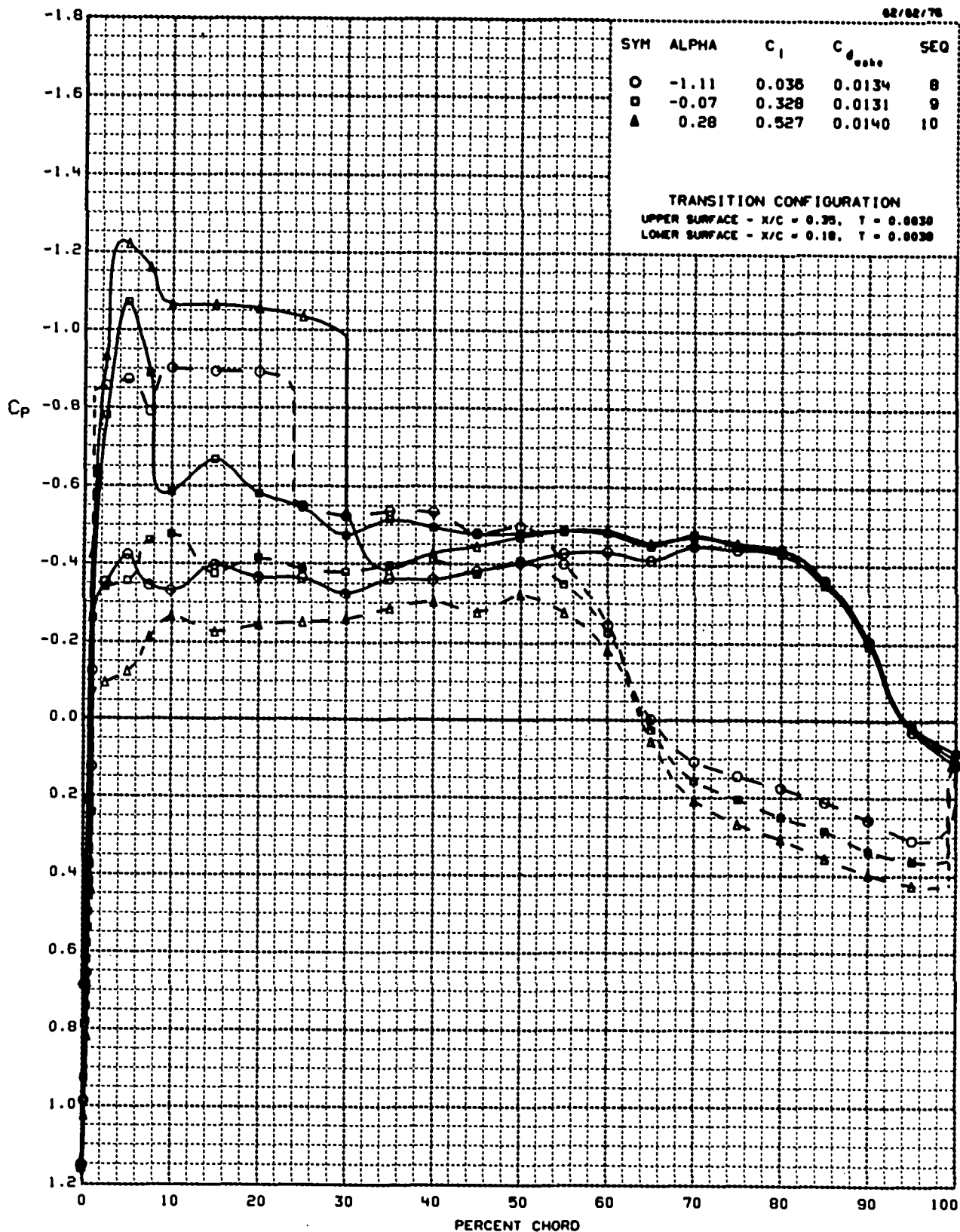
MACH NUMBER = 0.758

REYNOLDS NUMBER =  $3.94 \times 10^6$

RUN = 88

AMES 22-060-5

02/02/78



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

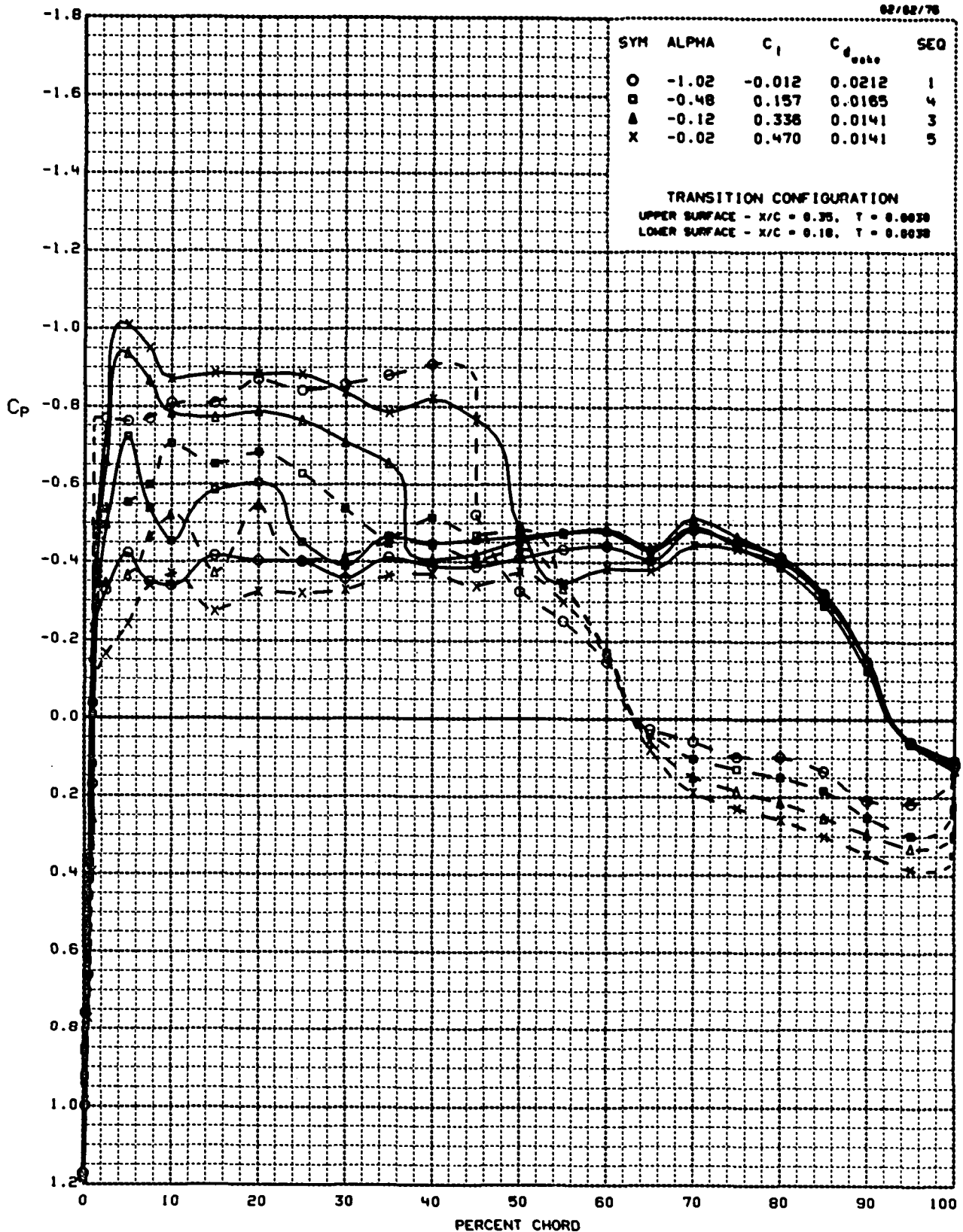
MACH NUMBER = 0.800

REYNOLDS NUMBER =  $2.99 \times 10^6$

RUN = 89

AMES 22-060-5

02/02/78



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

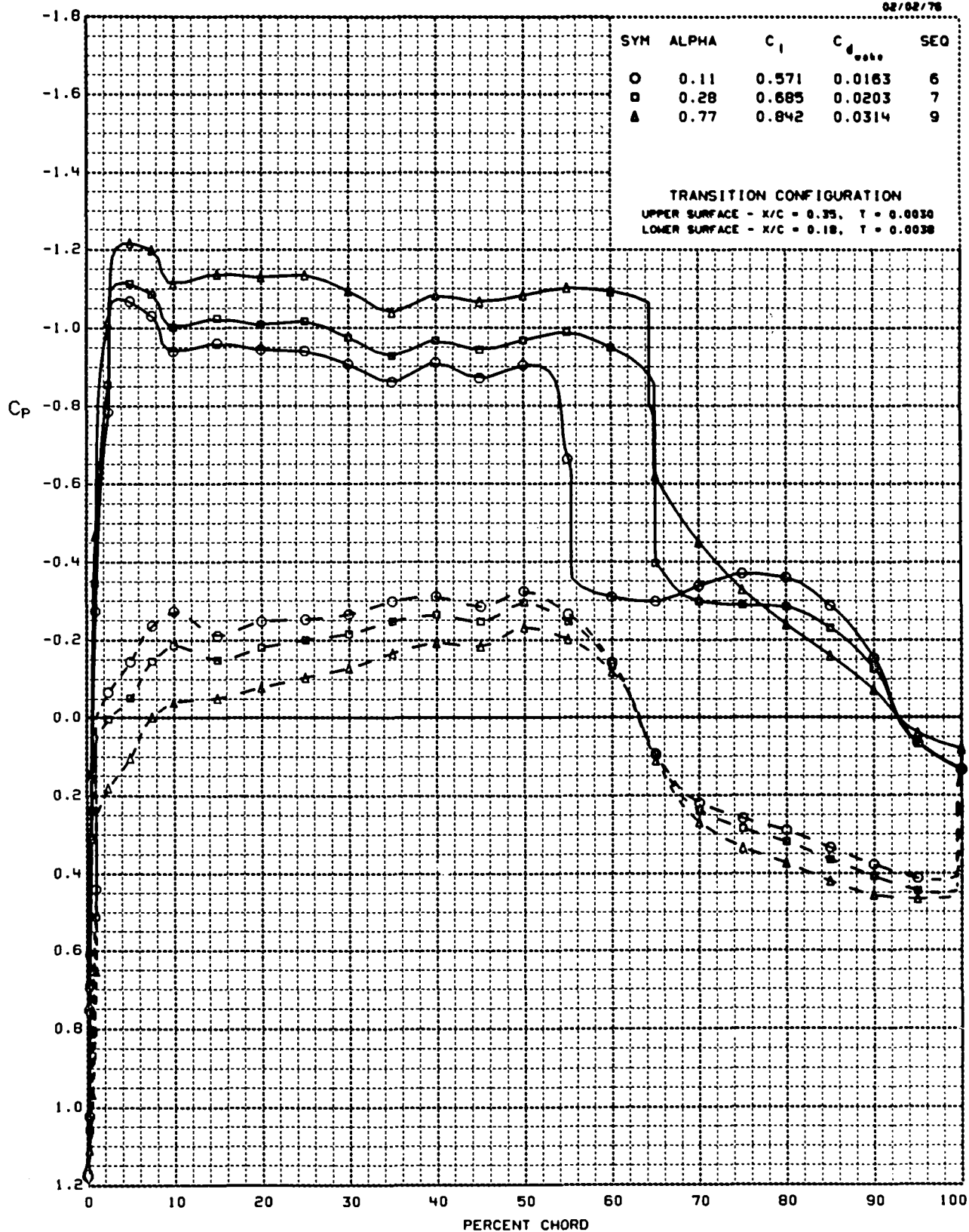
MACH NUMBER = 0.799

REYNOLDS NUMBER =  $2.99 \times 10^6$

RUN = 89

AMES 22-060-5

02/02/76



# WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

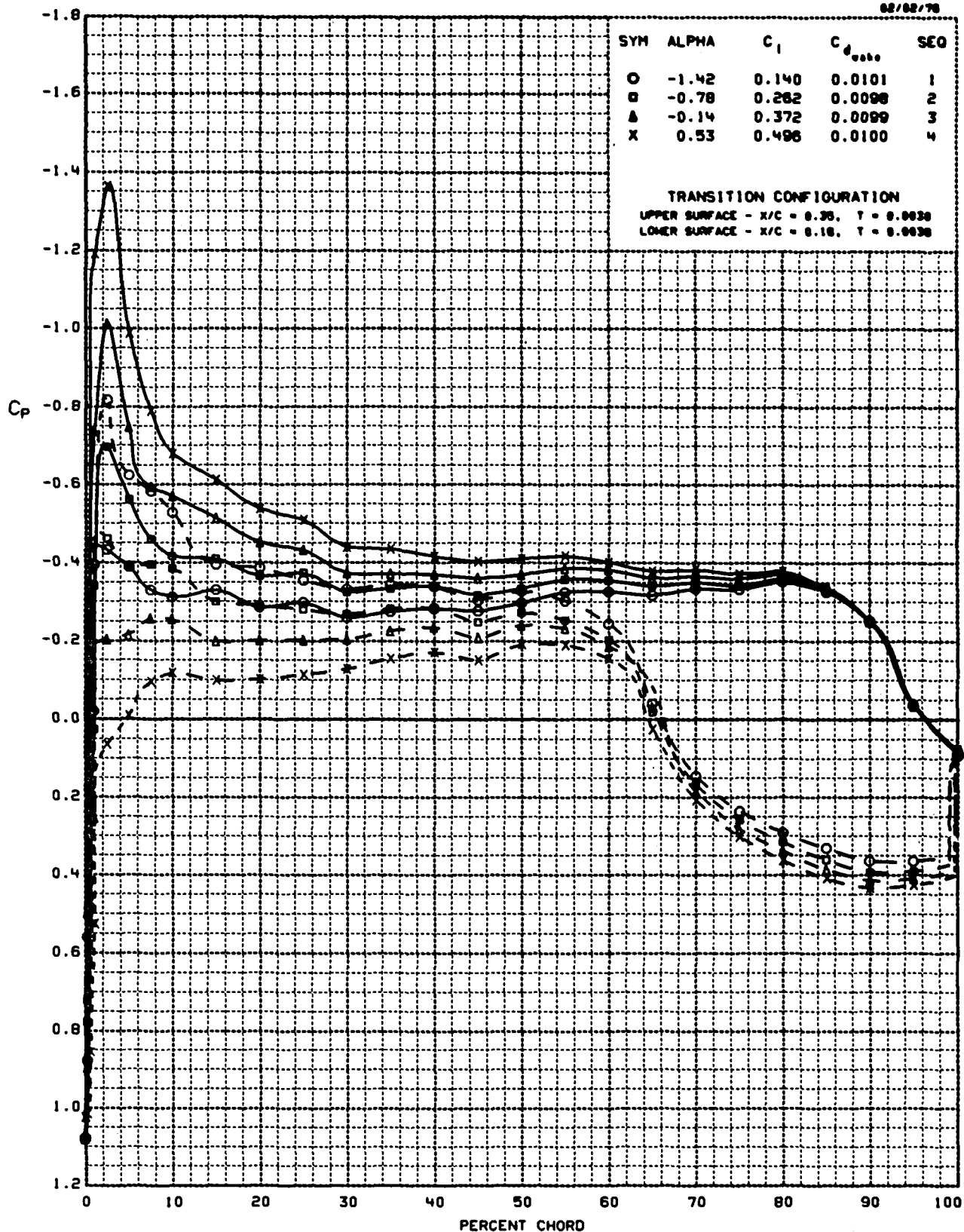
MACH NUMBER = 0.500

REYNOLDS NUMBER =  $3.99 \times 10^6$

RUN = 90

AMES 22-060-5

02/02/70



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

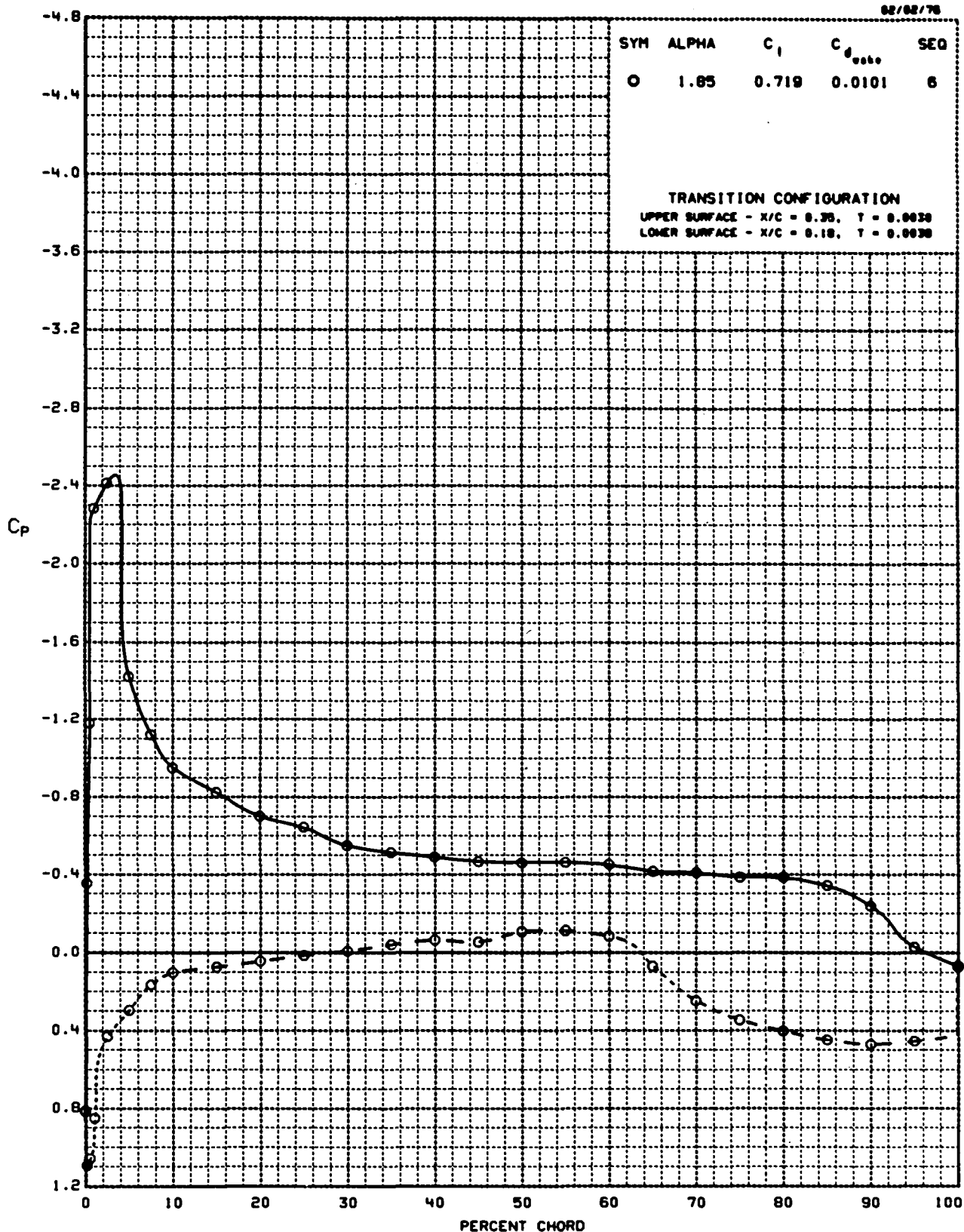
MACH NUMBER = 0.500

REYNOLDS NUMBER =  $3.98 \times 10^6$

RUN = 90

AHES 22-060-5

02/02/76



# WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

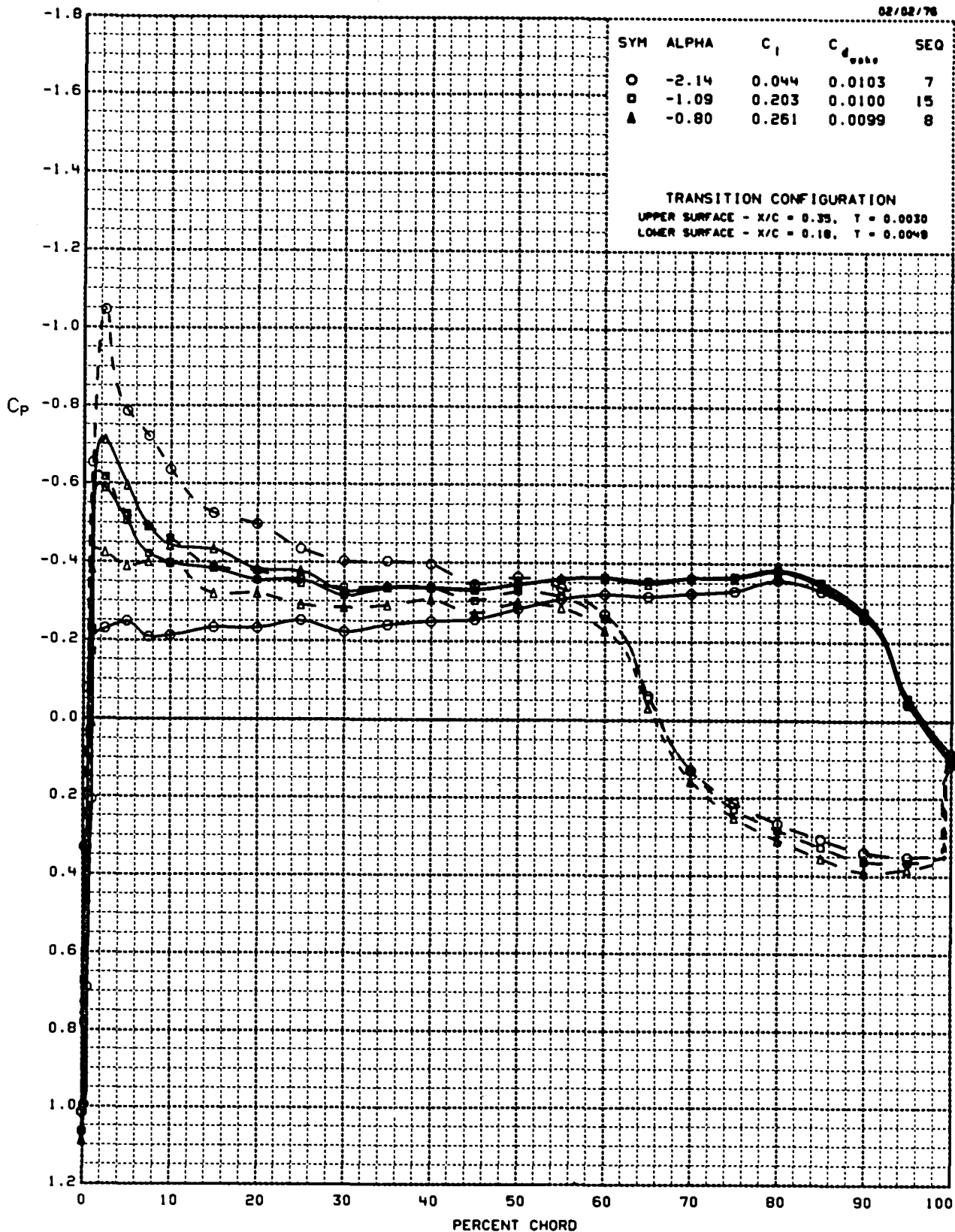
MACH NUMBER = 0.500

REYNOLDS NUMBER =  $3.99 \times 10^6$

RUN = 91

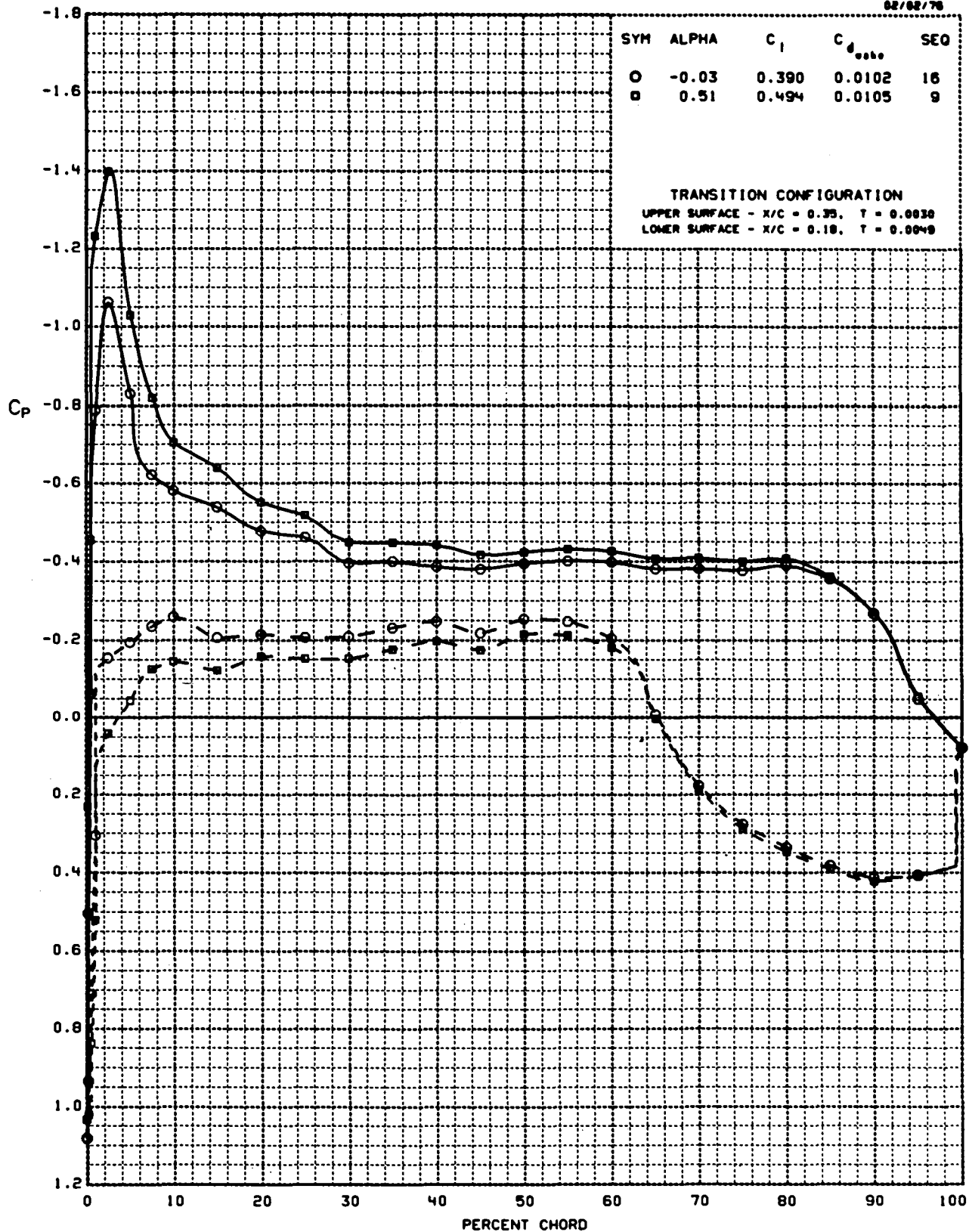
AMES 22-060-5

02/02/76



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS  
MACH NUMBER = 0.500 REYNOLDS NUMBER =  $4.01 \times 10^6$  RUN = 91 AMES 22-060-5

02/02/76





# WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523

## TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

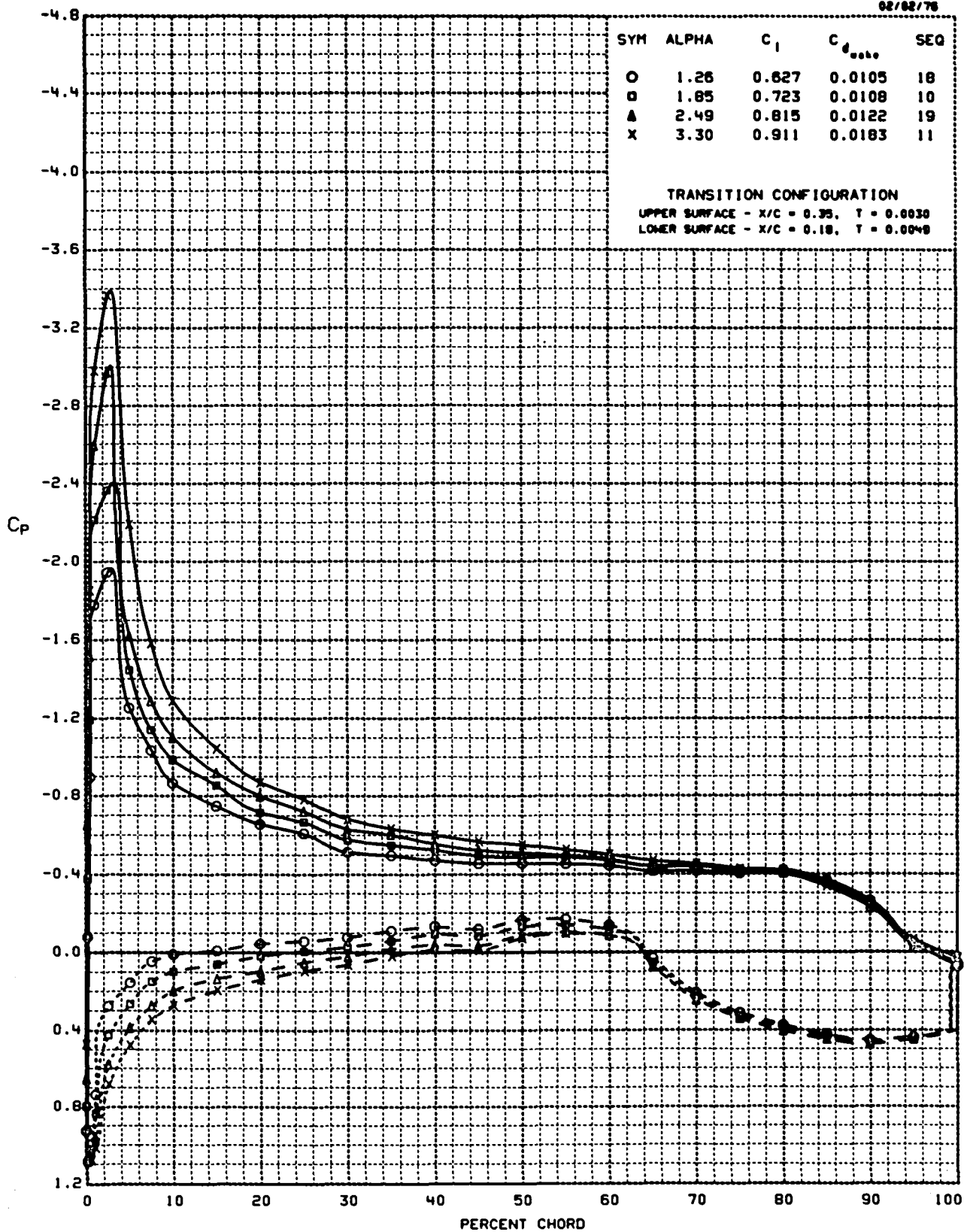
MACH NUMBER = 0.499

REYNOLDS NUMBER =  $3.99 \times 10^6$

RUN = 91

AMES 22-060-5

02/02/76



# WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

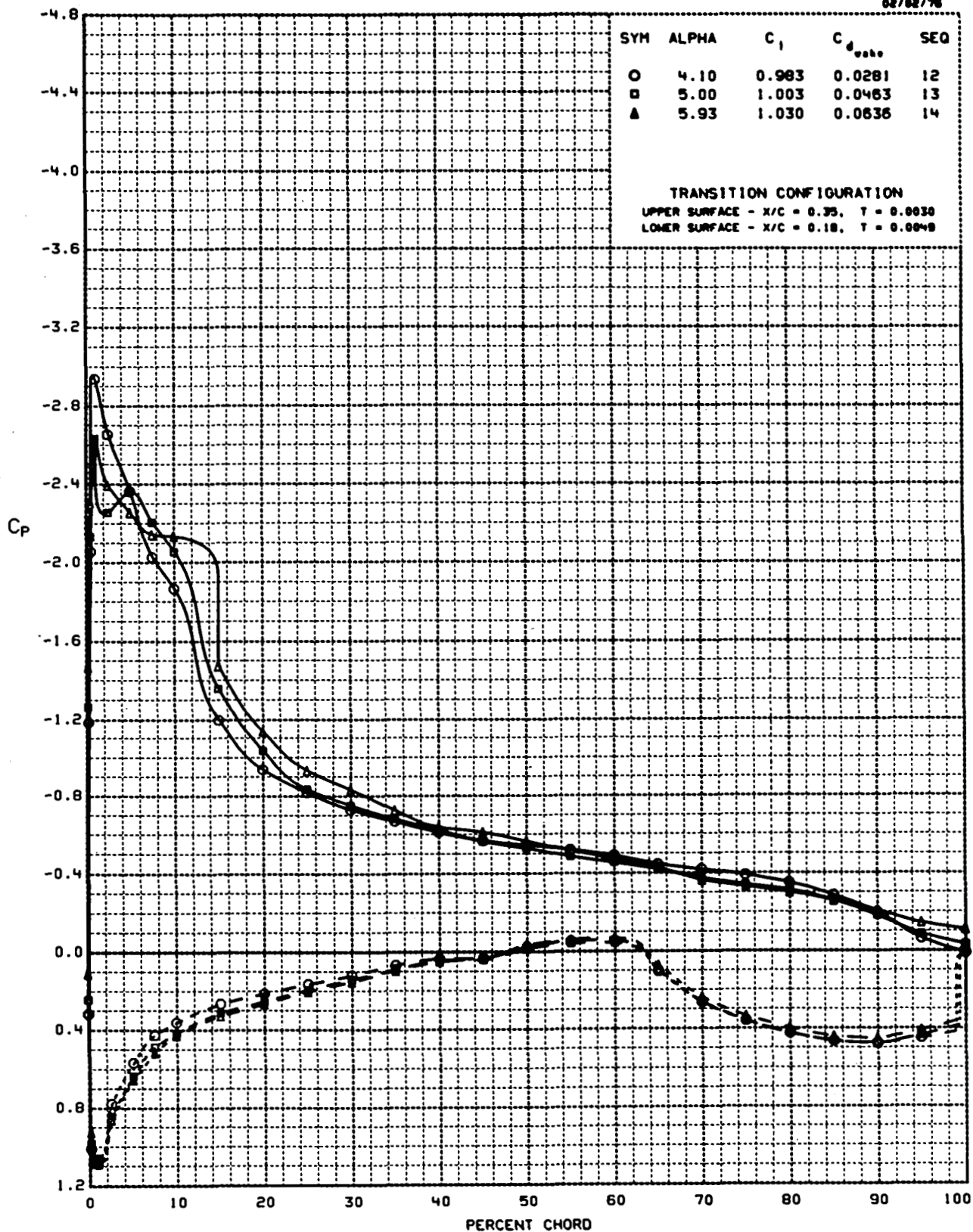
MACH NUMBER = 0.498

REYNOLDS NUMBER =  $3.98 \times 10^6$

RUN = 91

AMES 22-060-5

02/02/78



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

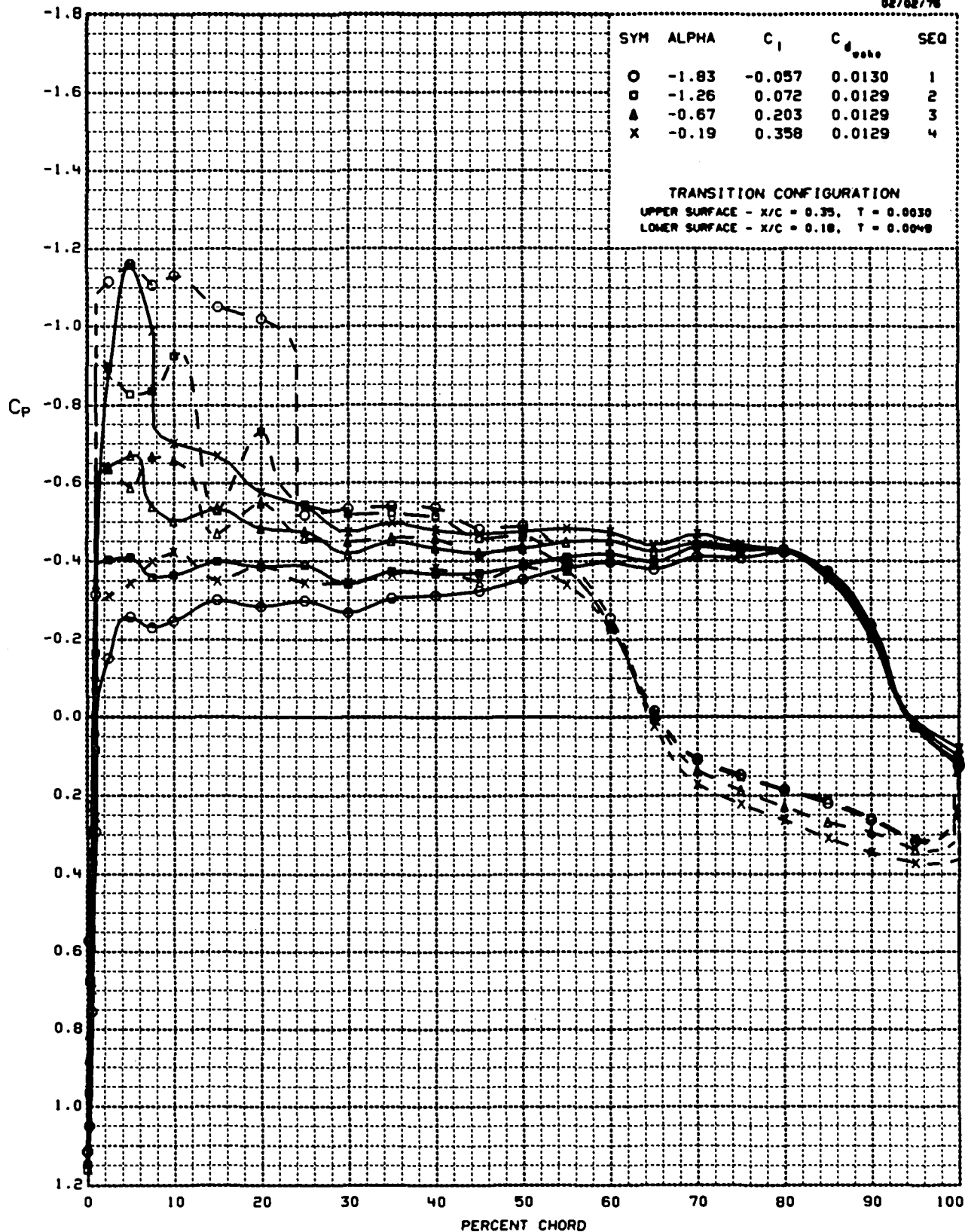
MACH NUMBER = 0.739

REYNOLDS NUMBER =  $3.96 \times 10^6$

RUN = 92

AMES 22-080-5

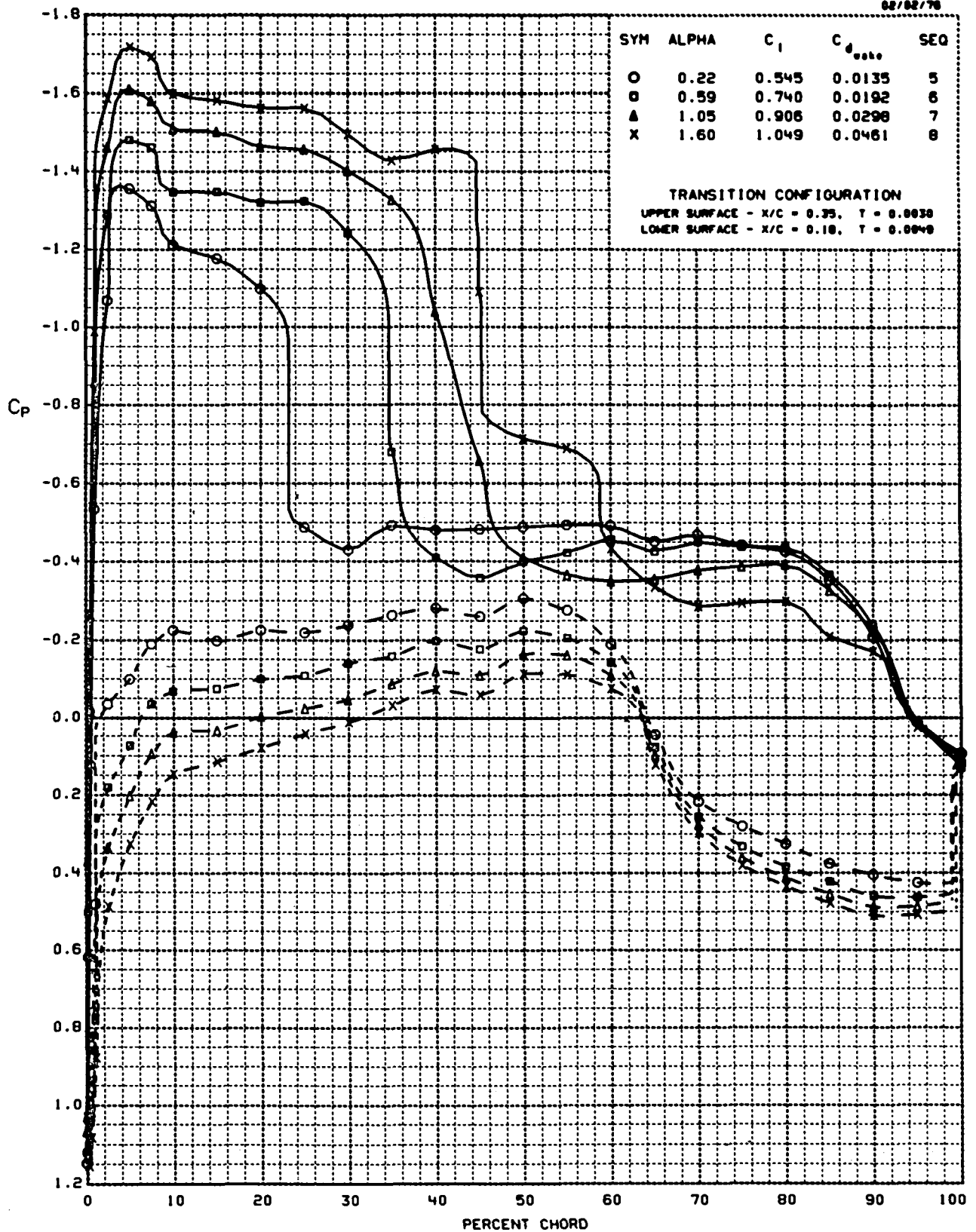
02/02/78



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

MACH NUMBER = 0.738      REYNOLDS NUMBER =  $3.92 \times 10^6$       RUN = 92      AMES 22-060-5

02/02/78



# WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

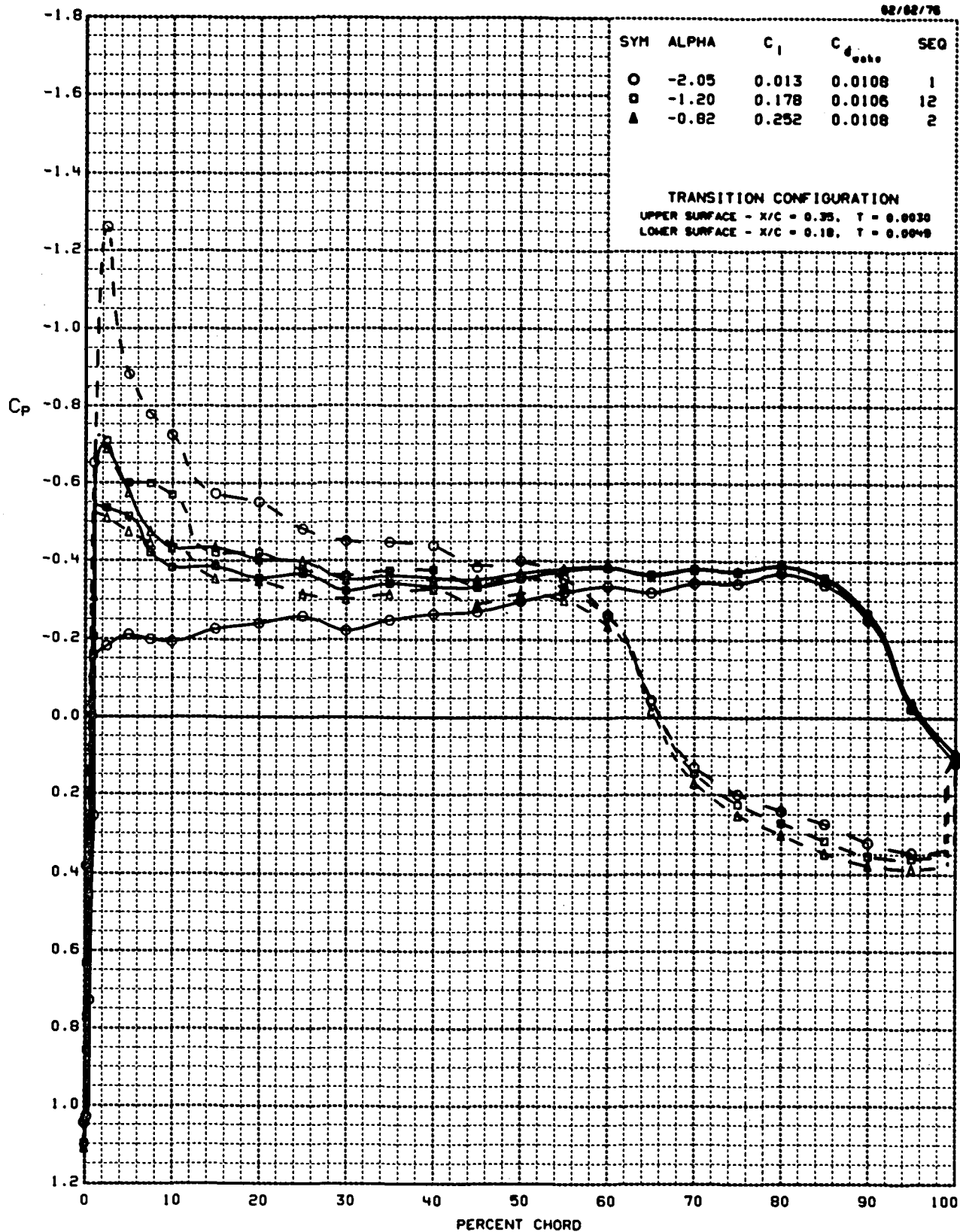
MACH NUMBER = 0.599

REYNOLDS NUMBER =  $4.02 \times 10^6$

RUN = 93

AMES 22-060-5

02/02/78



# WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

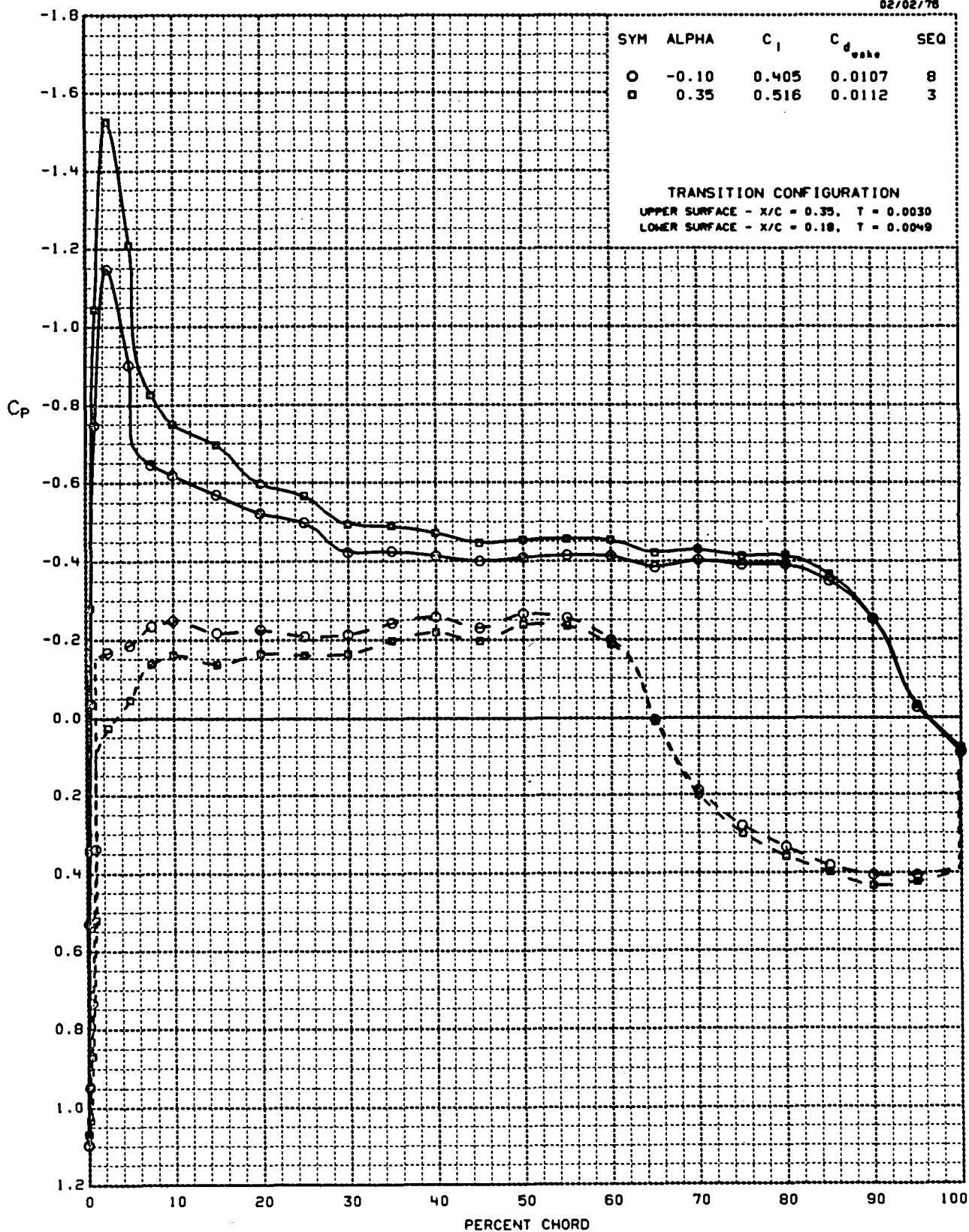
MACH NUMBER = 0.601

REYNOLDS NUMBER =  $4.02 \times 10^6$

RUN = 93

AMES 22-060-5

02/02/78



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

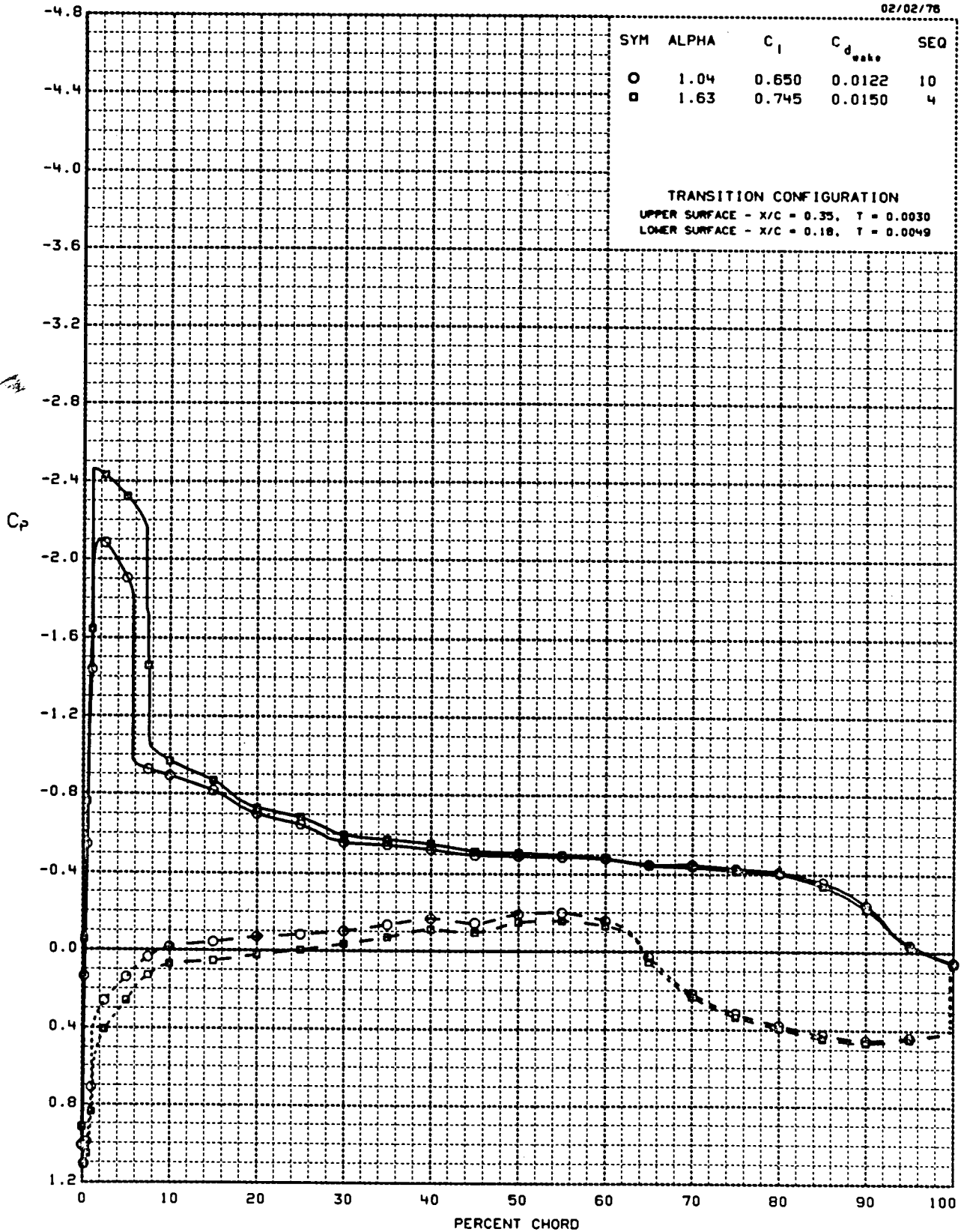
MACH NUMBER = 0.597

REYNOLDS NUMBER =  $4.01 \times 10^6$

RUN = 93

AMES 22-060-5

02/02/76





WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

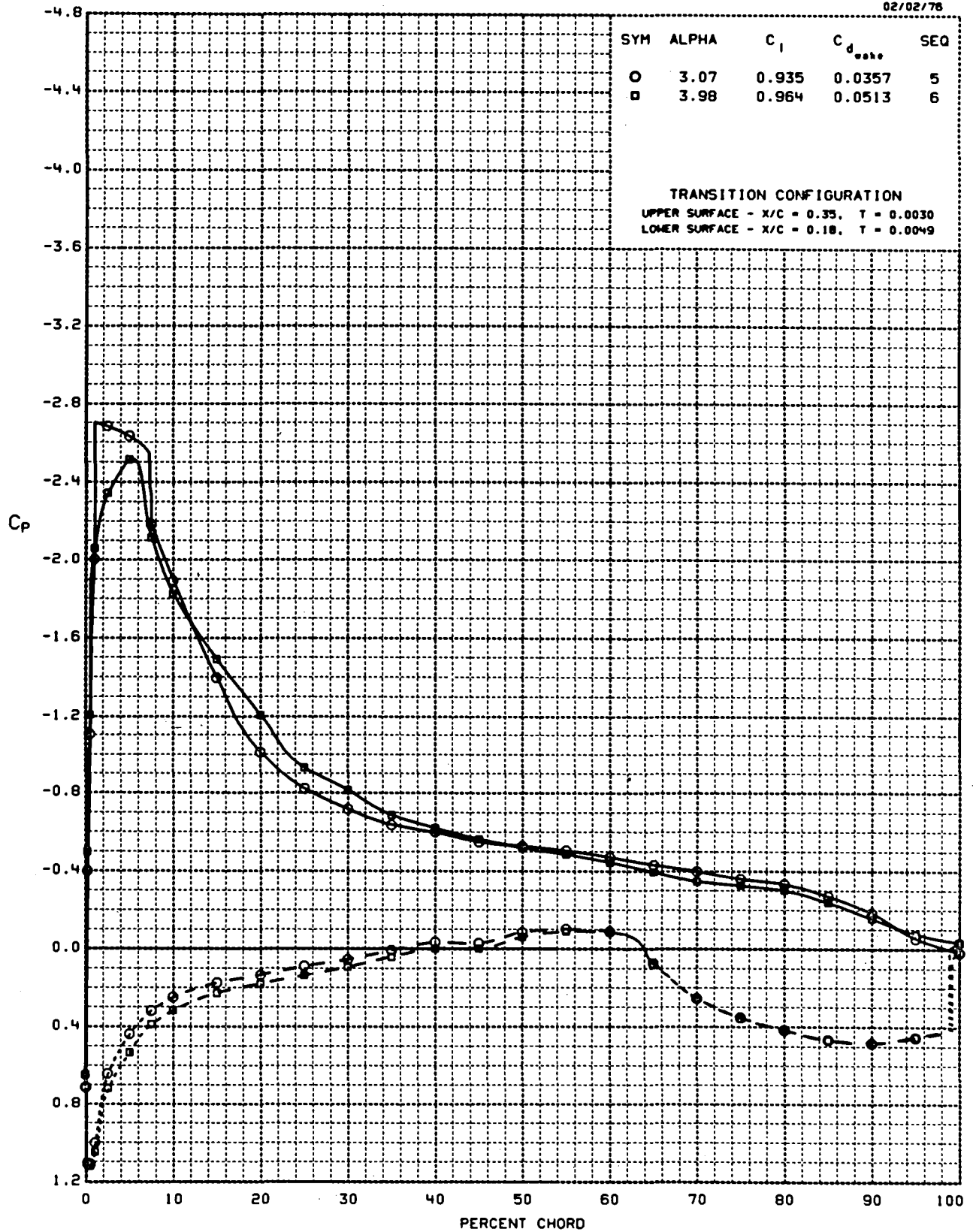
MACH NUMBER = 0.600

REYNOLDS NUMBER =  $4.00 \times 10^6$

RUN = 93

AMES 22-060-5

02/02/78





WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

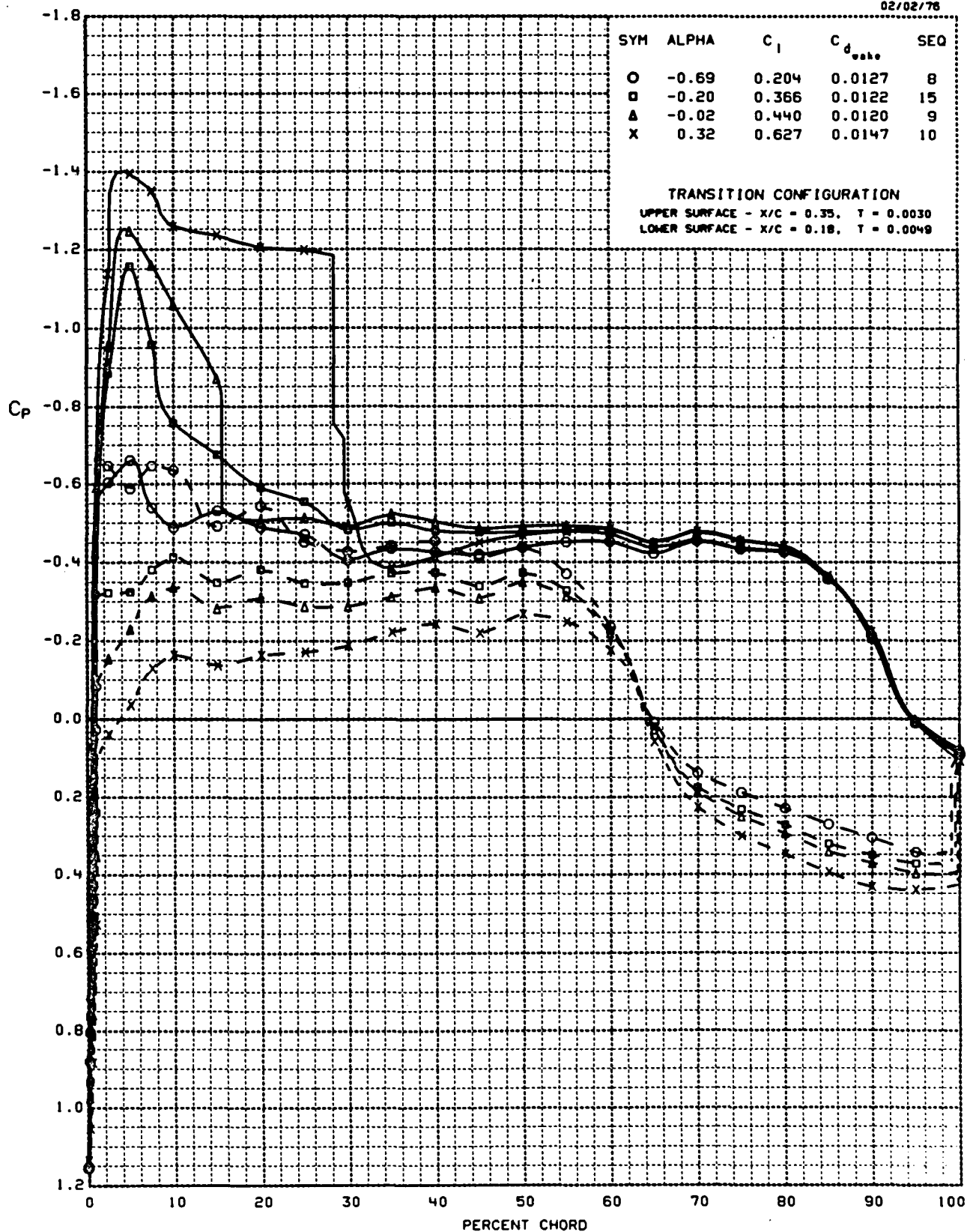
MACH NUMBER = 0.740

REYNOLDS NUMBER =  $3.98 \times 10^6$

RUN = 94

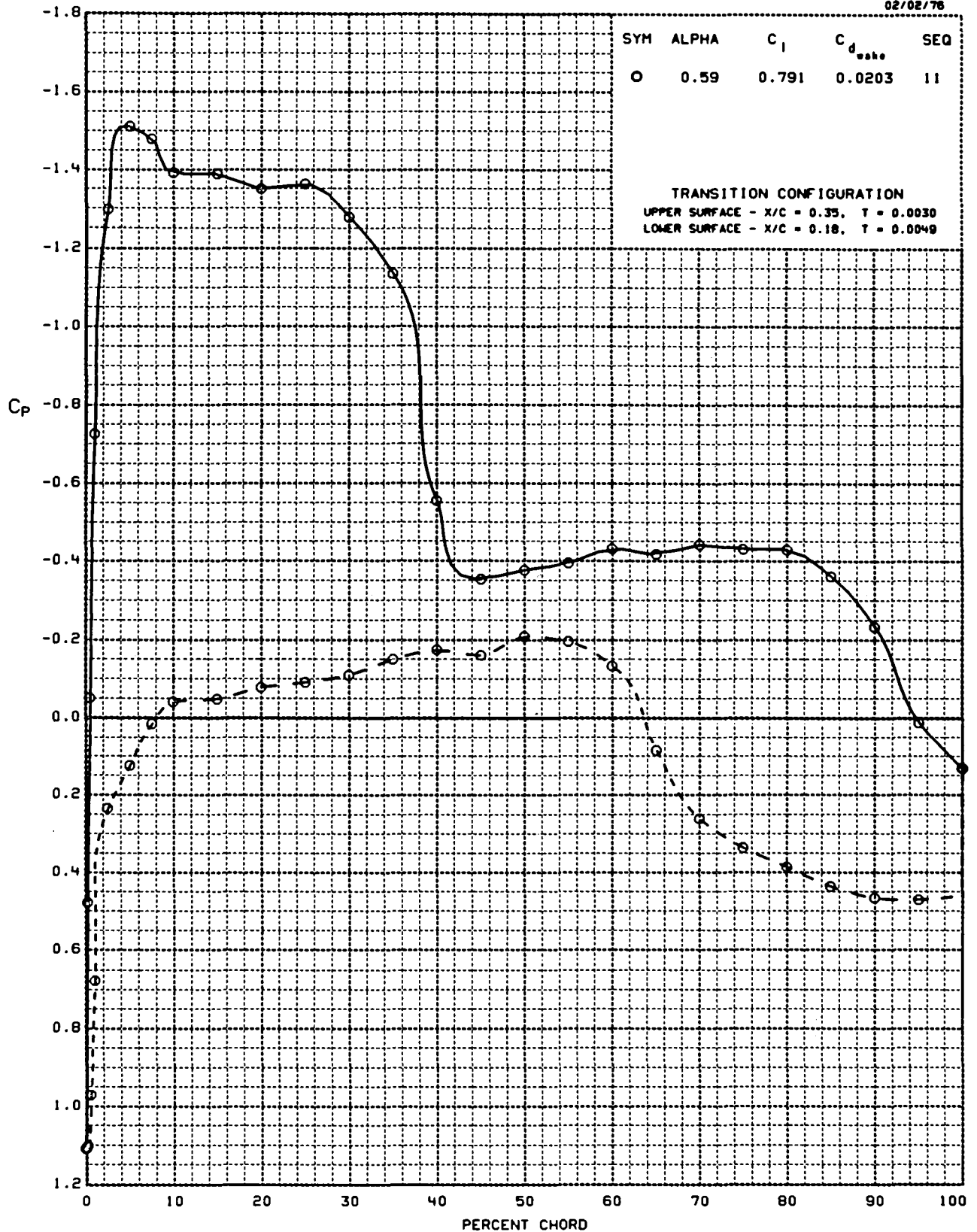
AMES 22-060-5

02/02/78



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS  
 MACH NUMBER = 0.741 REYNOLDS NUMBER =  $3.95 \times 10^6$  RUN = 94 AMES 22-060-5

02/02/76



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

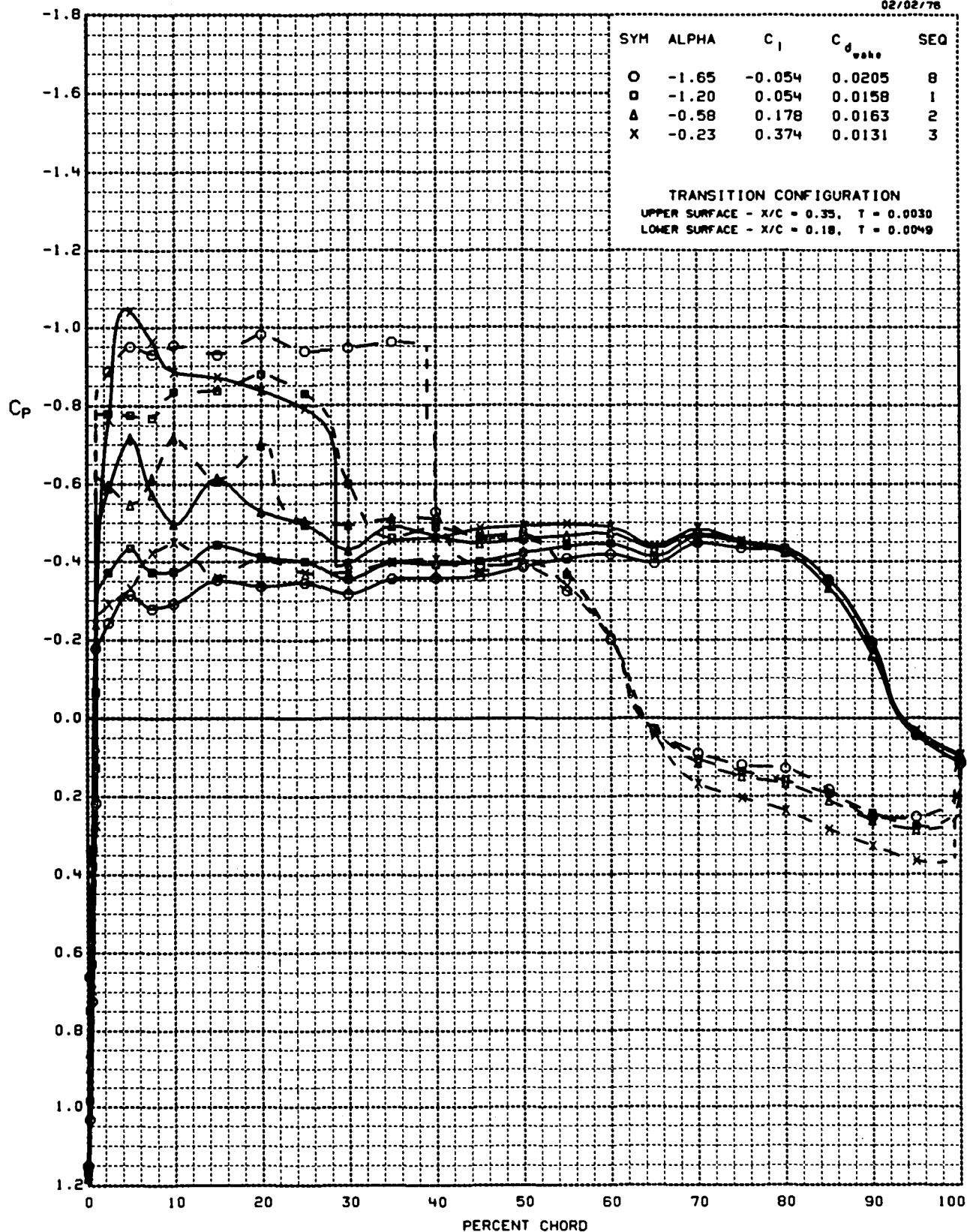
MACH NUMBER = 0.778

REYNOLDS NUMBER =  $2.98 \times 10^6$

RUN = 95

AMES 22-060-5

02/02/78



# WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

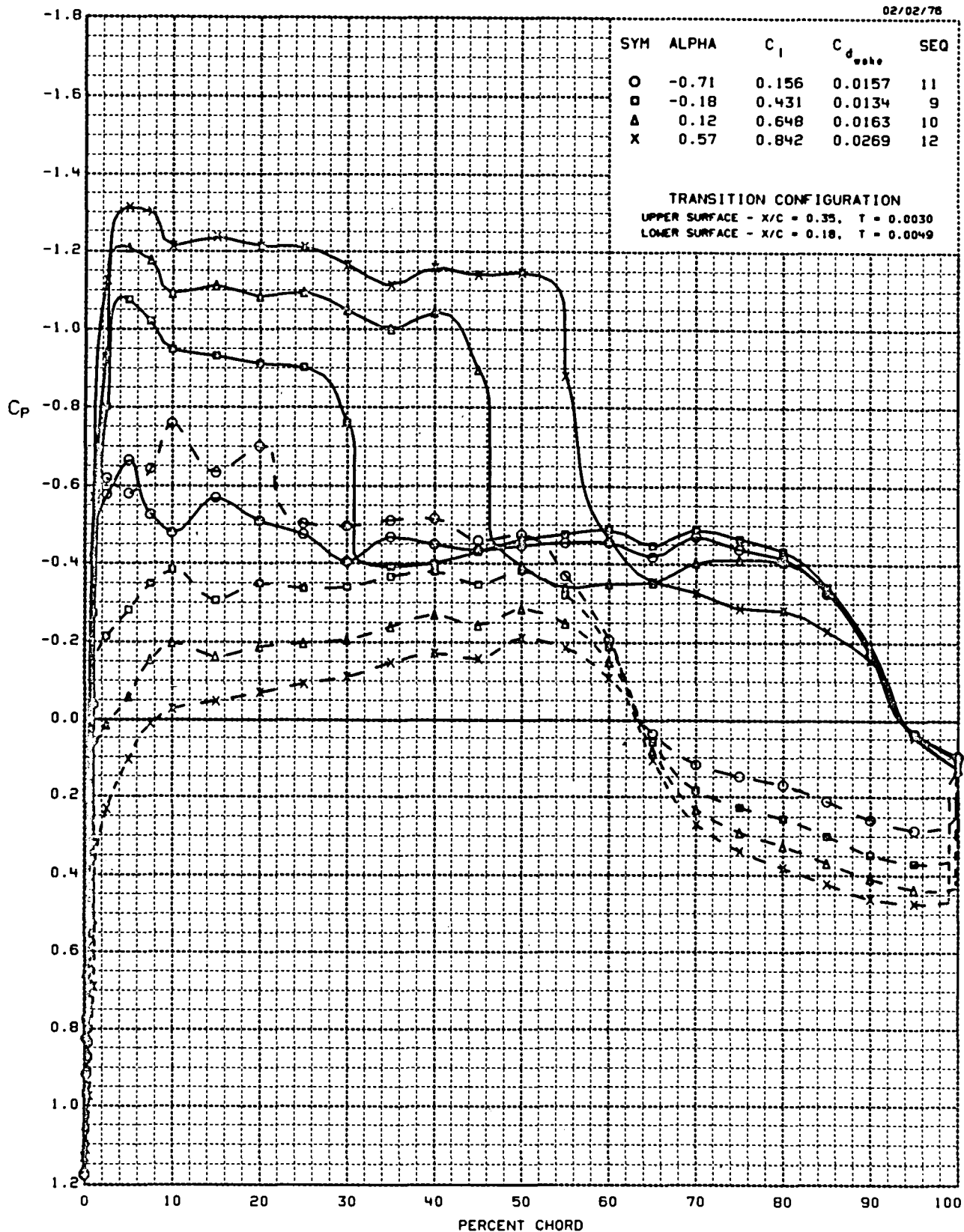
MACH NUMBER = 0.777

REYNOLDS NUMBER =  $2.96 \times 10^6$

RUN = 95

AMES 22-060-5

02/02/78



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

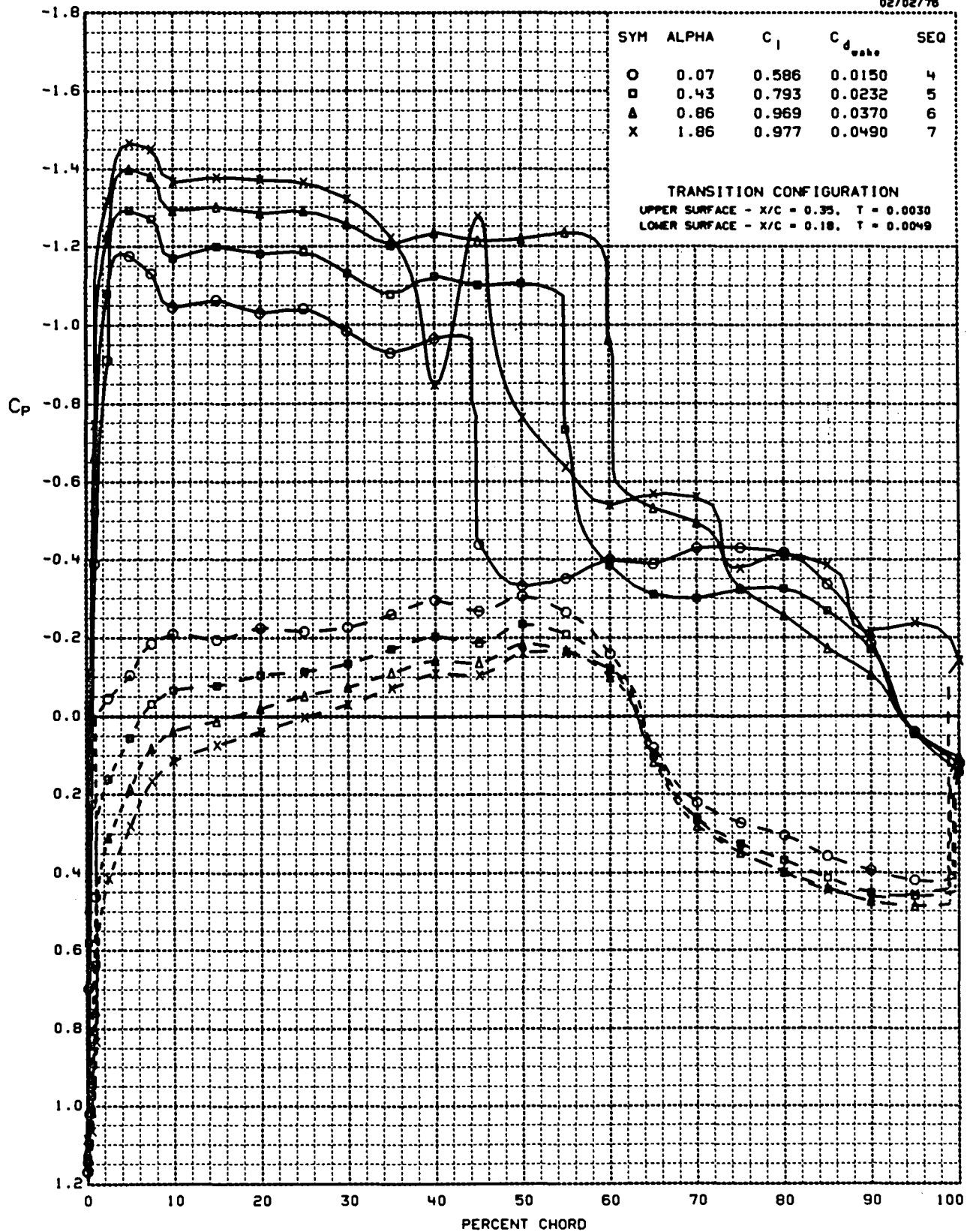
MACH NUMBER = 0.778

REYNOLDS NUMBER =  $2.95 \times 10^6$

RUN = 95

AMES 22-060-5

02/02/76



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

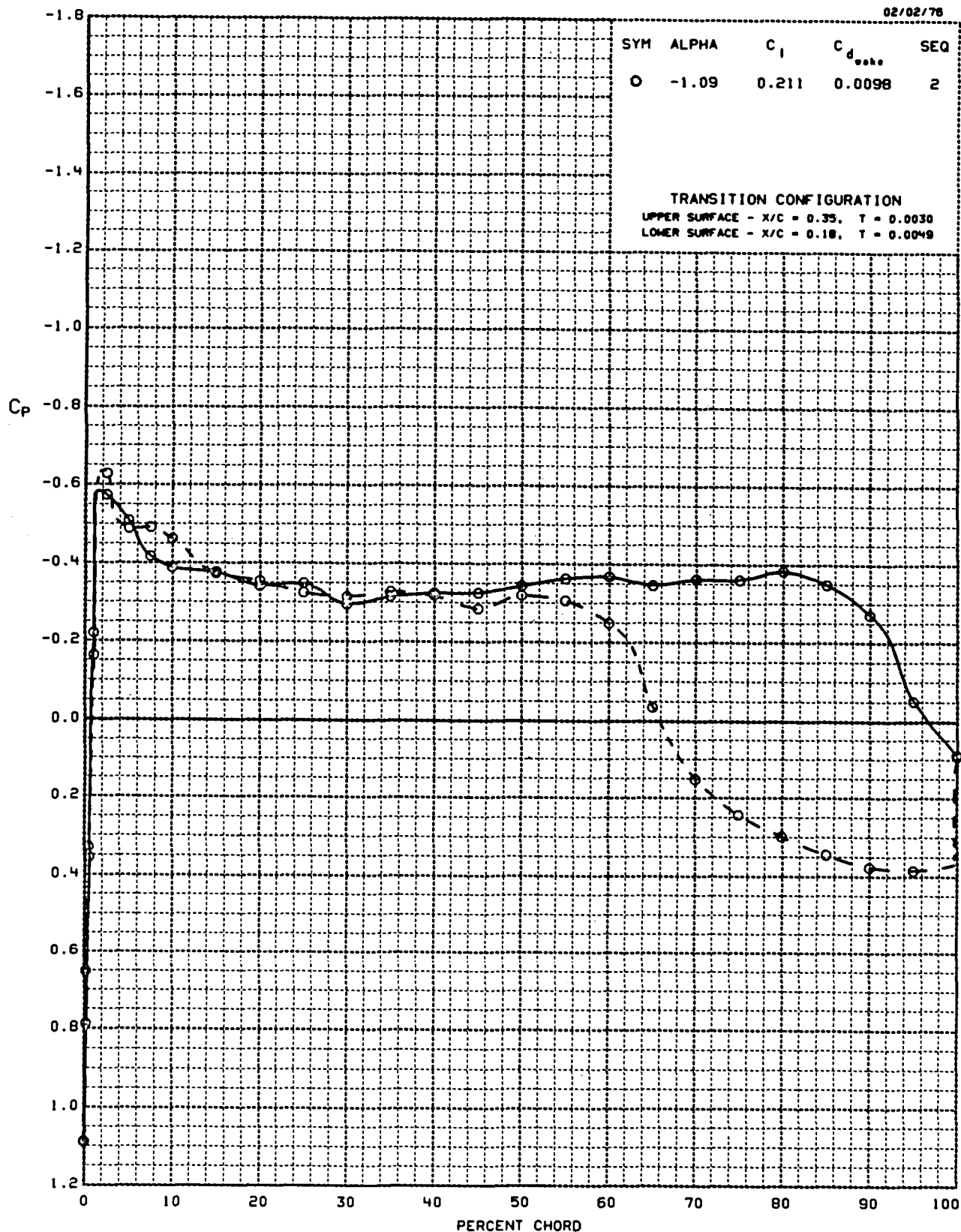
MACH NUMBER = 0.500

REYNOLDS NUMBER =  $4.05 \times 10^6$

RUN = 97

AMES 22-060-5

02/02/78



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

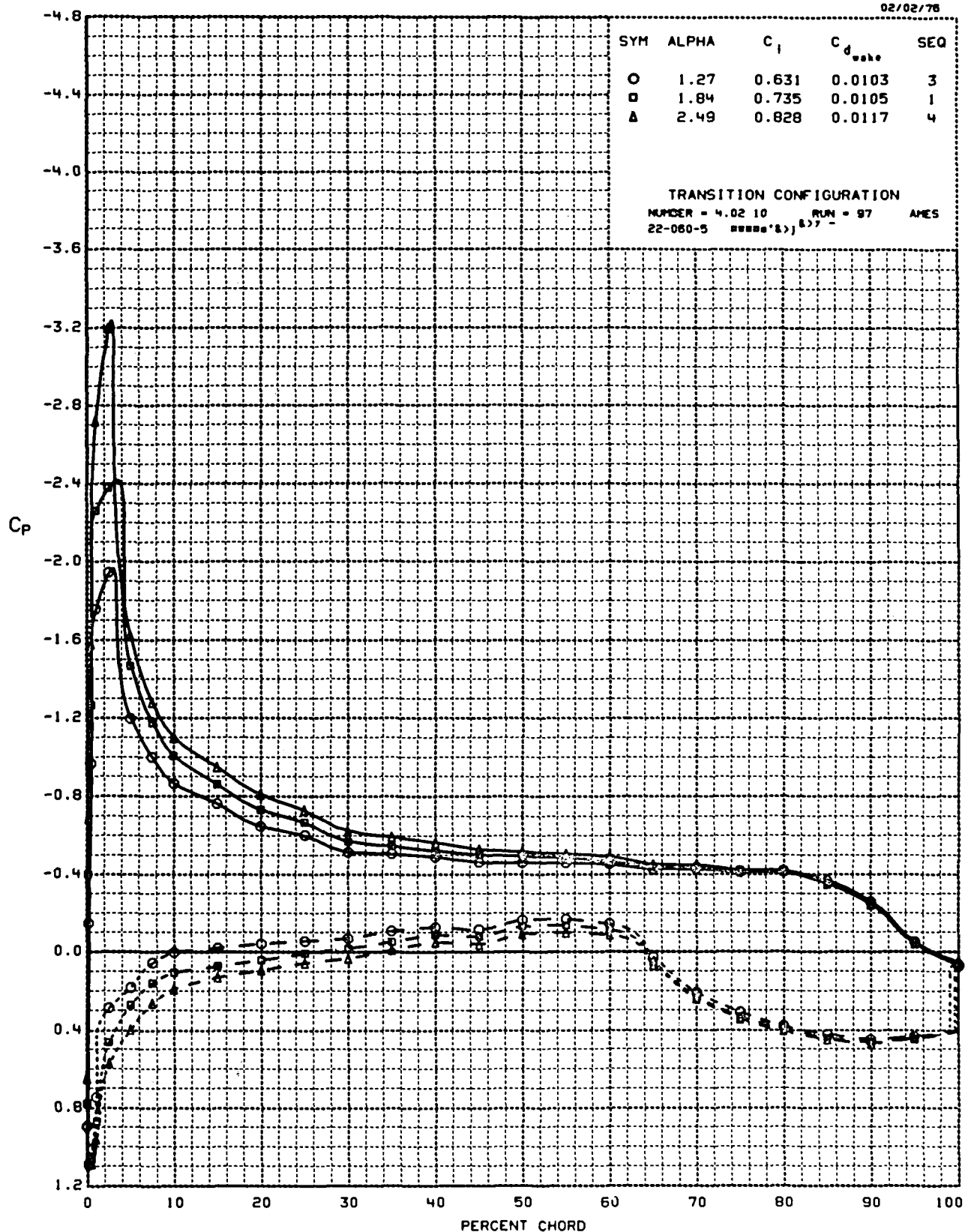
MACH NUMBER = 0.500

REYNOLDS NUMBER =  $4.02 \times 10^6$

RUN = 97

AMES 22-060-5

02/02/76



# WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

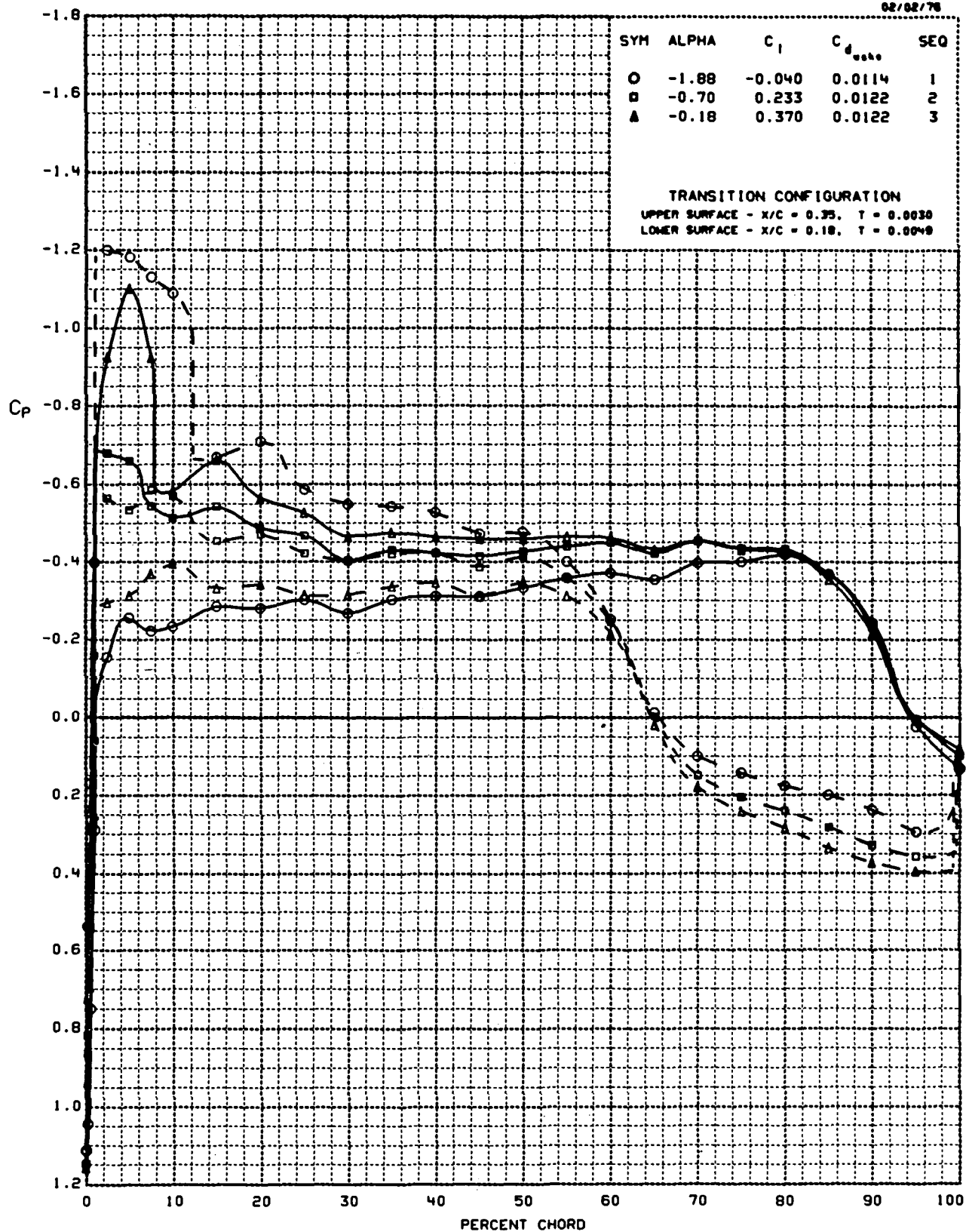
MACH NUMBER = 0.720

REYNOLDS NUMBER =  $3.91 \times 10^6$

RUN = 98

AMES 22-060-5

02/02/76





WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

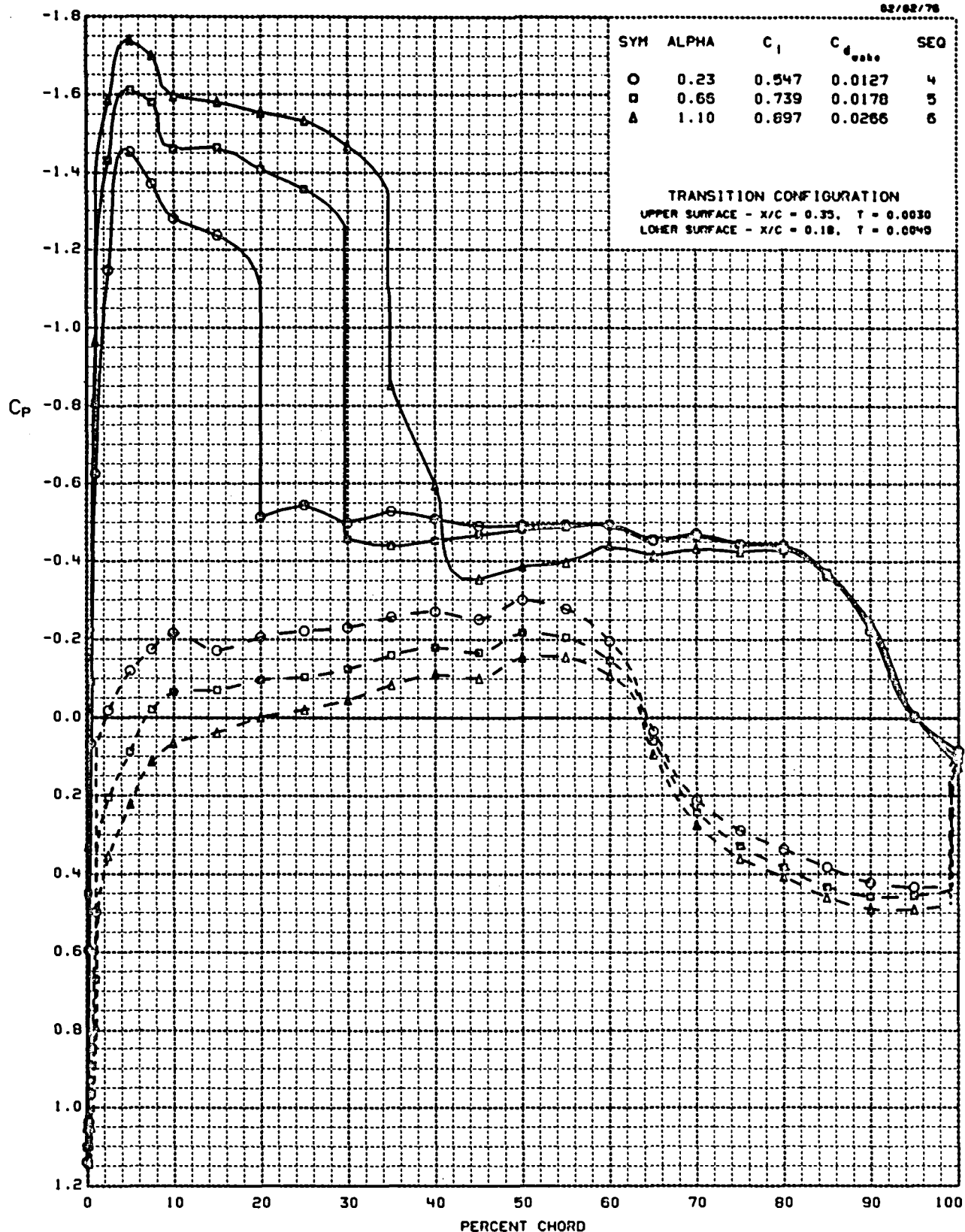
MACH NUMBER = 0.719

REYNOLDS NUMBER =  $3.98 \times 10^6$

RUN = 93

AMES 22-000-5

02/02/78



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

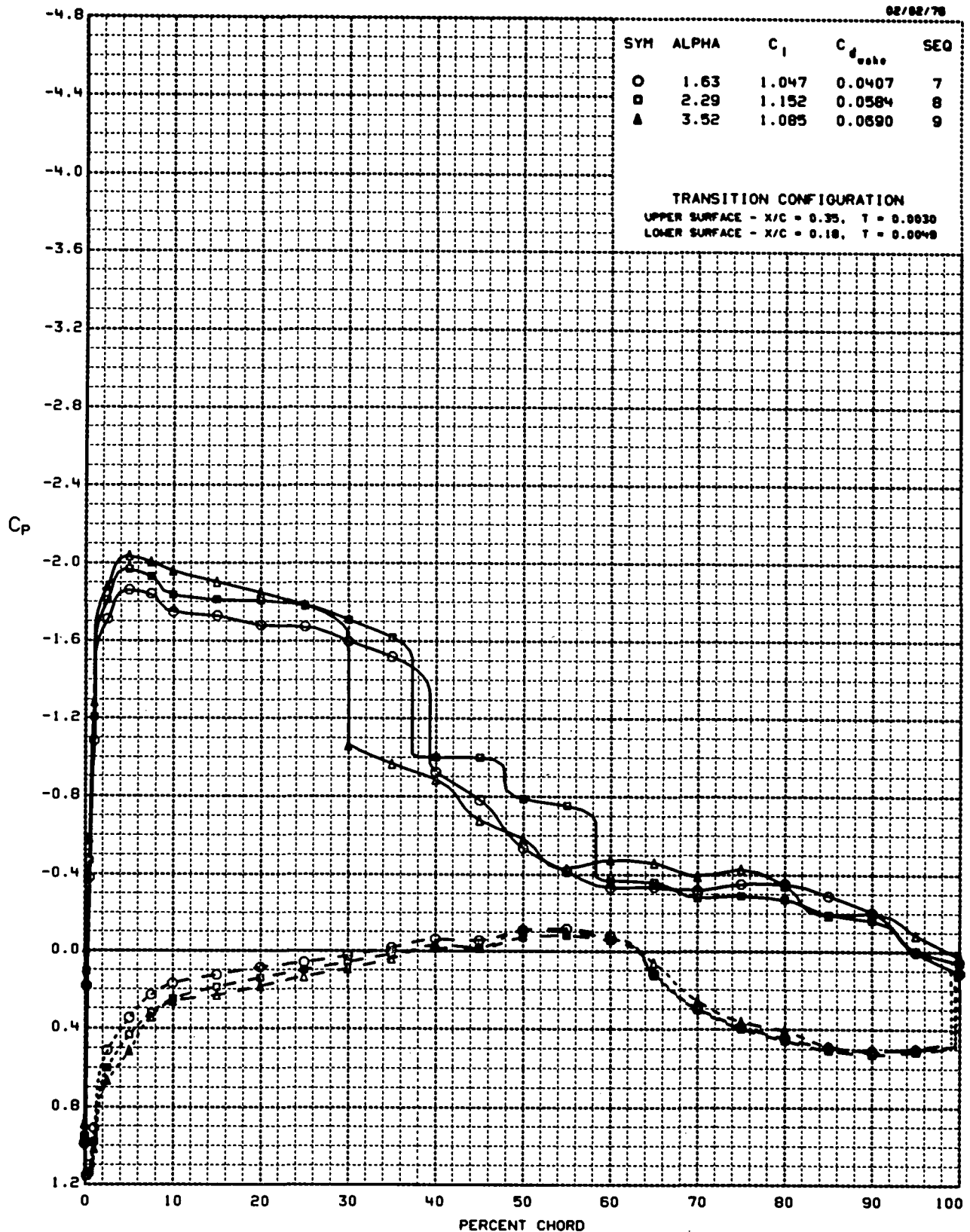
MACH NUMBER = 0.718

REYNOLDS NUMBER =  $3.95 \times 10^6$

RUN = 98

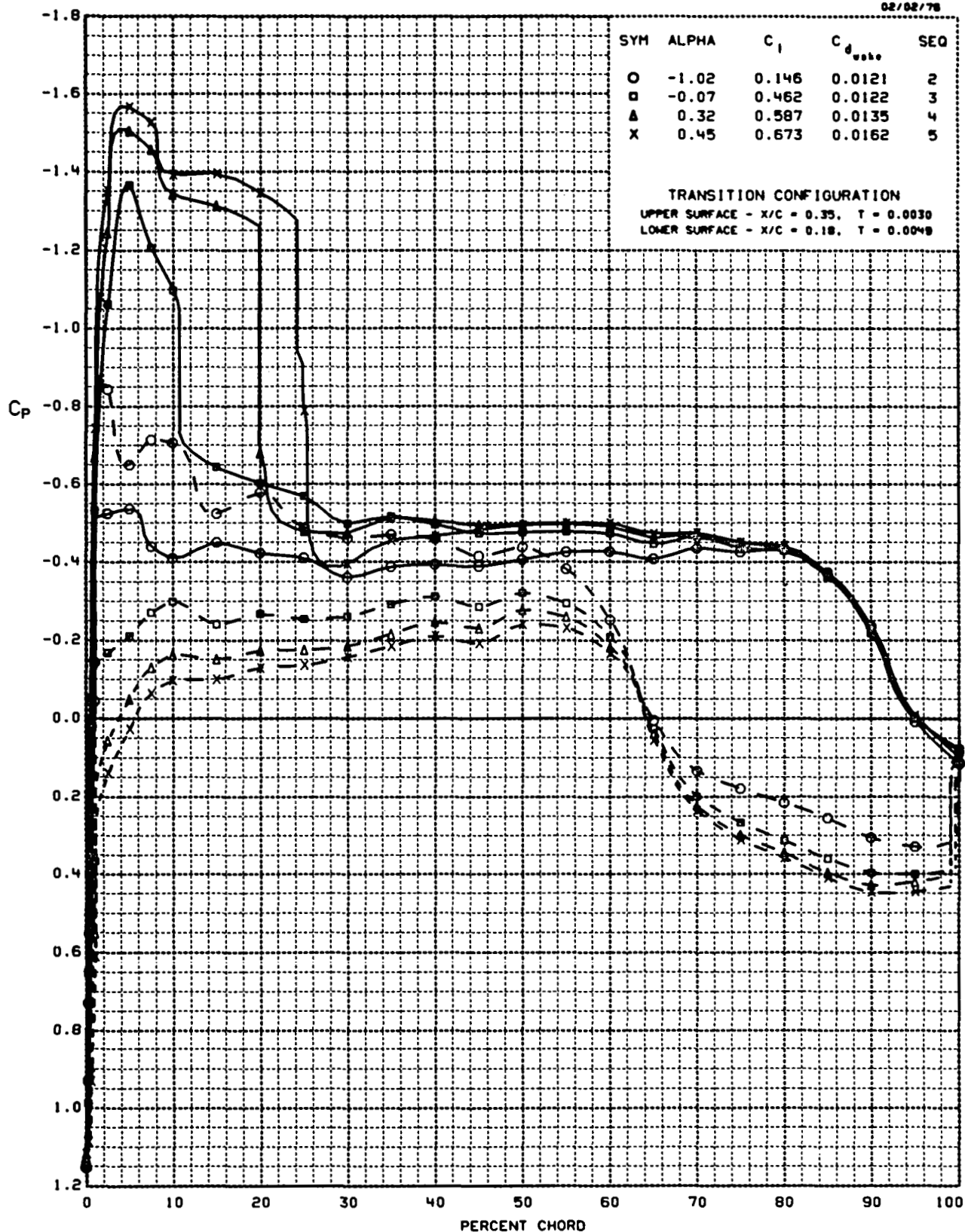
AMES 22-060-5

02/02/78



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS  
 MACH NUMBER = 0.719 REYNOLDS NUMBER =  $3.95 \times 10^6$  RUN = 99 AMES 22-060-5

02/02/78



# WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

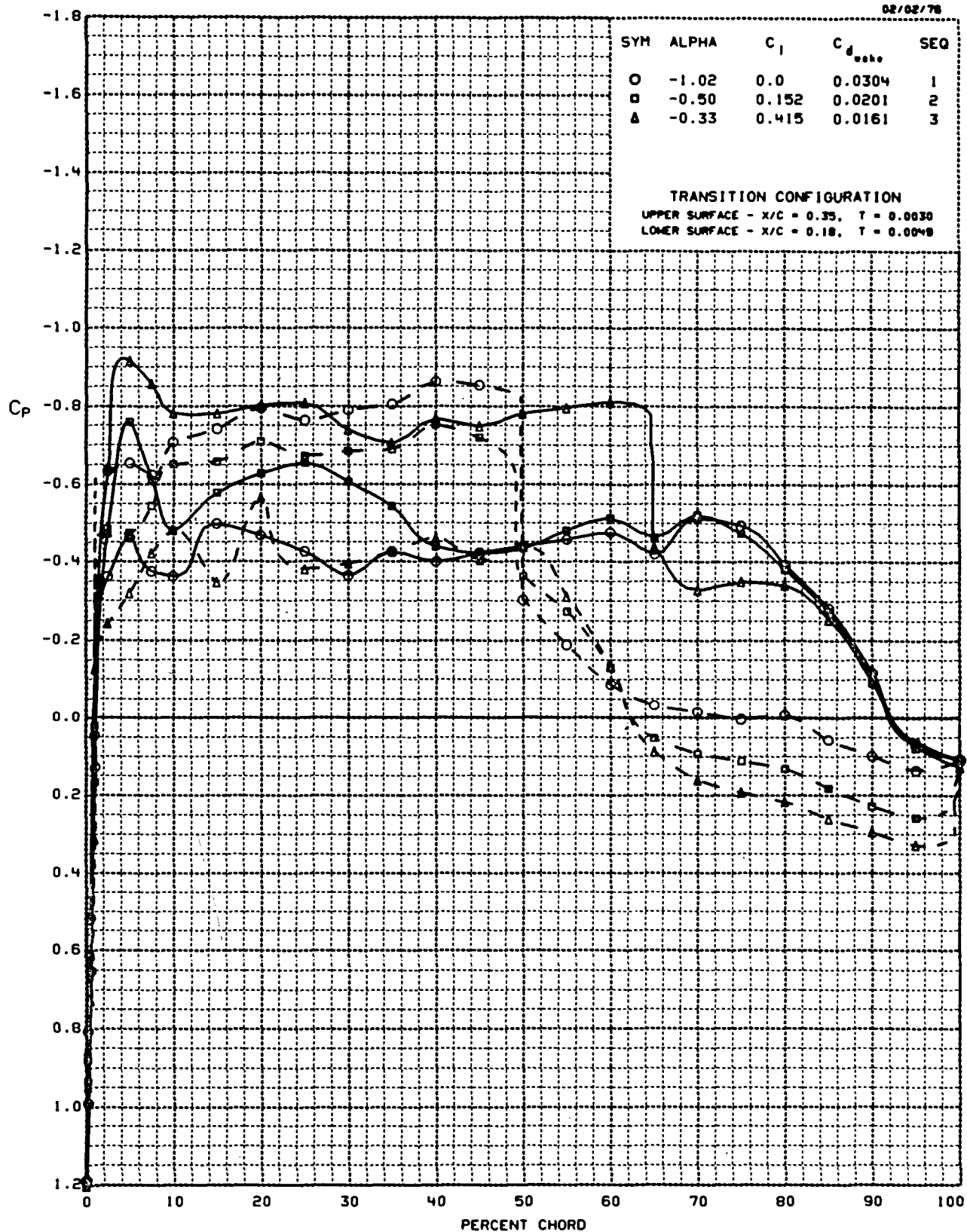
MACH NUMBER = 0.820

REYNOLDS NUMBER =  $2.96 \times 10^6$

RUN = 100

AMES 22-060-5

02/02/76



# WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

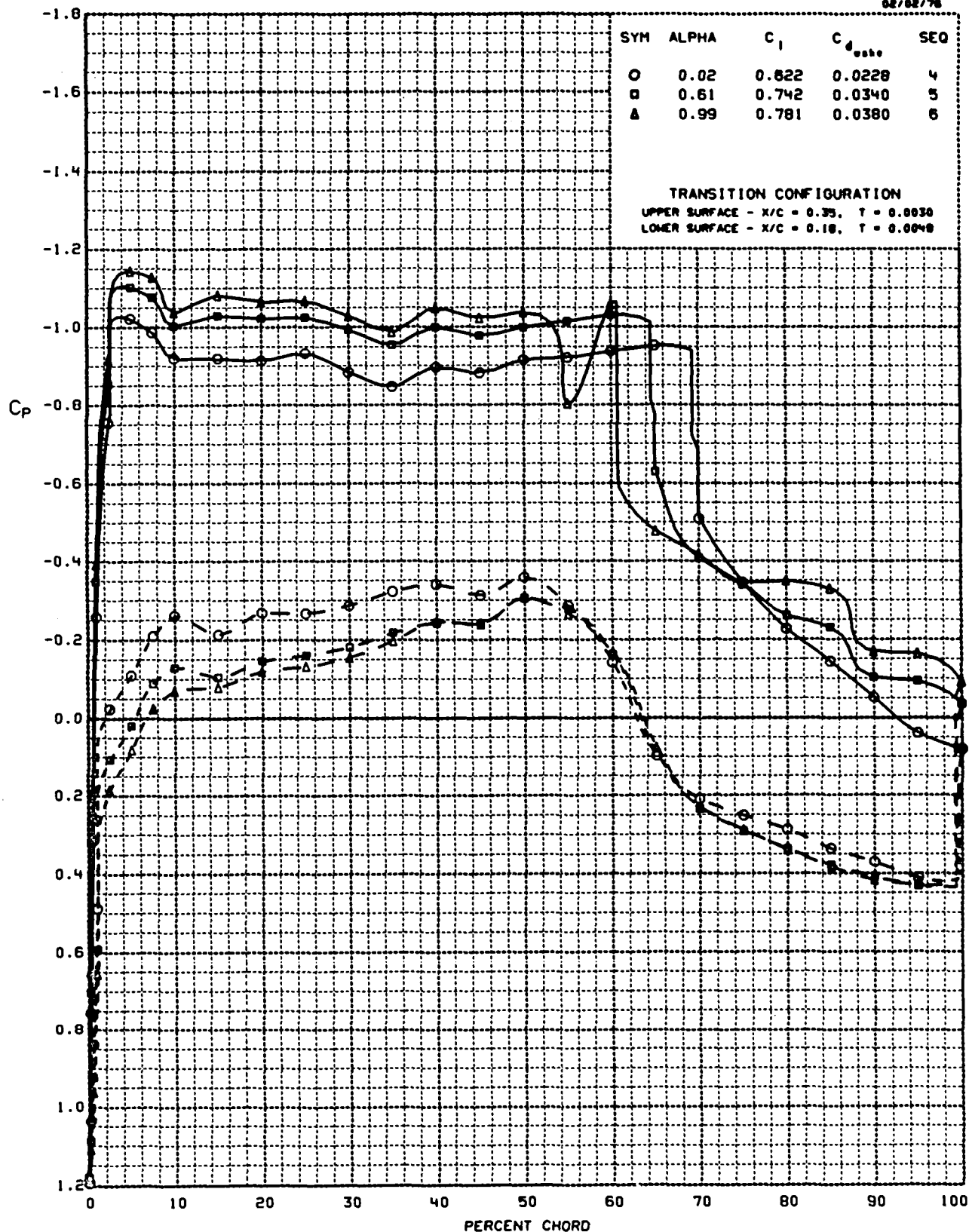
MACH NUMBER = 0.819

REYNOLDS NUMBER =  $2.96 \times 10^6$

RUN =100

AMES 22-060-5

02/02/78



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

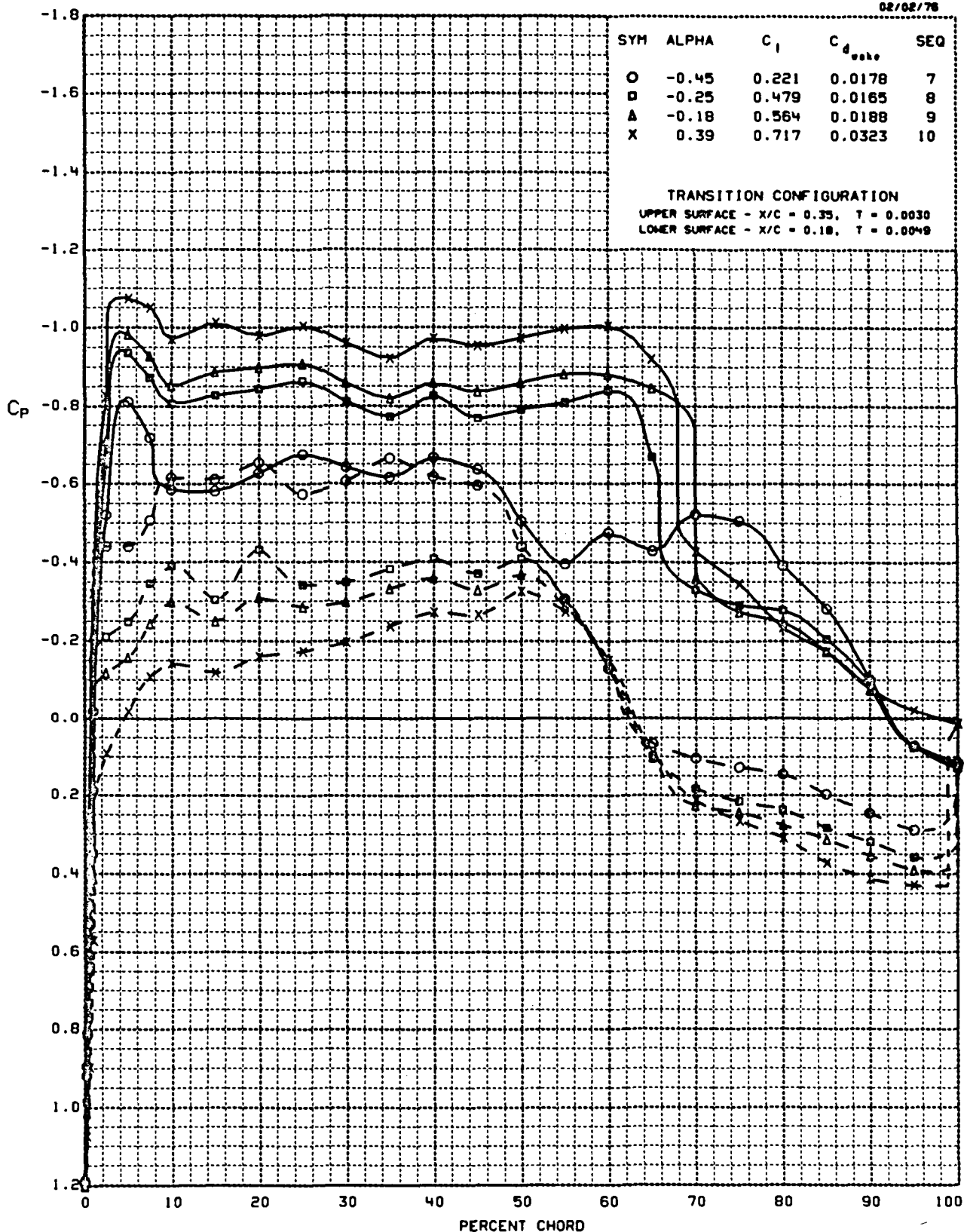
MACH NUMBER = 0.820

REYNOLDS NUMBER =  $2.99 \times 10^6$

RUN = 100

AMES 22-060-5

02/02/76



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

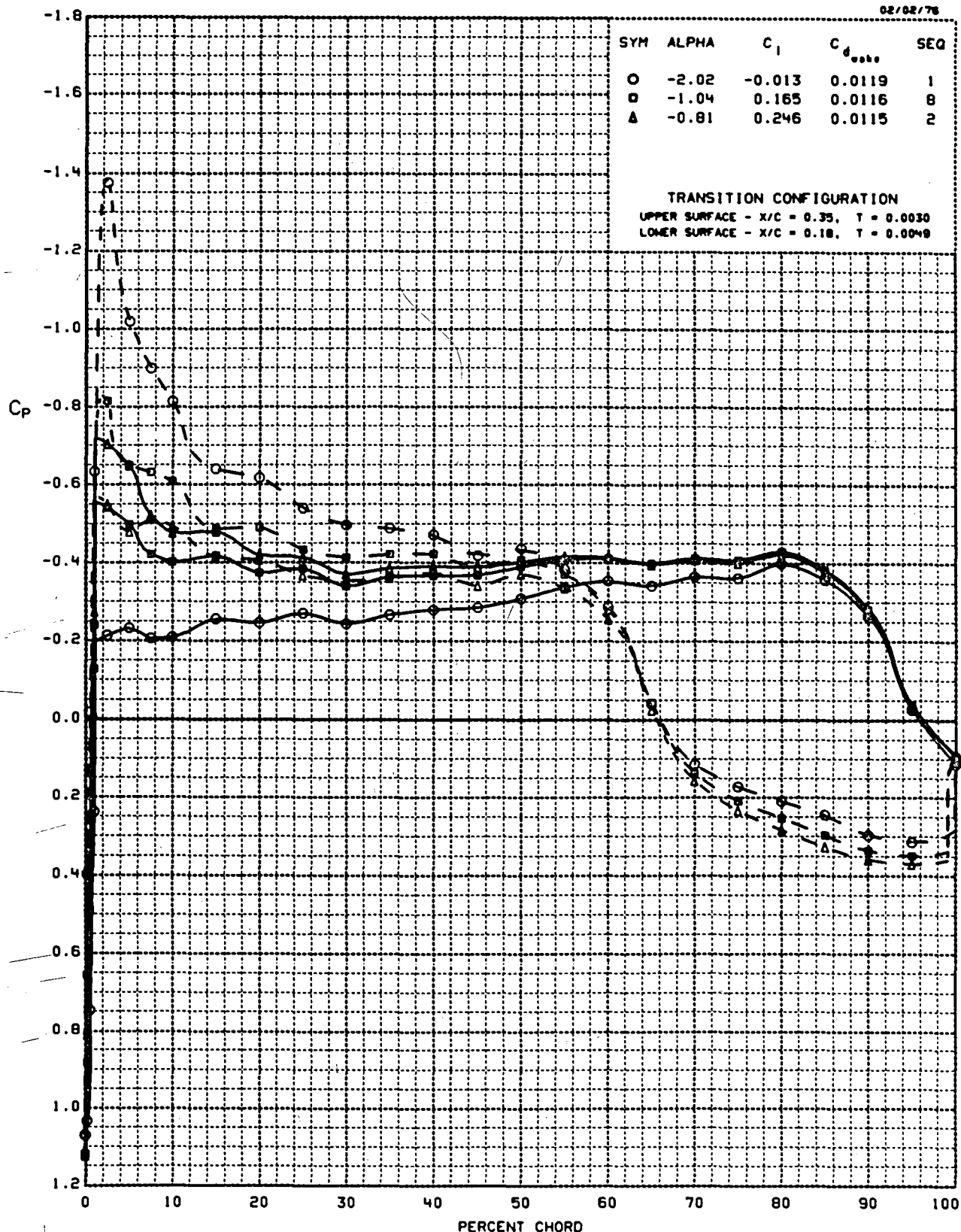
MACH NUMBER = 0.639

REYNOLDS NUMBER =  $4.01 \times 10^6$

RUN -101

AMES 22-060-5

02/02/78





WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

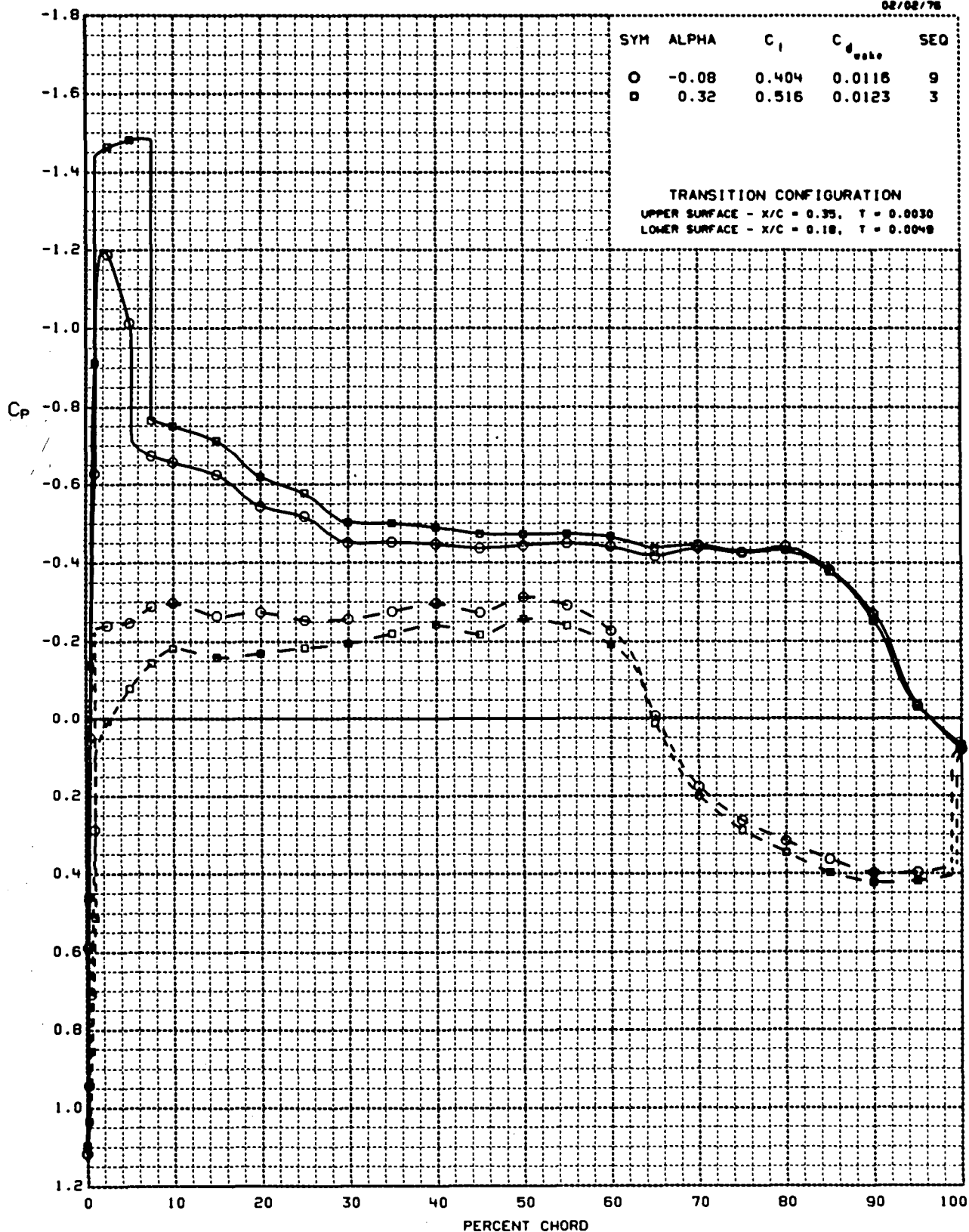
MACH NUMBER = 0.639

REYNOLDS NUMBER =  $4.00 \times 10^6$

RUN =101

AMES 22-060-5

02/02/76





# WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

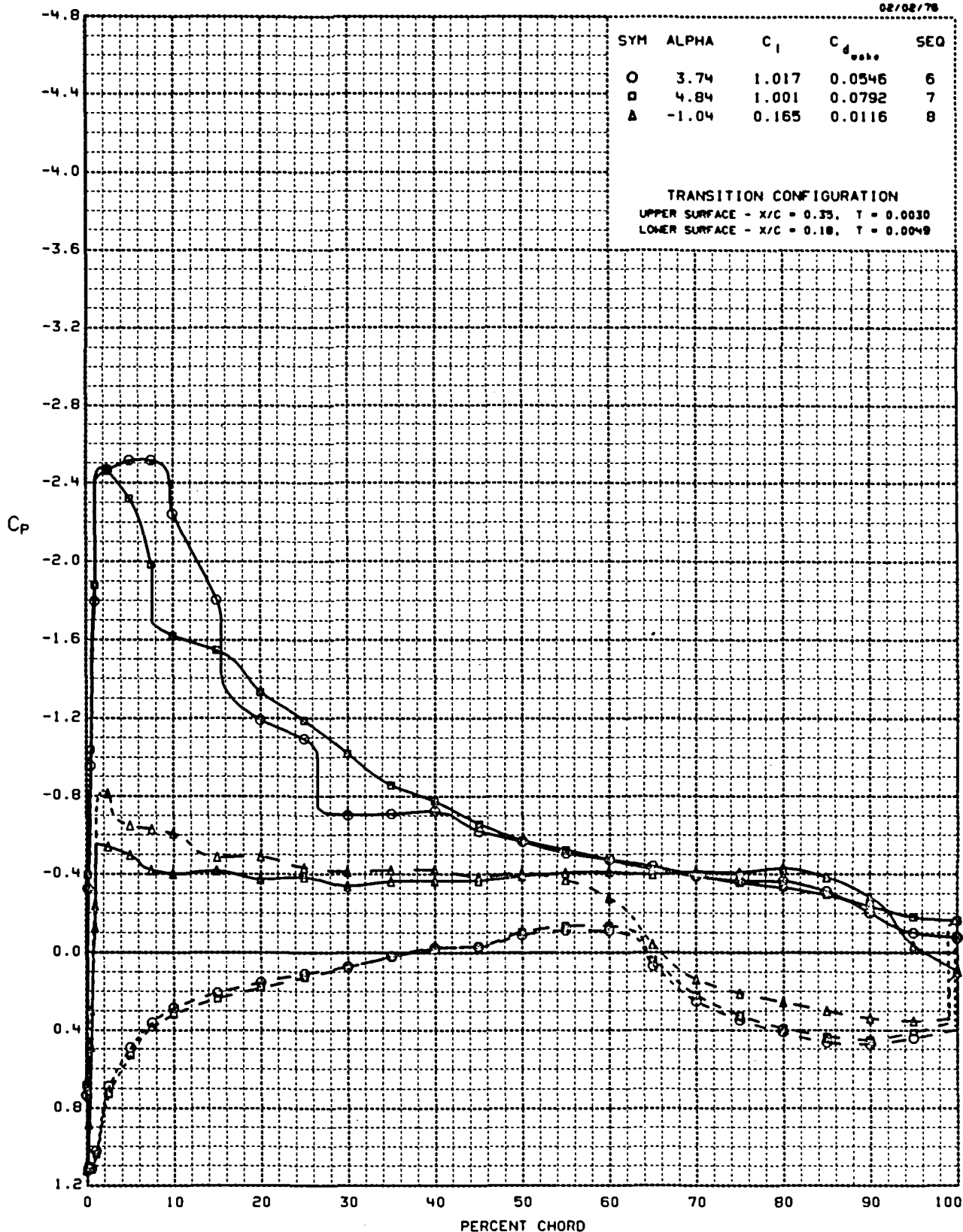
MACH NUMBER = 0.639

REYNOLDS NUMBER =  $3.95 \times 10^6$

RUN -101

AMES 22-060-5

02/02/78



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

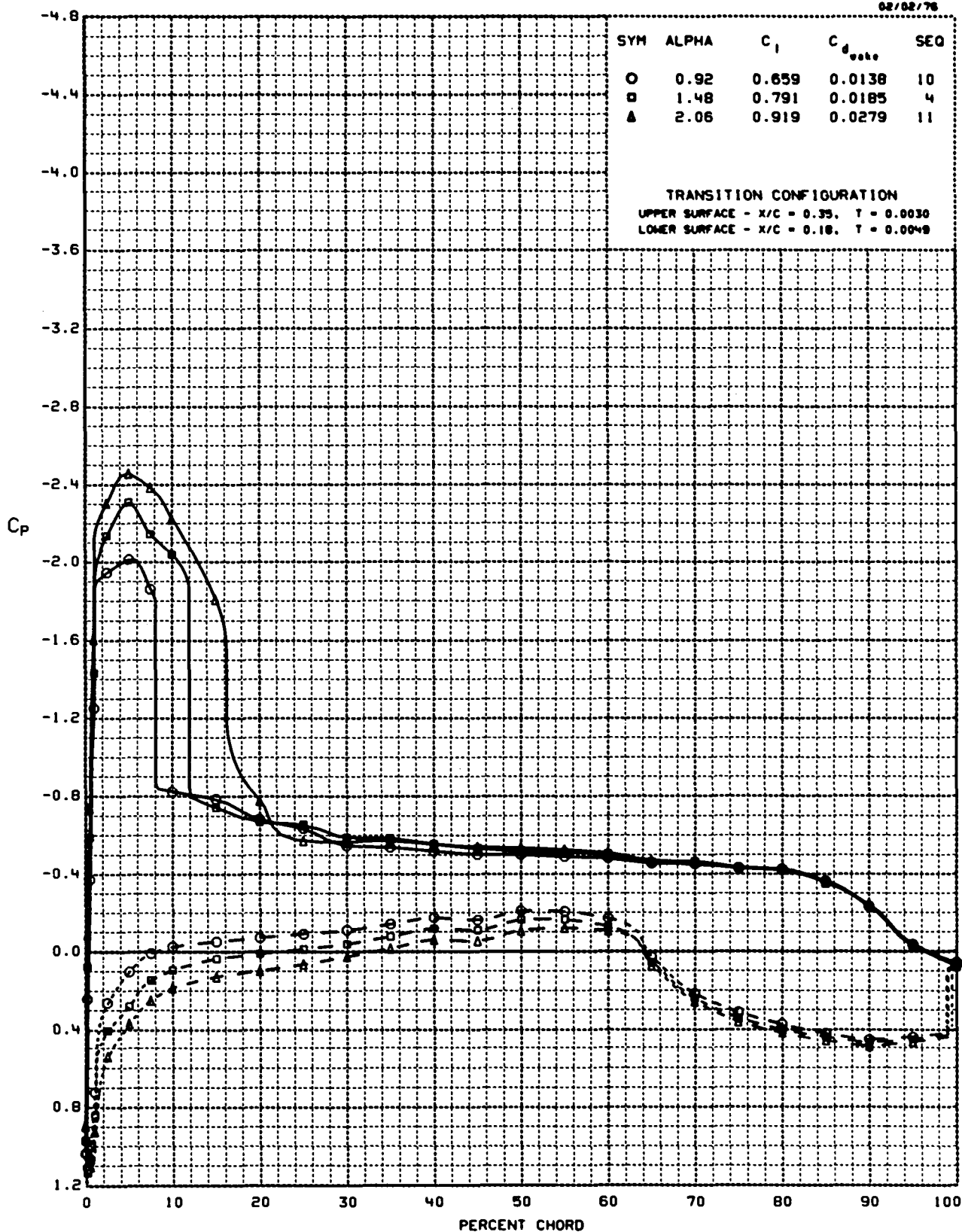
MACH NUMBER = 0.639

REYNOLDS NUMBER =  $3.97 \times 10^6$

RUN = 101

AMES 22-060-5

02/02/76



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

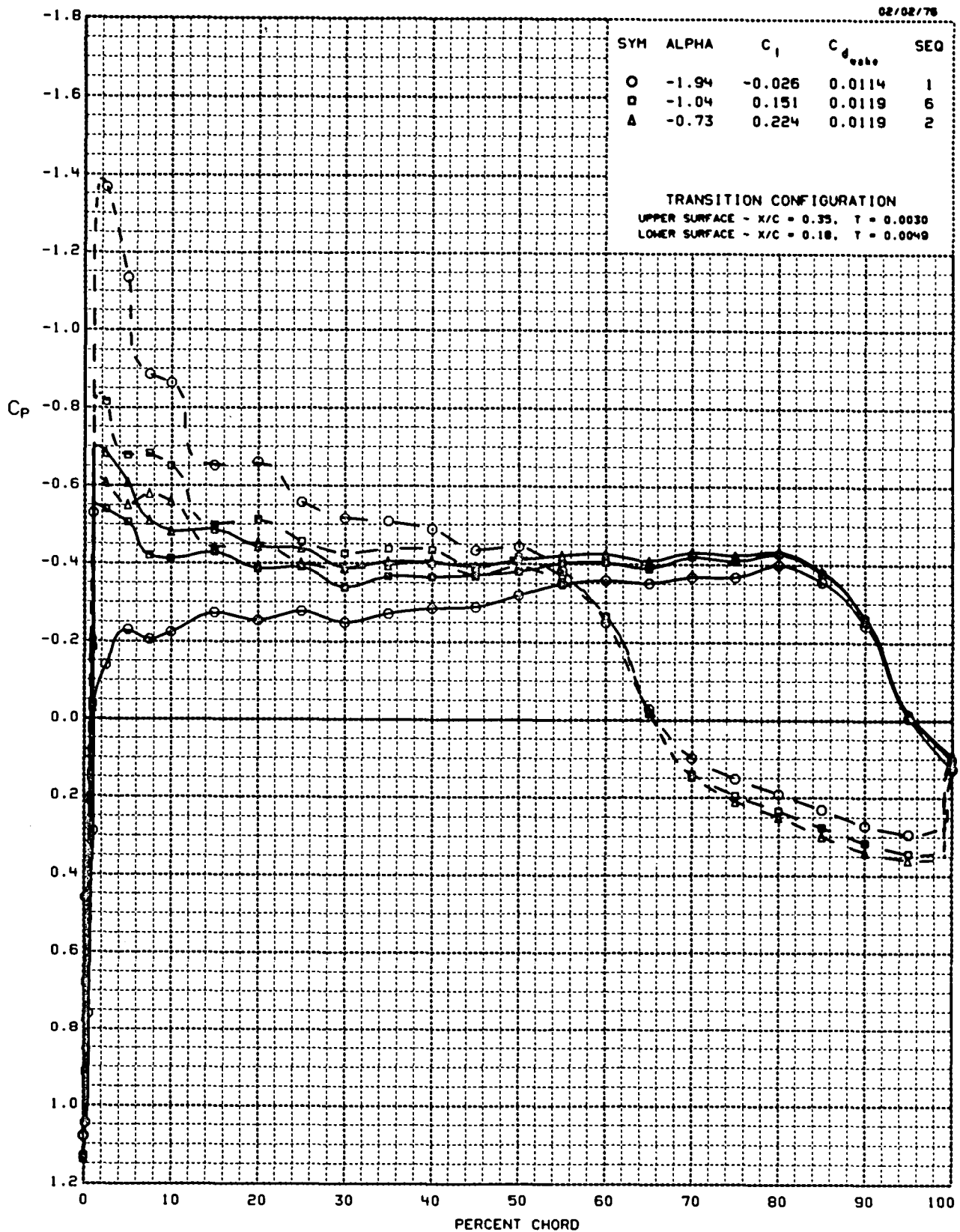
MACH NUMBER = 0.681

REYNOLDS NUMBER =  $3.97 \times 10^6$

RUN = 102

AMES 22-060-5

02/02/76



# WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

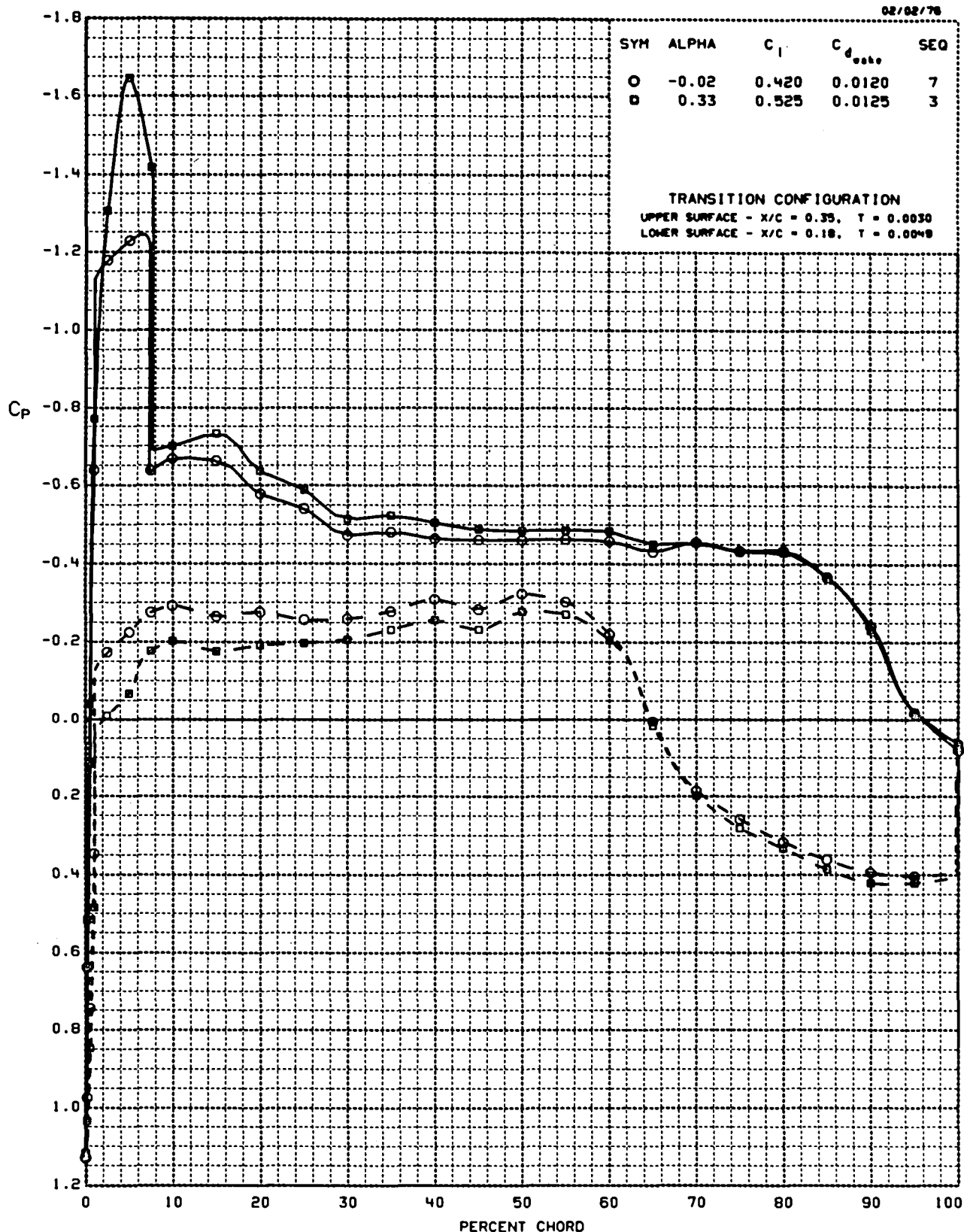
MACH NUMBER = 0.680

REYNOLDS NUMBER =  $3.94 \times 10^6$

RUN =102

AMES 22-060-5

02/02/78



# WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523

## TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

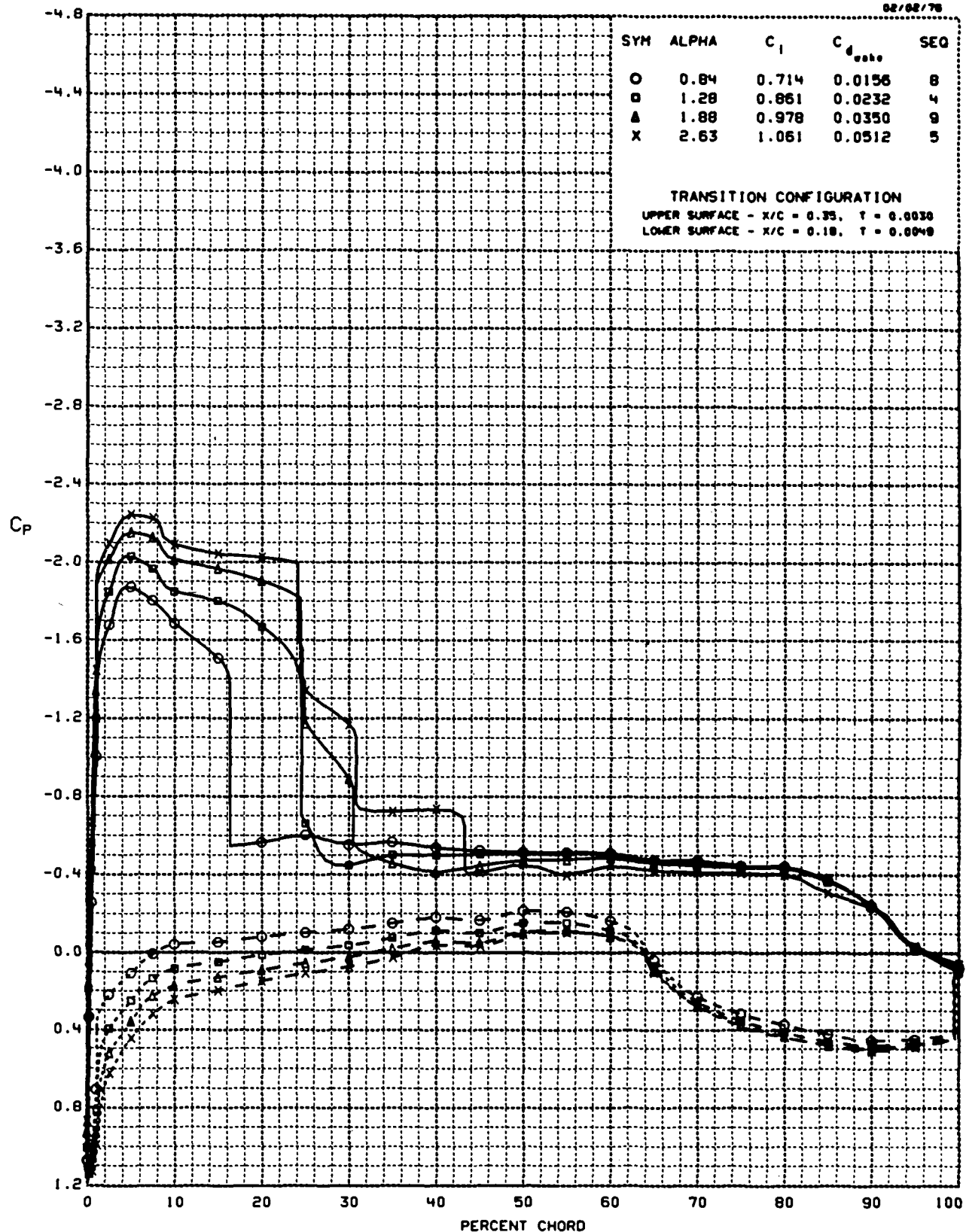
MACH NUMBER = 0.679

REYNOLDS NUMBER =  $3.94 \times 10^6$

RUN = 102

AMES 22-060-5

02/02/78



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

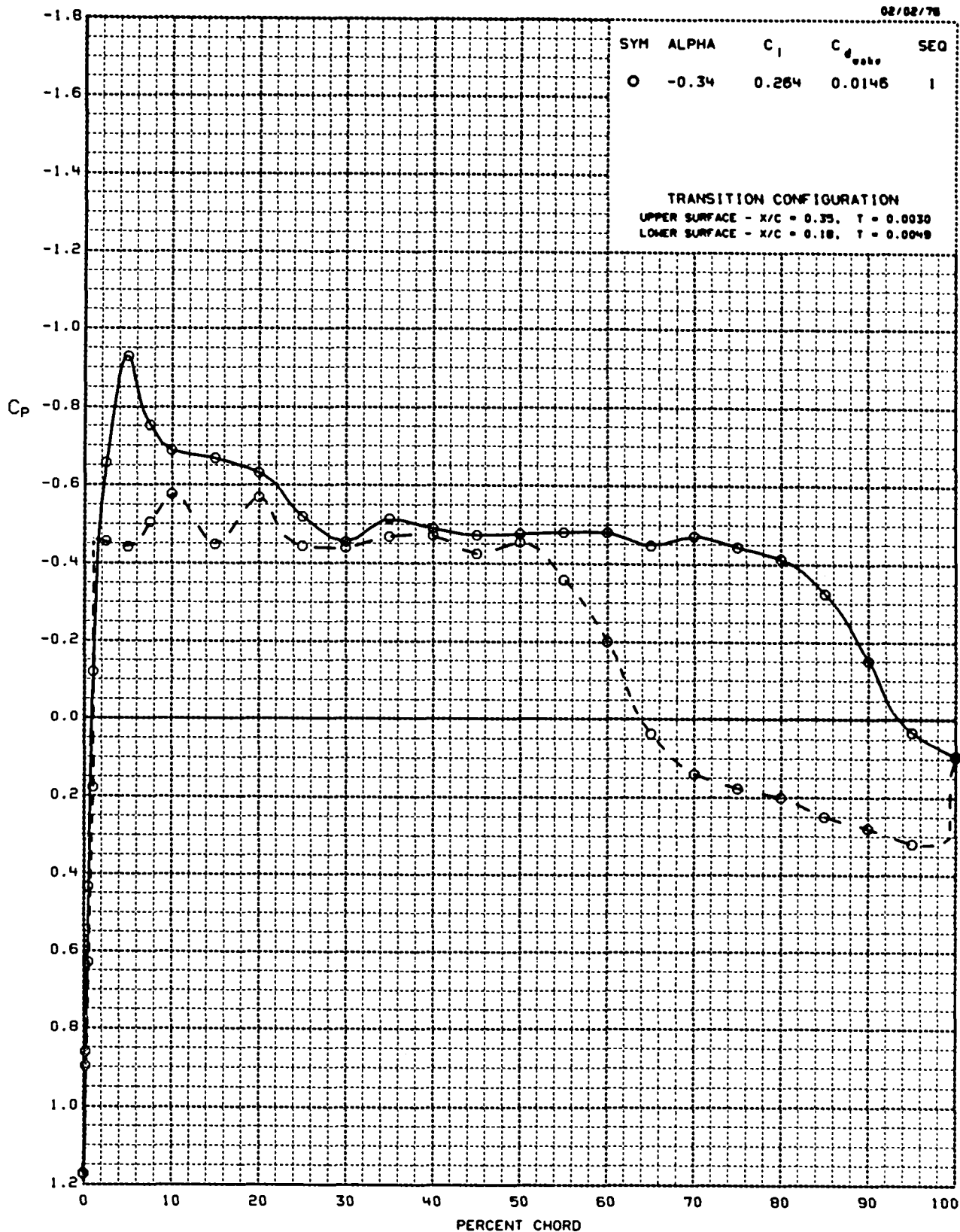
MACH NUMBER = 0.780

REYNOLDS NUMBER =  $2.95 \times 10^6$

RUN = 103

AMES 22-060-5

02/02/76



# WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523

## TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

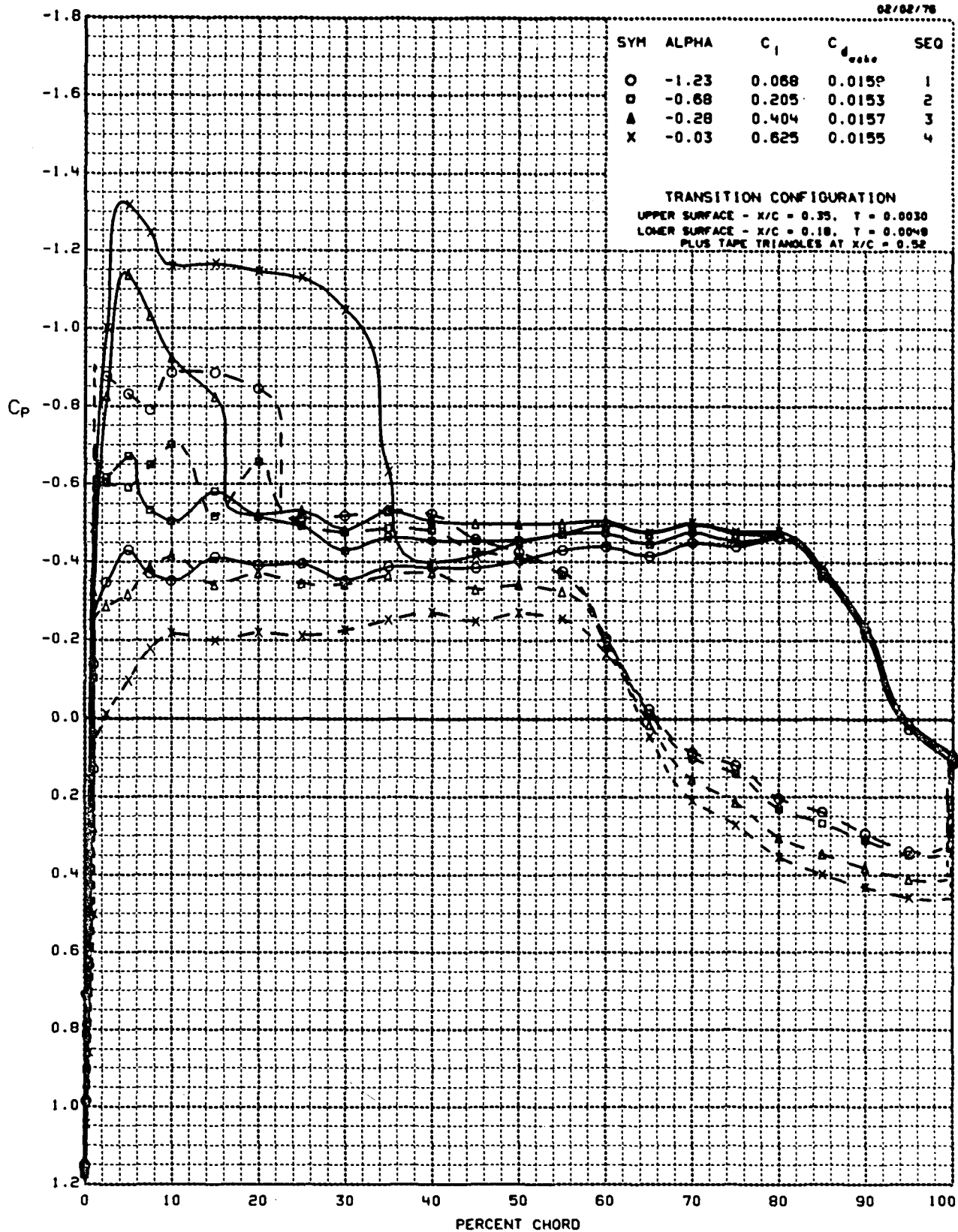
MACH NUMBER = 0.758

REYNOLDS NUMBER =  $3.97 \times 10^6$

RUN = 106

AMES 22-060-5

02/02/78



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

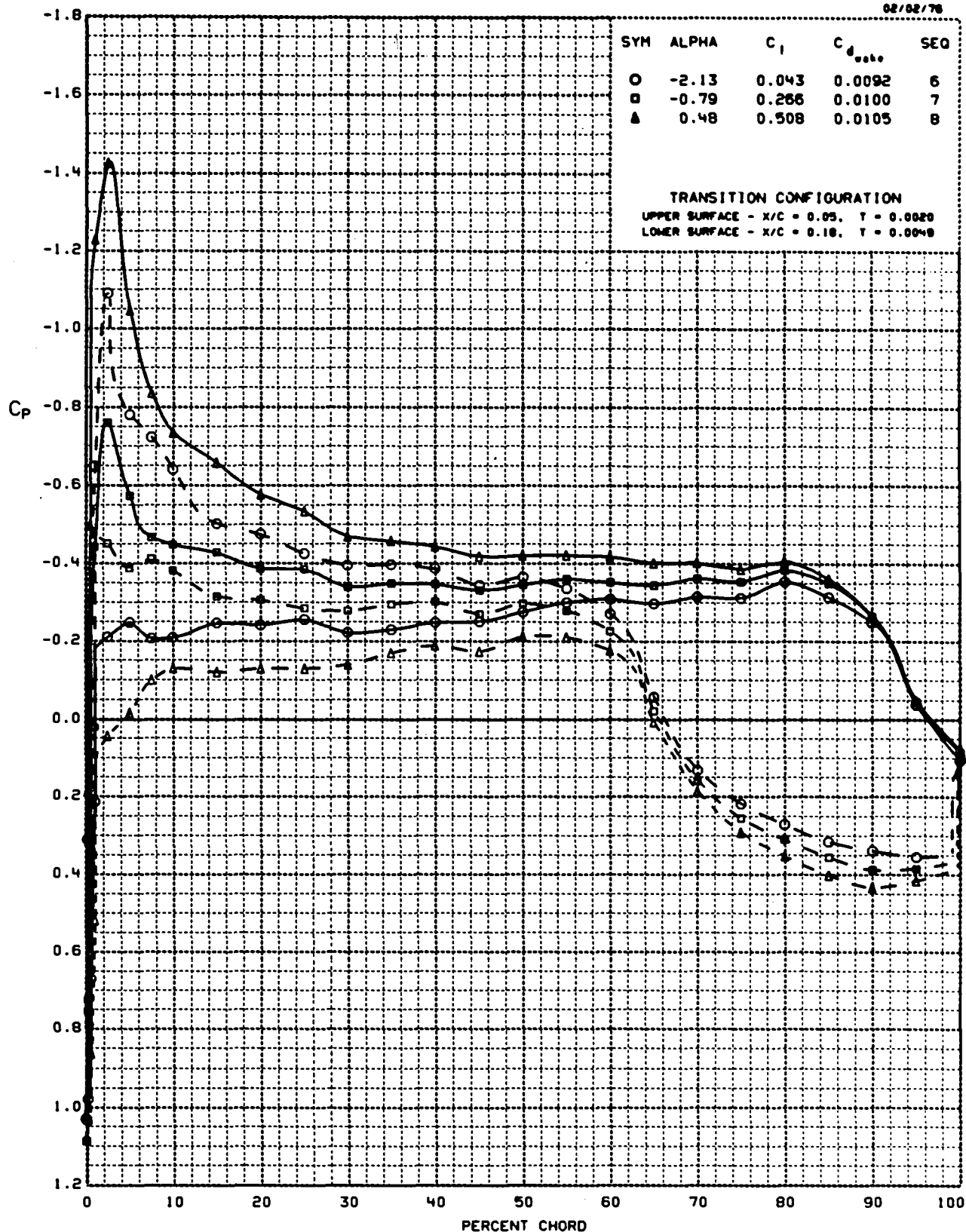
MACH NUMBER = 0.501

REYNOLDS NUMBER =  $4.05 \times 10^6$

RUN = 107

AMES 22-060-5

02/02/78





WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

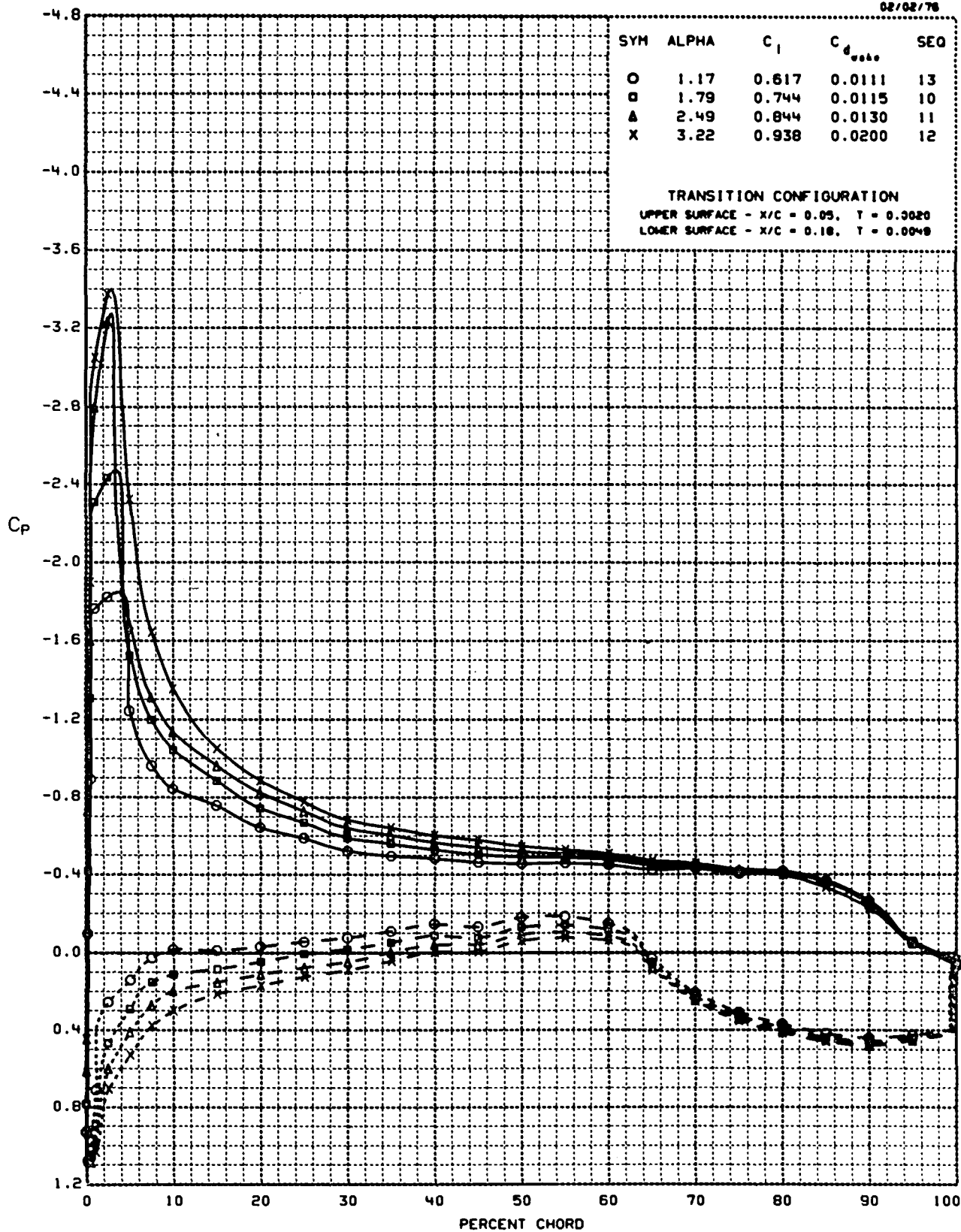
MACH NUMBER = 0.500

REYNOLDS NUMBER =  $3.97 \times 10^6$

RUN -107

AMES 22-060-5

02/02/78



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

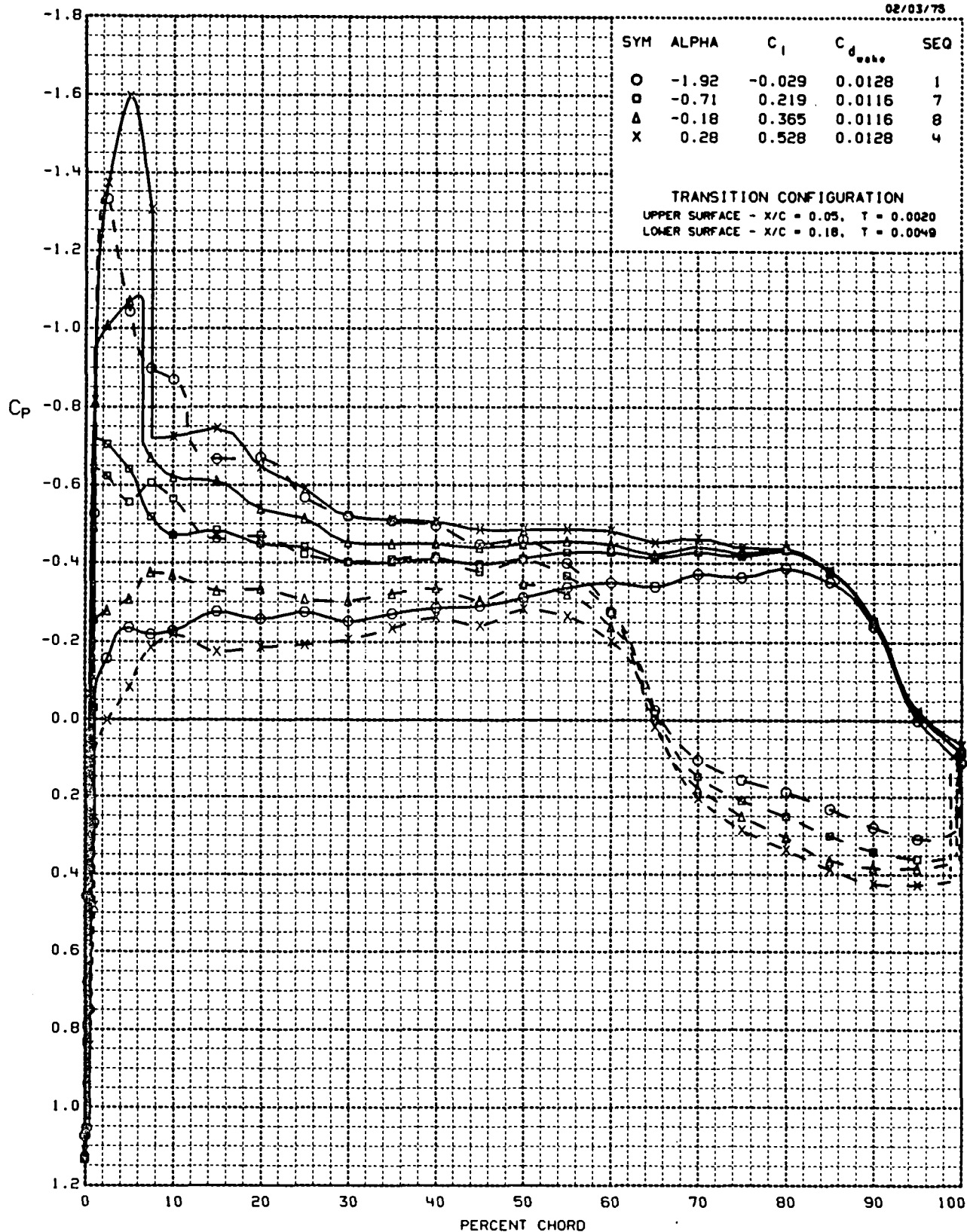
MACH NUMBER = 0.679

REYNOLDS NUMBER =  $3.97 \times 10^6$

RUN = 108

AMES 22-060-5

02/03/75

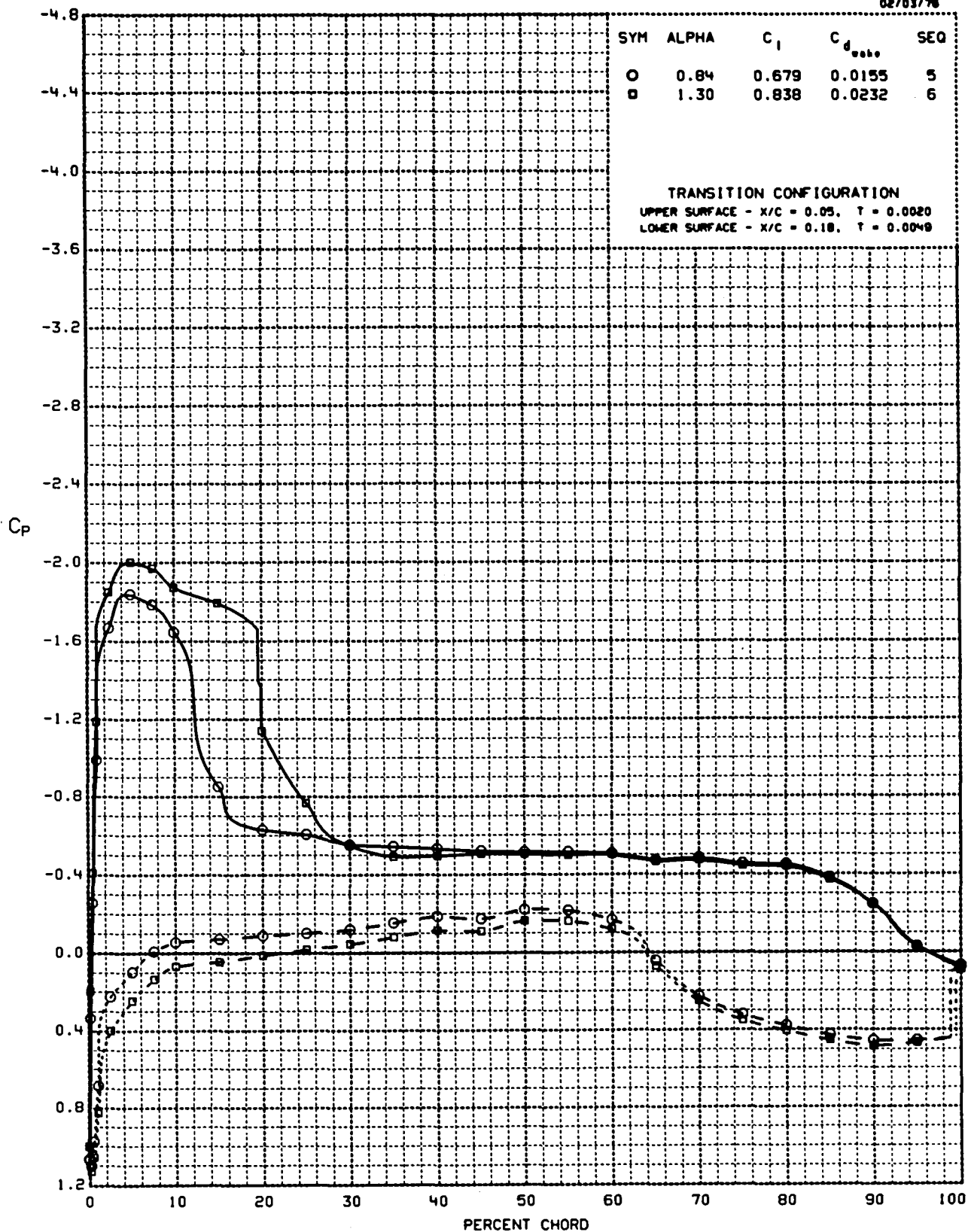


WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS  
 MACH NUMBER = 0.679 REYNOLDS NUMBER =  $3.95 \times 10^6$  RUN = 108 AMES 22-060-5

02/03/78

SYM	ALPHA	$C_l$	$C_{d_{total}}$	SEQ
O	0.84	0.679	0.0155	5
□	1.30	0.838	0.0232	6

TRANSITION CONFIGURATION  
 UPPER SURFACE -  $X/C = 0.05$ ,  $\tau = 0.0020$   
 LOWER SURFACE -  $X/C = 0.18$ ,  $\tau = 0.0049$



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

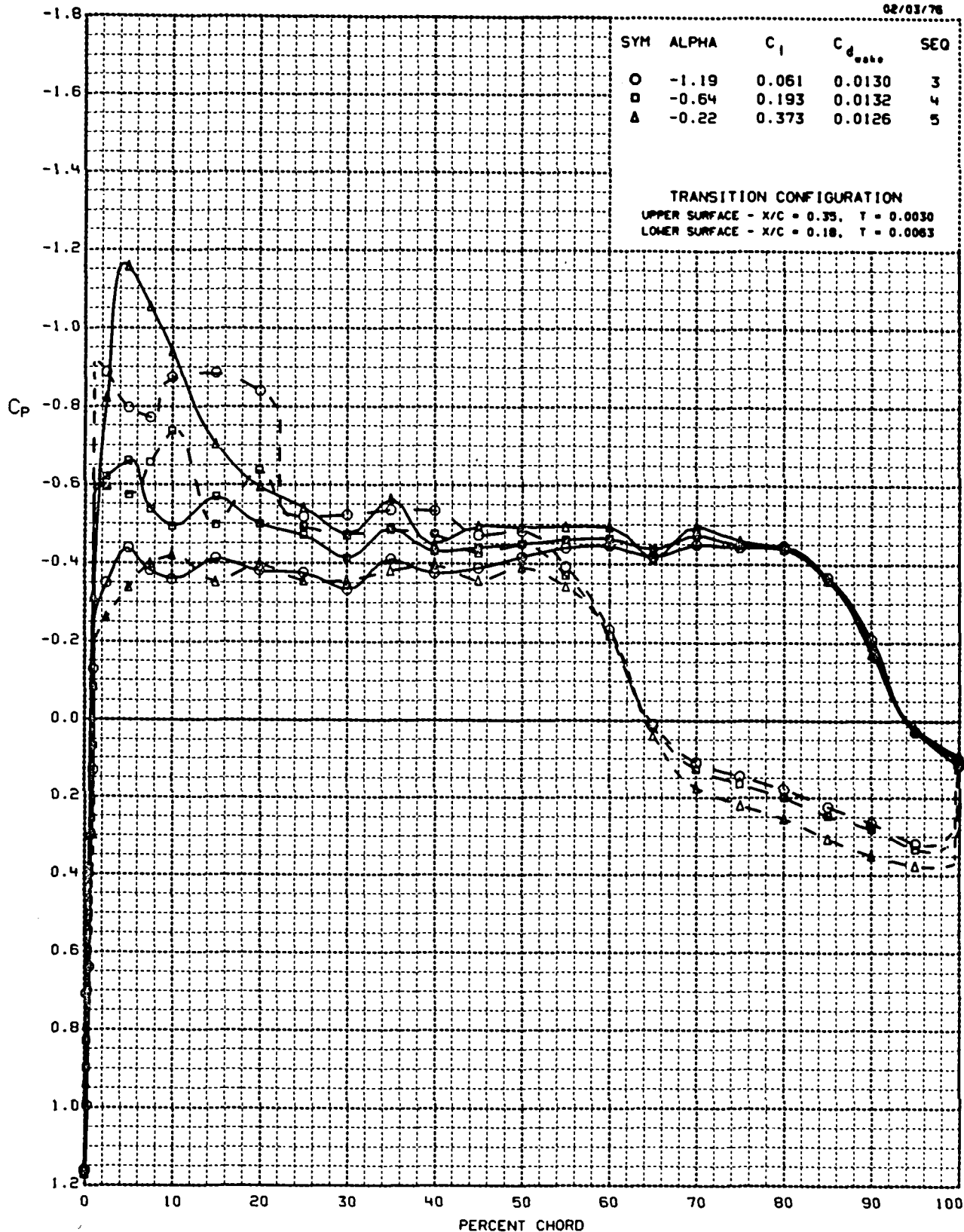
MACH NUMBER = 0.759

REYNOLDS NUMBER =  $4.00 \times 10^6$

RUN = 109

AMES 22-060-5

02/03/76



# WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

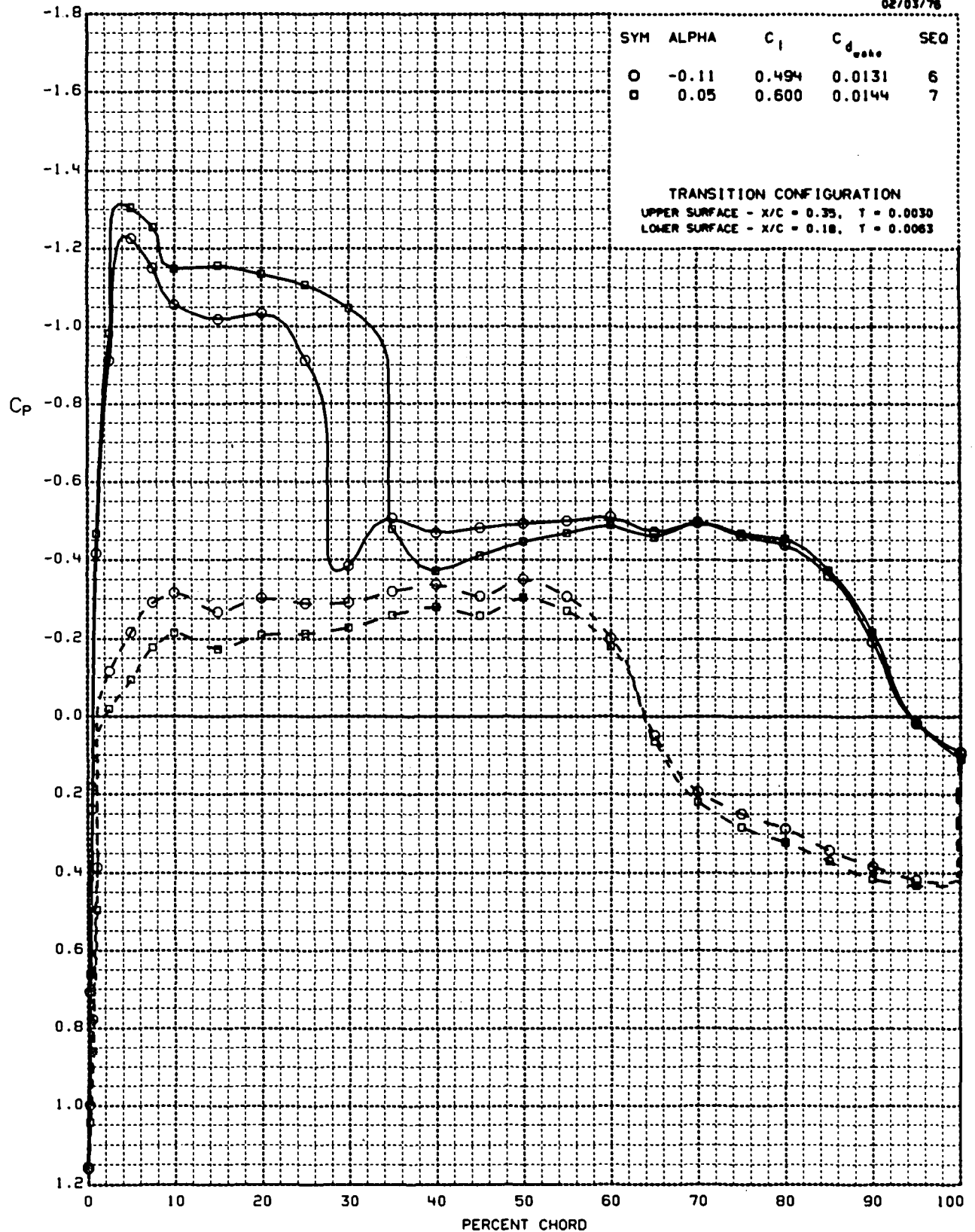
MACH NUMBER = 0.759

REYNOLDS NUMBER =  $3.93 \times 10^6$

RUN = 109

AMES 22-060-5

02/03/76



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

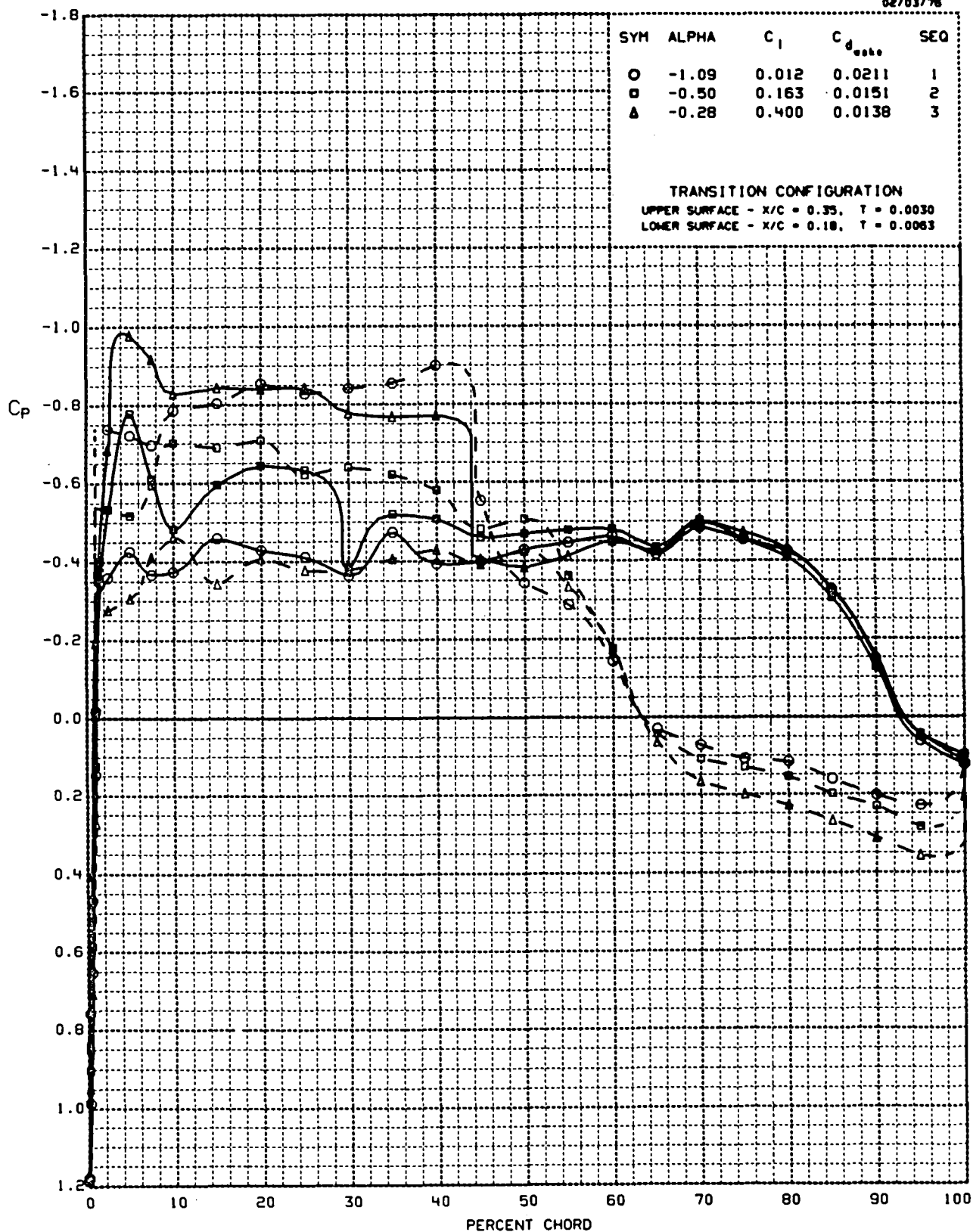
MACH NUMBER = 0.799

REYNOLDS NUMBER =  $2.99 \times 10^6$

RUN =110

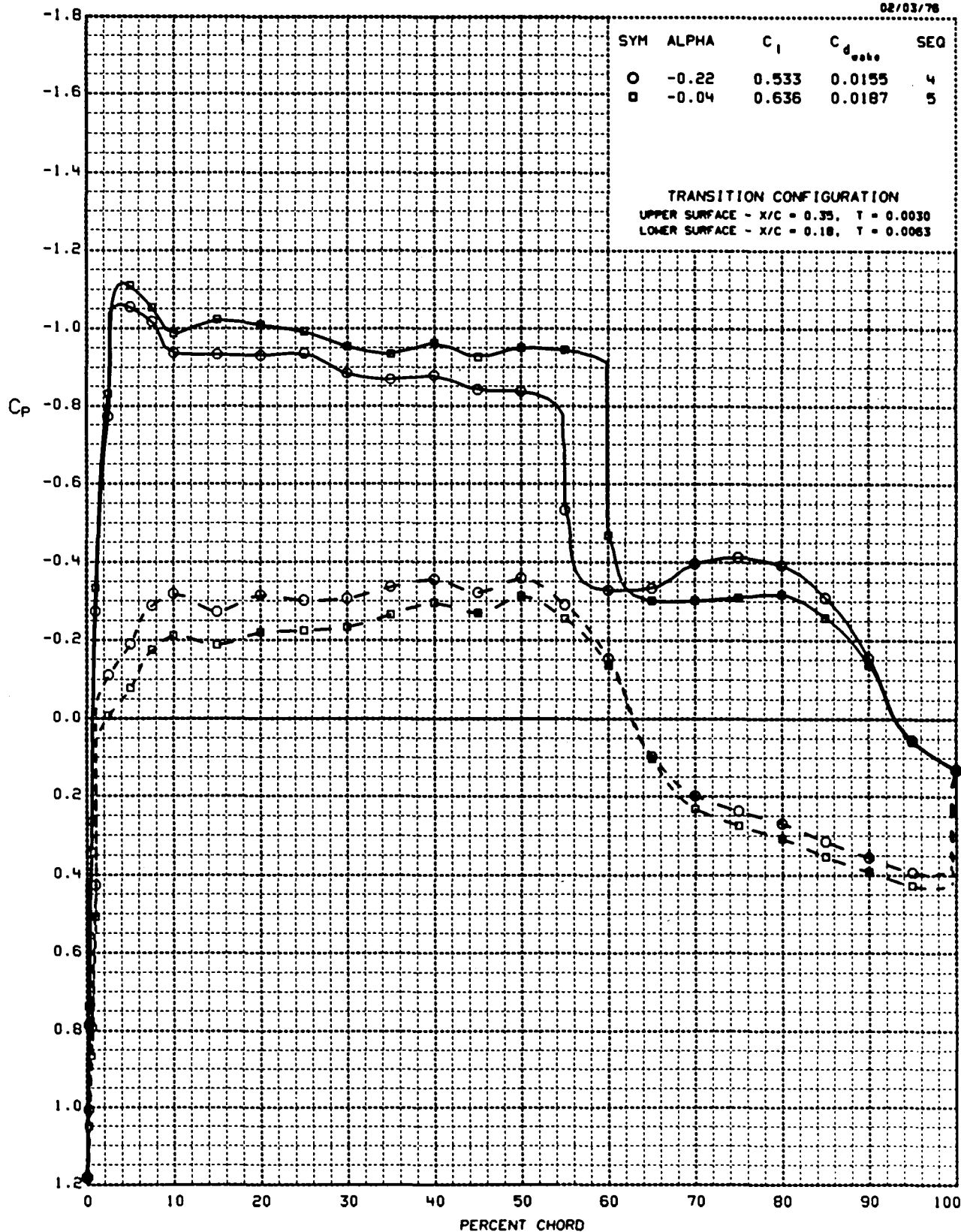
AMES 22-060-5

02/03/76



WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523  
 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS  
 MACH NUMBER = 0.799      REYNOLDS NUMBER =  $2.97 \times 10^6$       RUN = 110      AMES 22-060-5

02/03/78



# WIND TUNNEL MODEL LB-400C -- AIRFOIL DSMA 523 TWO DIMENSIONAL CHORDWISE PRESSURE DISTRIBUTIONS

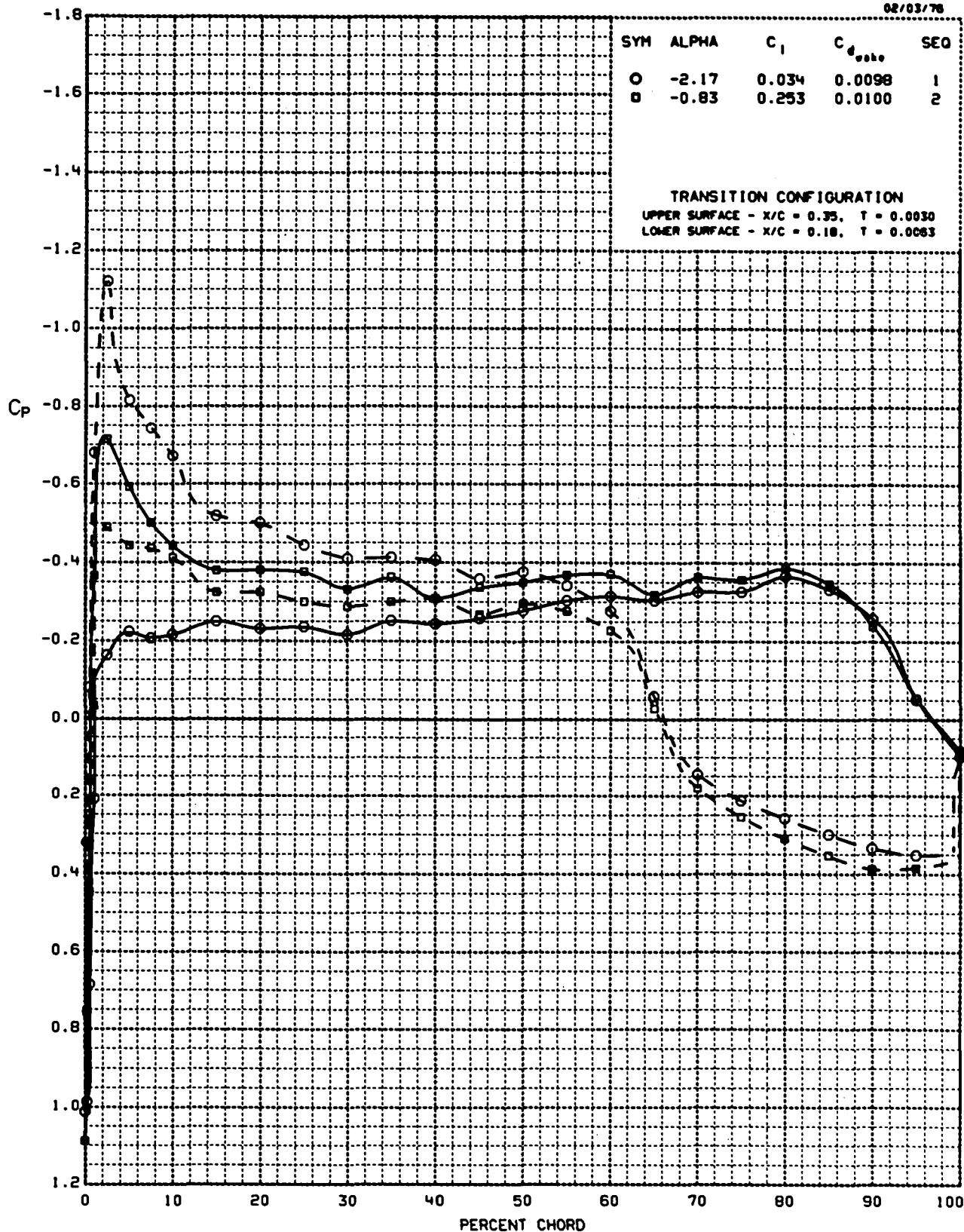
MACH NUMBER = 0.500

REYNOLDS NUMBER =  $4.07 \times 10^6$

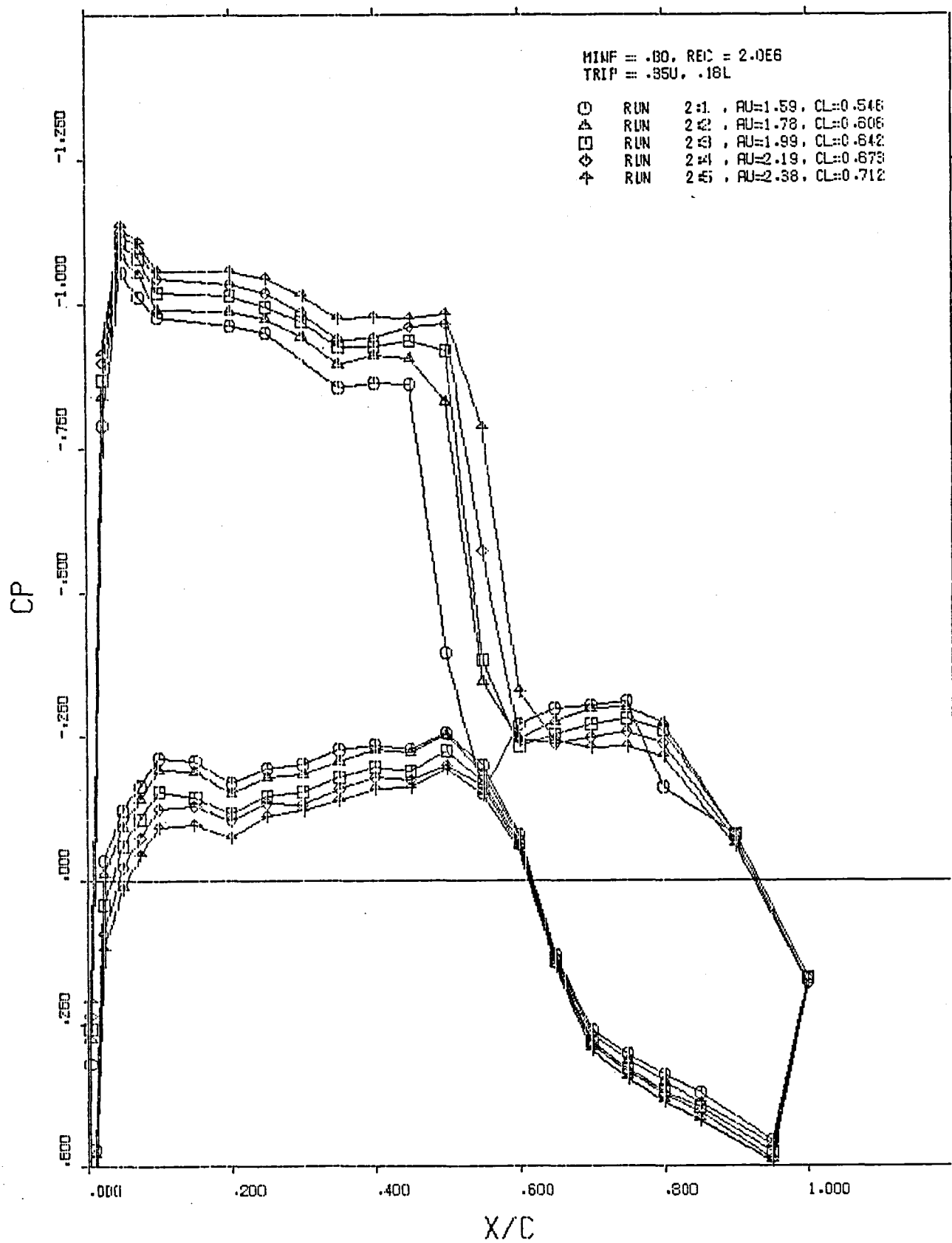
RUN =111

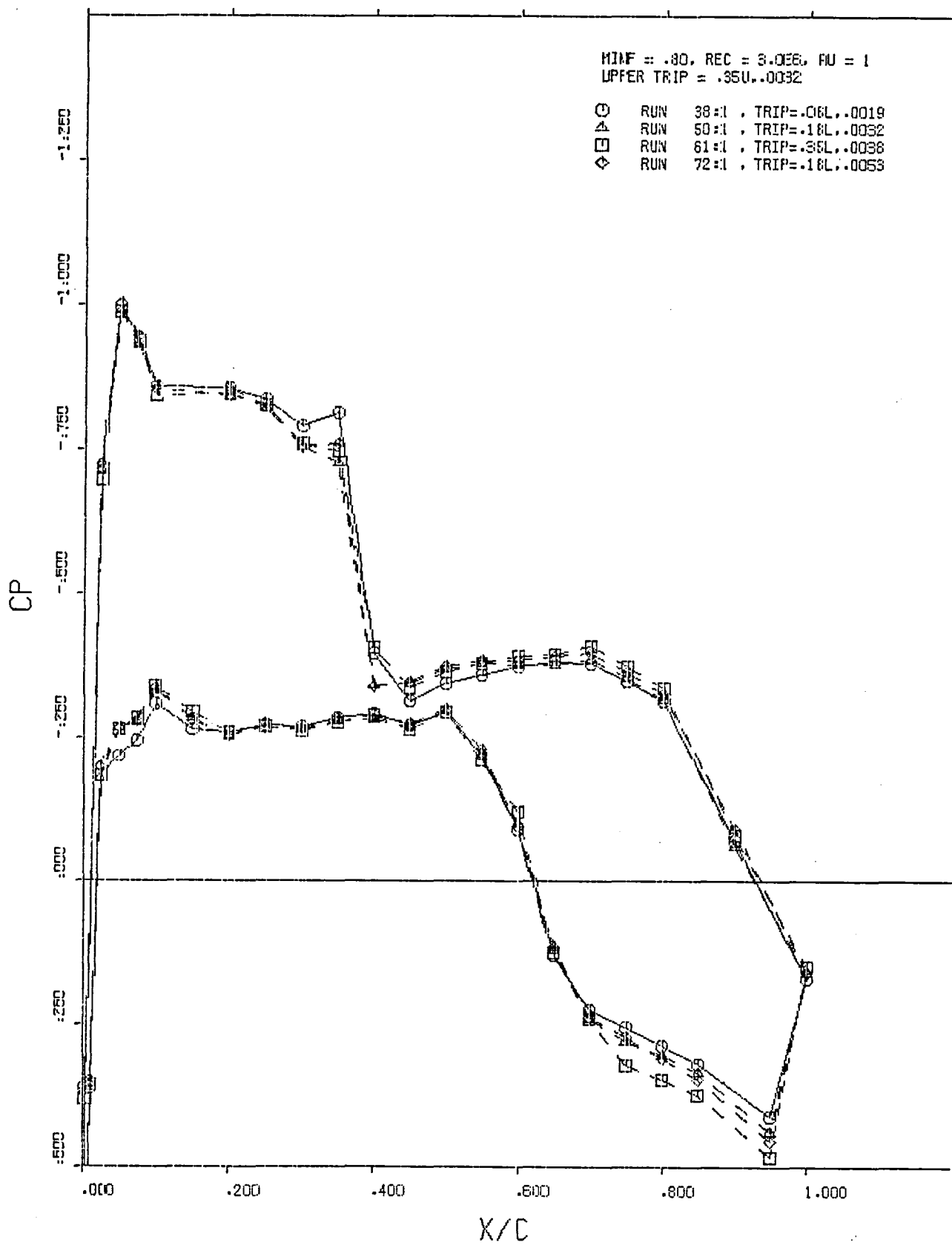
AMES 22-060-5

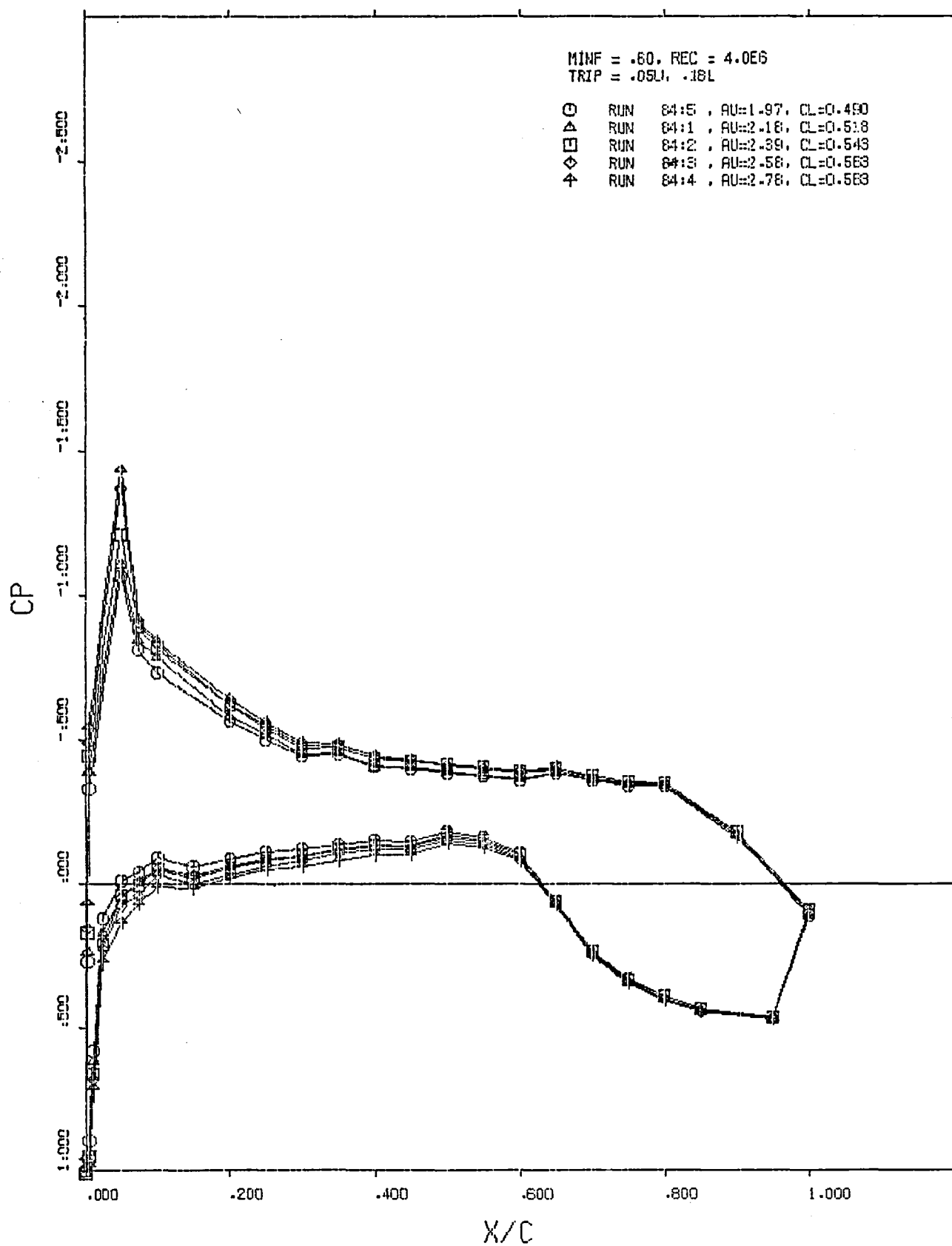
02/03/76











## APPENDIX B

### DSMA 523 MODEL, BLUNT TRAILING EDGE, 1975, 1976, AND 1977

The trip configuration designation "L.E. - 0.002" means a leading-edge trip with a bead diameter of 0.002 in. For data taken during 1976 (runs 22-56) and 1977 (runs 4-80) the year is shown in the plot titles. The year is omitted from the plots of the 1975 data, which have run numbers of 112-130.

TABLE B1. RUN SCHEDULE, DSMA 523 MODEL, BLUNT TRAILING EDGE

(1975 data)

Run no.	Nominal $M_\infty$	Nominal $Re_c$	Boundary-layer trip			
			Upper		Lower	
			x/c	T(in.)	x/c	T(in.)
112	0.75	$2 \times 10^6$	leading edge	0.002	leading edge	0.002
113	.80	$2 \times 10^6$	↓	↓	↓	↓
114	.75	$2 \times 10^6$				
115	.80	$2 \times 10^6$				
116	.83	$2 \times 10^6$				
117	.75	$4 \times 10^6$				
118	.83	$2 \times 10^6$				
119, 120	.75	$2 \times 10^6$	0.35	.0049	0.18	.0053
121	.80	$2 \times 10^6$	↓	.0049	↓	.0053
122	.83	$2 \times 10^6$		.0049		.0053
123	.80	$4 \times 10^6$		.0030		.0049
124	.83	$4 \times 10^6$		.0030		.0049
125	.80	$2 \times 10^6$		.0049	.35	.0075
126	.83	$2 \times 10^6$		↓	↓	↓
127	.75	$2 \times 10^6$		↓		
128	.60	$2 \times 10^6$		↓		
129	.60	$2 \times 10^6$	.05	.0035	.18	.0049
130	.70	$2 \times 10^6$	.05	.0035	.18	.0049

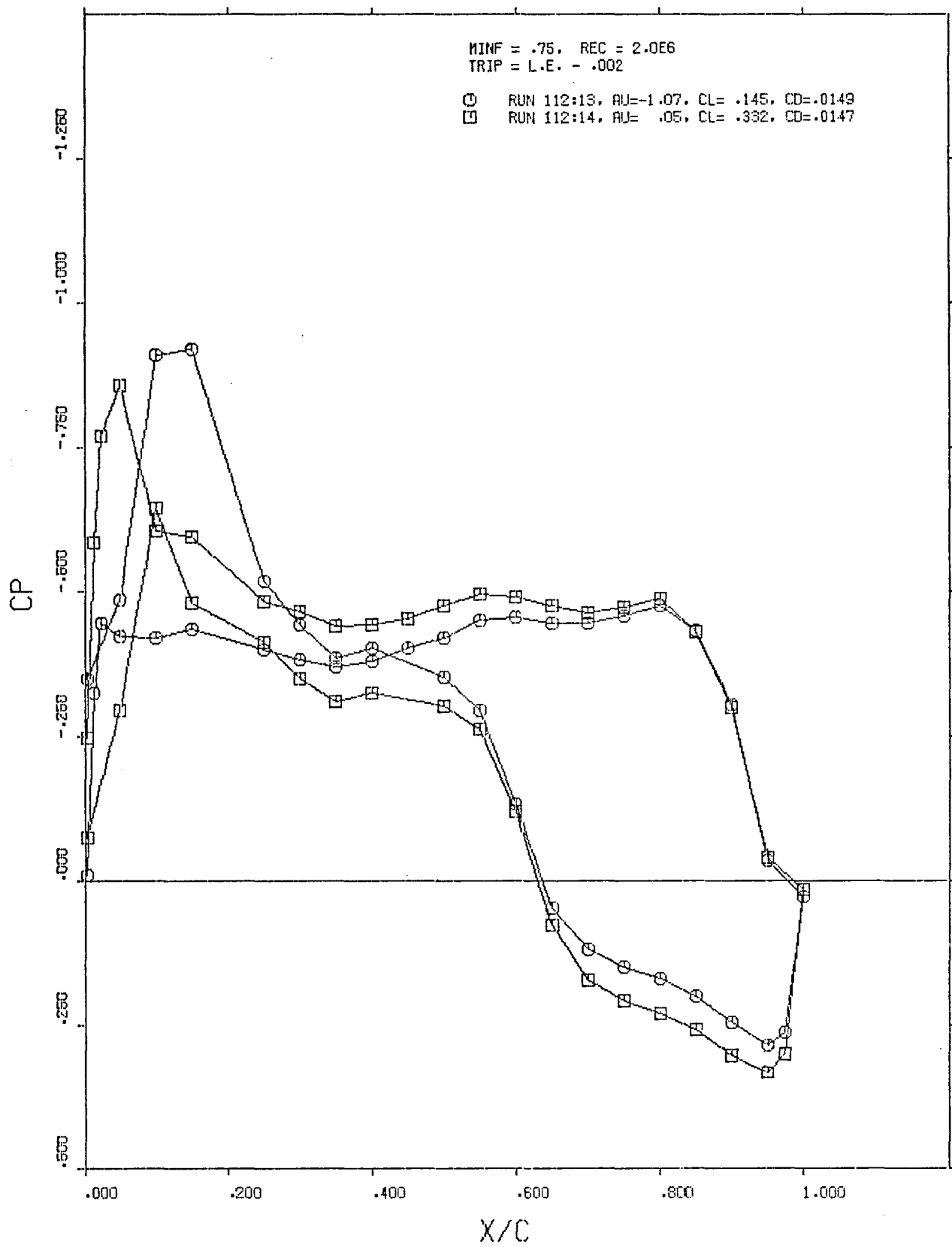
TABLE B1. CONCLUDED.

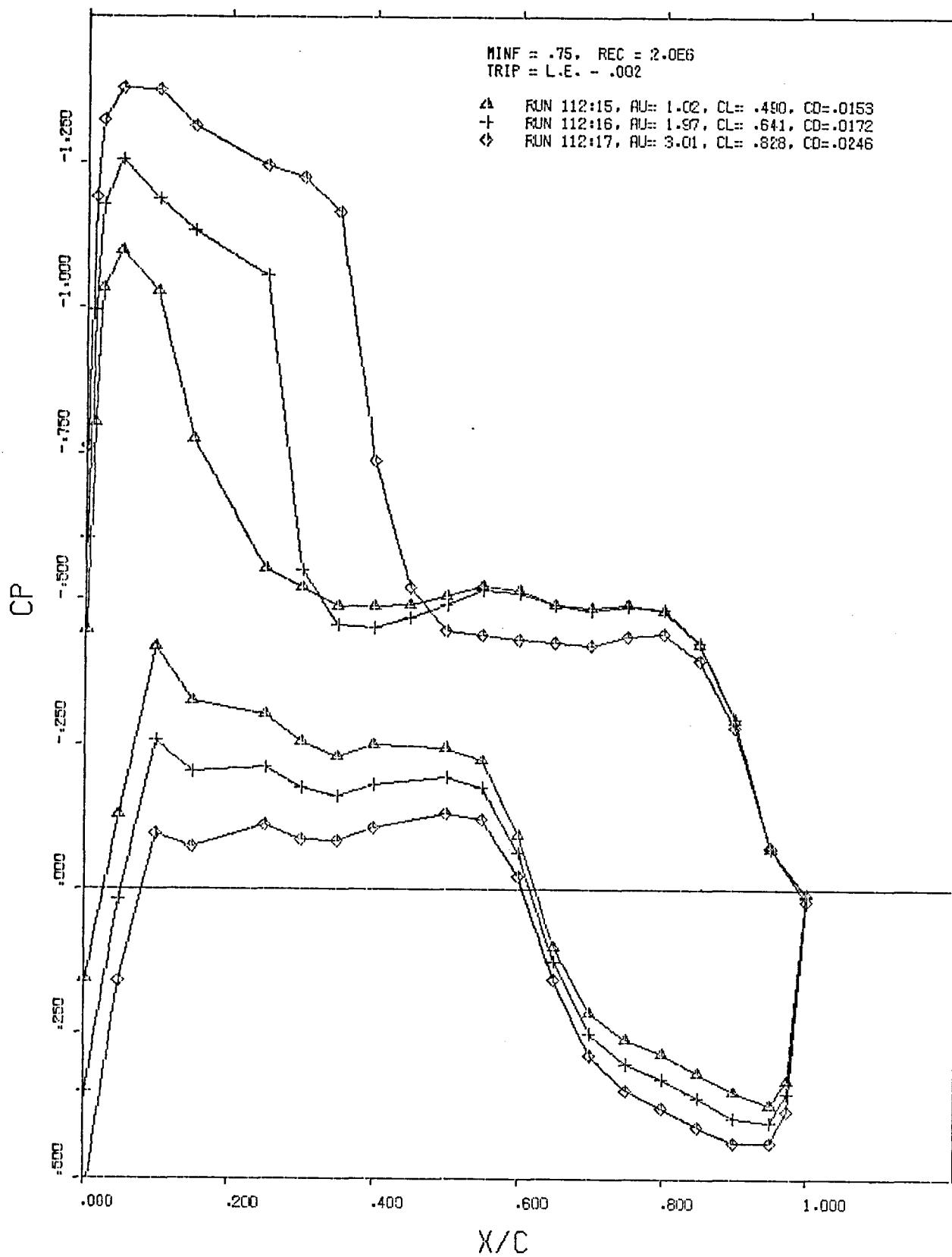
(1976 data)

Run no.	Nominal $M_\infty$	Nominal $Re_c$	Boundary-layer trip			
			Upper		Lower	
			x/c	T(in.)	x/c	T(in.)
22	0.60	$2 \times 10^6$	0.05	0.0035	0.18	0.0053
26	.75	$2 \times 10^6$	.05	.0035	↓	↓
43	.80	$2 \times 10^6$	.35	.0053		
44	.82	$2 \times 10^6$	↓	↓		
45	.84	$2 \times 10^6$				
46	.87	$2 \times 10^6$				
47	.90	$2 \times 10^6$				
48	.80	$2 \times 10^6$				
49	.82	$2 \times 10^6$				
50	.84	$2 \times 10^6$				
51	.84	$2 \times 10^6$				
52	.874	$2 \times 10^6$				
53	.90	$2 \times 10^6$				
54	.75	$2 \times 10^6$				
55	.70	$2 \times 10^6$				
56	.60	$2 \times 10^6$				

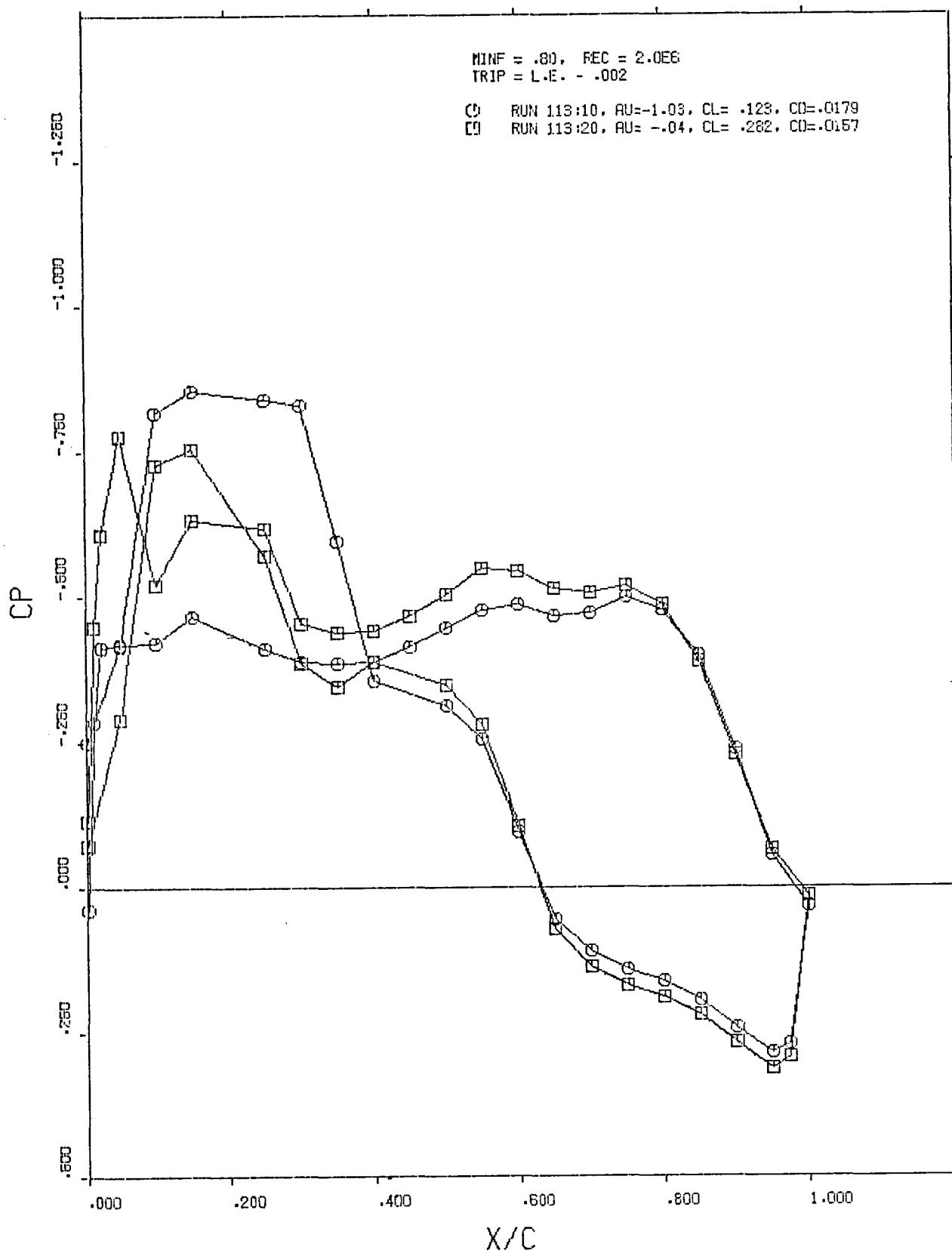
(1977 data)

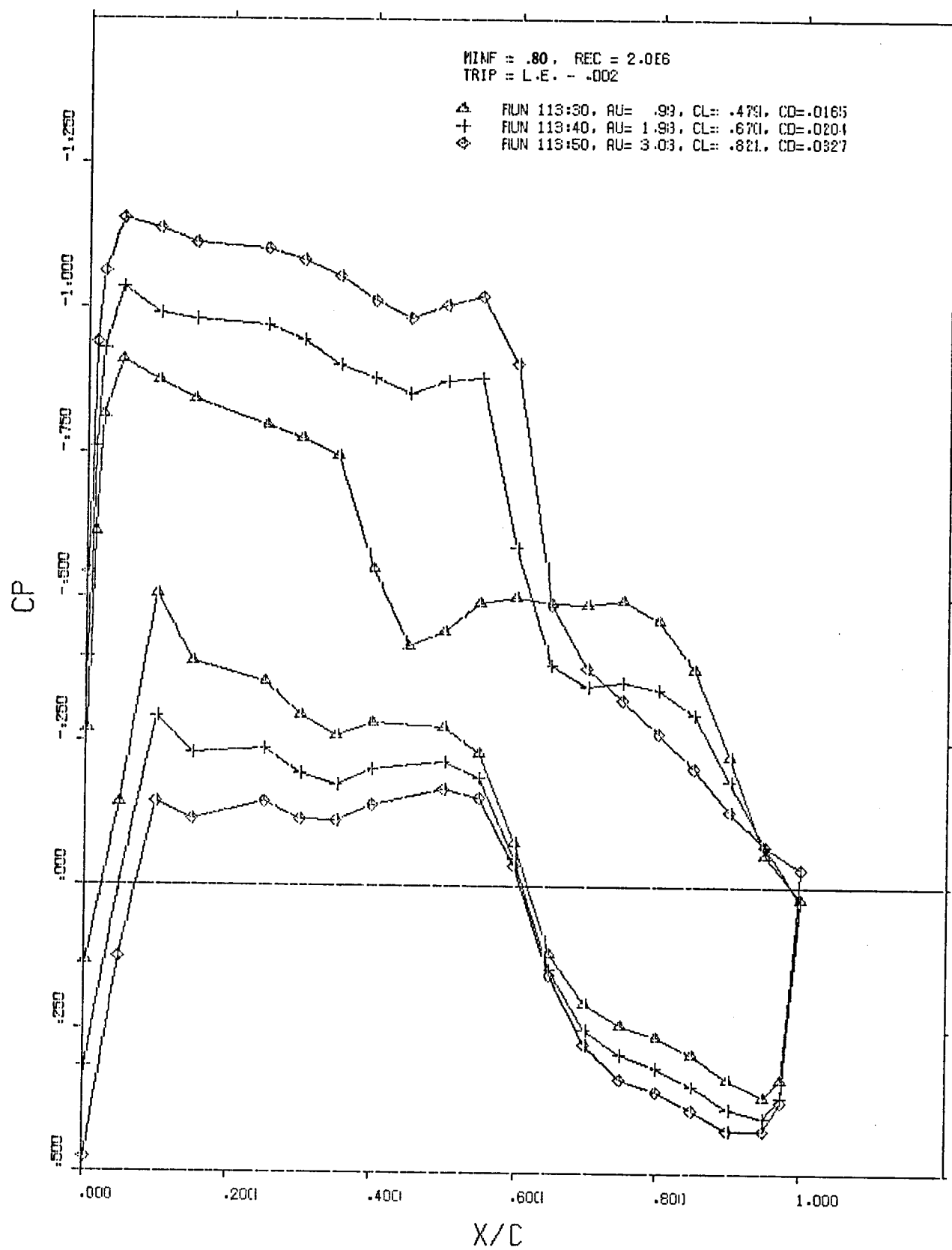
Run no.	Nominal $M_\infty$	Nominal $Re_c$	Boundary-layer trip			
			Upper		Lower	
			x/c	T(in.)	x/c	T(in.)
4	0.60	$2 \times 10^6$	0.05	0.0038	0.18	0.0053
44,45	.75	$2 \times 10^6$	.05	.0038	↓	↓
77	.83	$2 \times 10^6$	.35	.0053		
78	.80	$2 \times 10^6$	↓	↓		
79	.83	$2 \times 10^6$				
80	.80	$2 \times 10^6$				

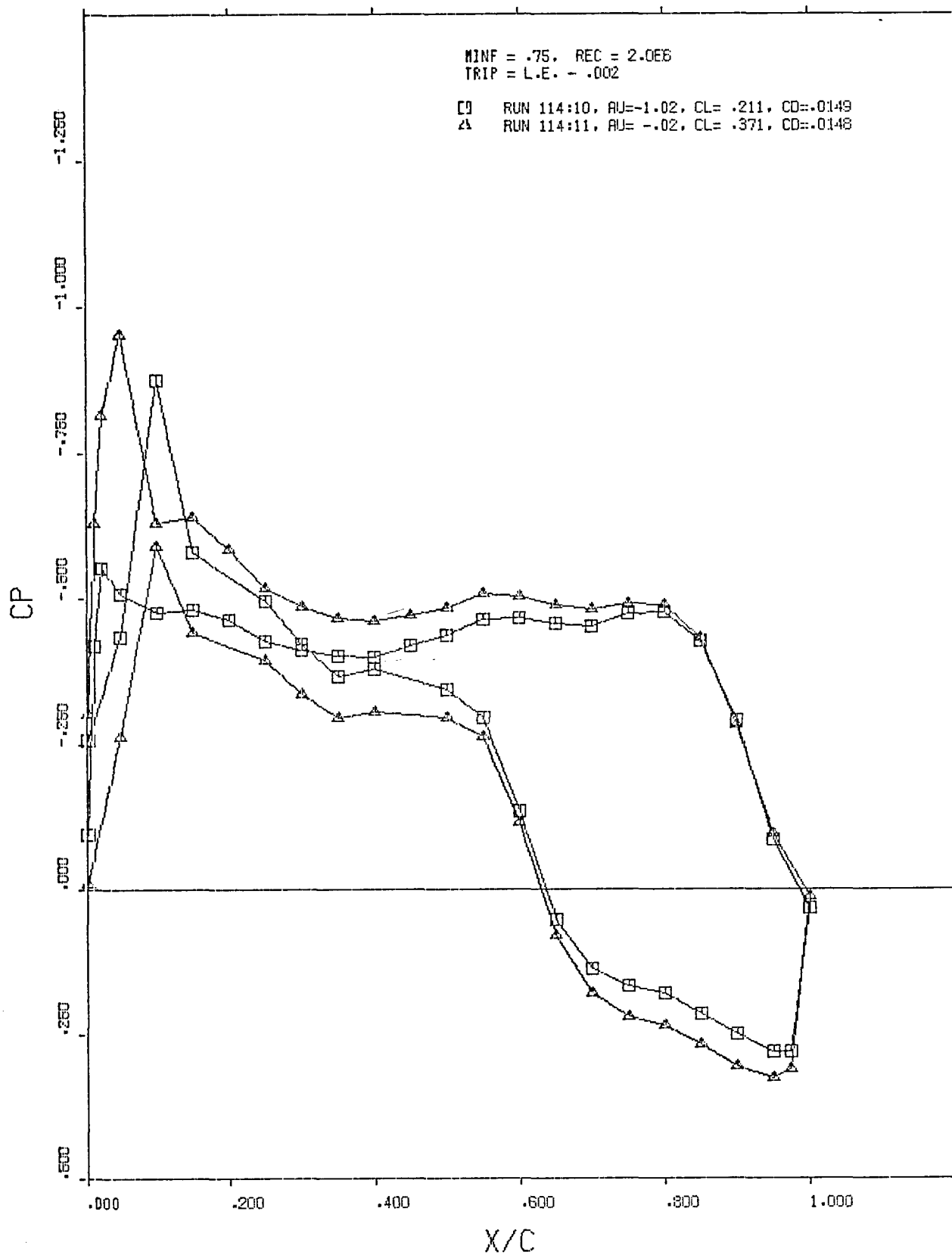


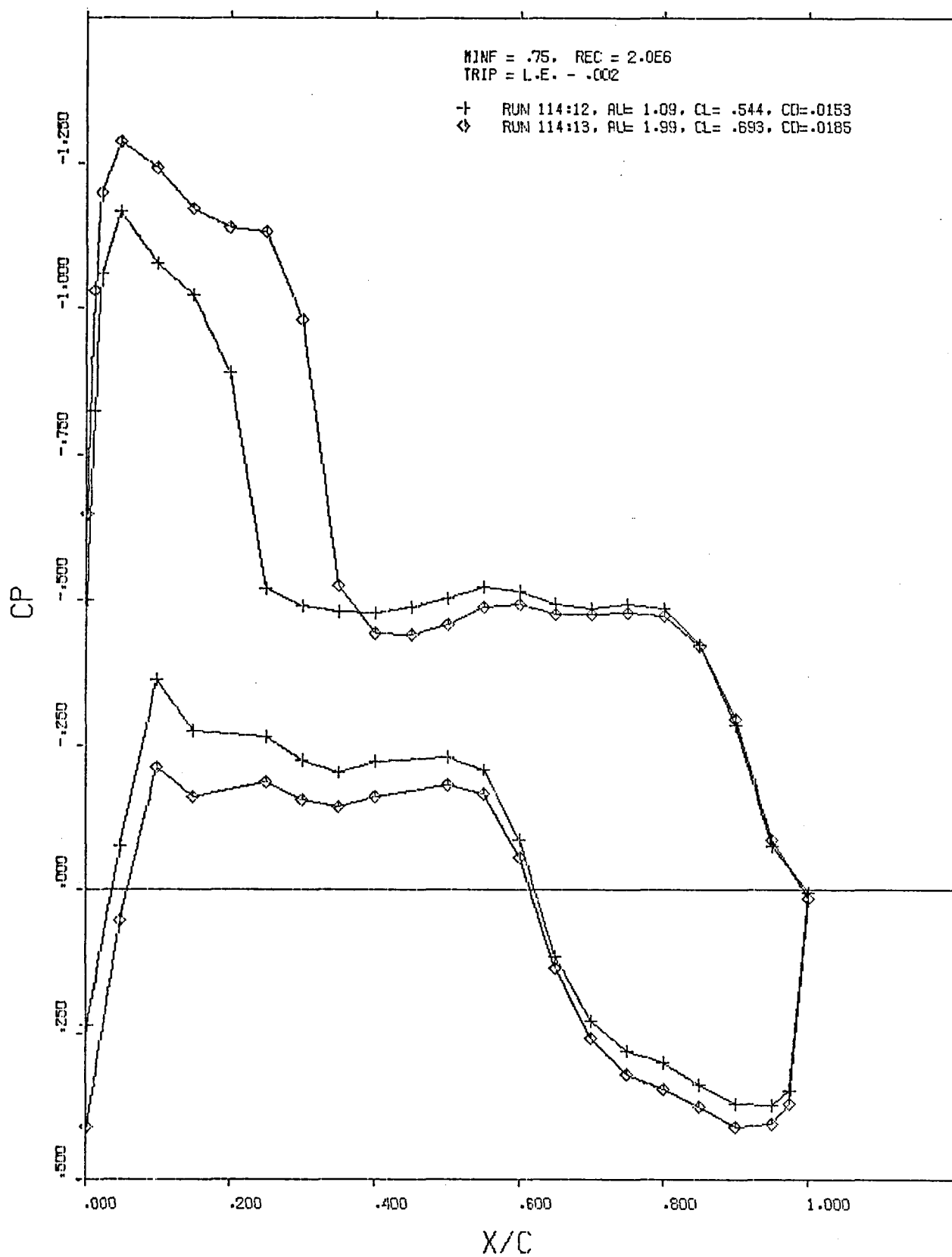


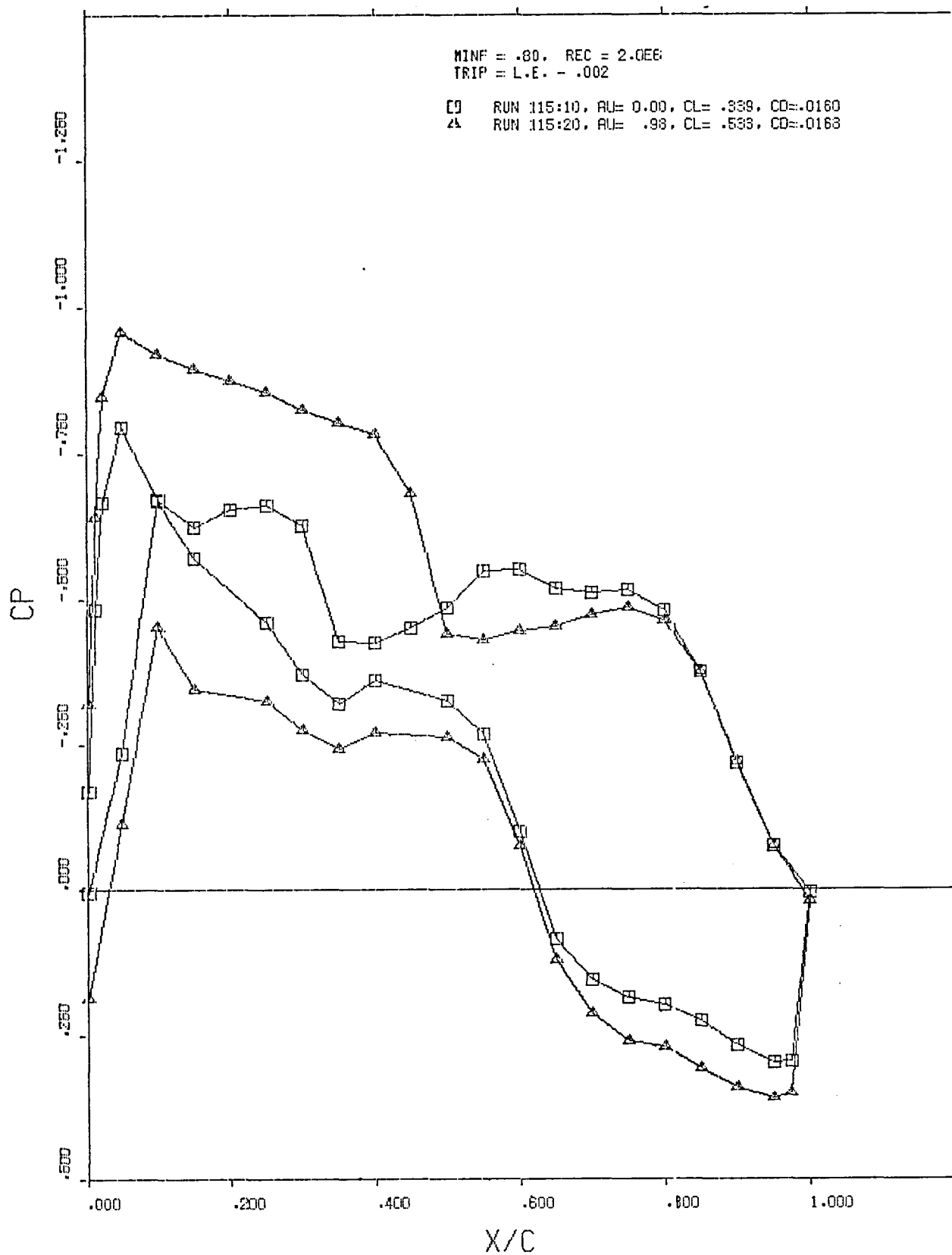


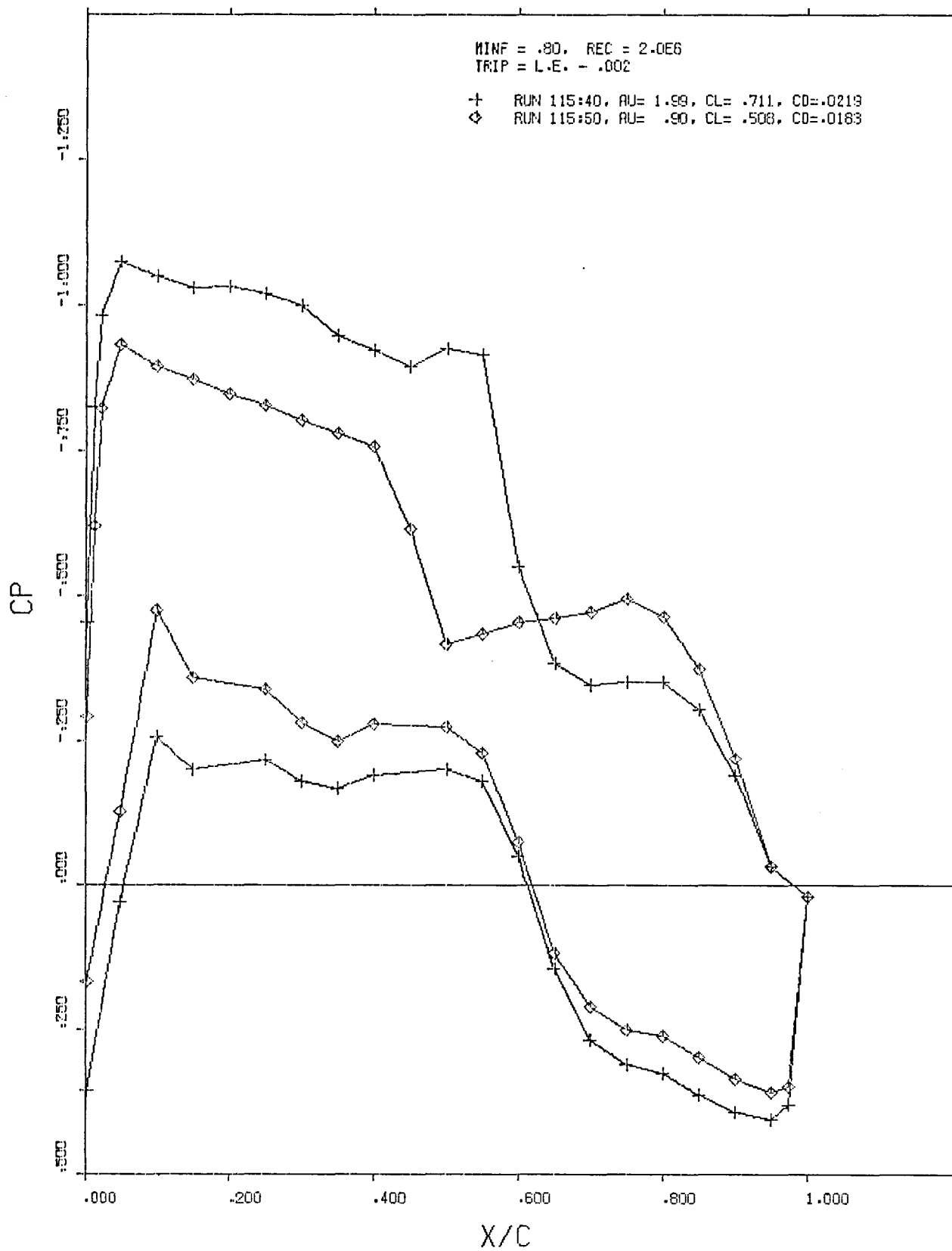


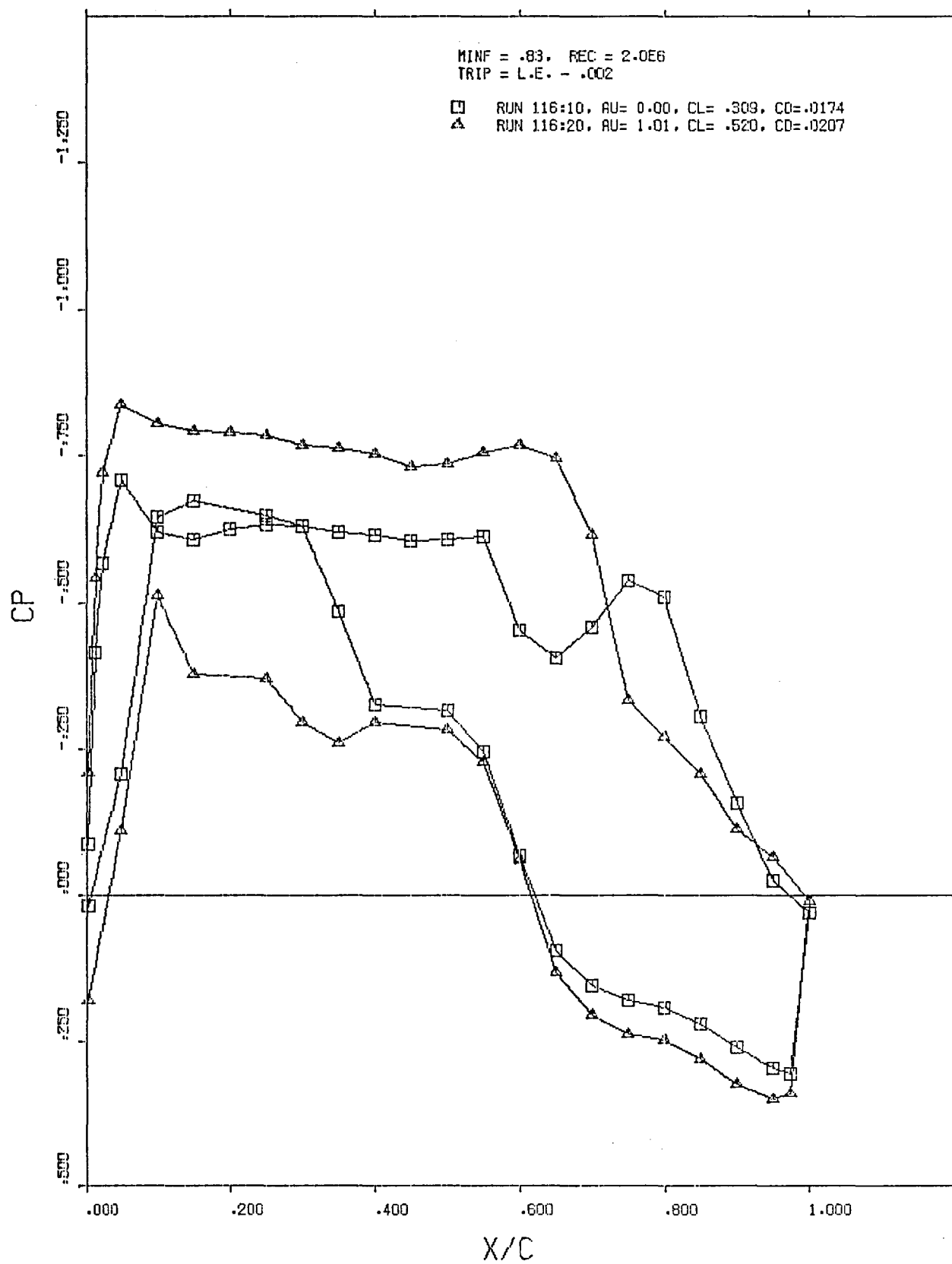


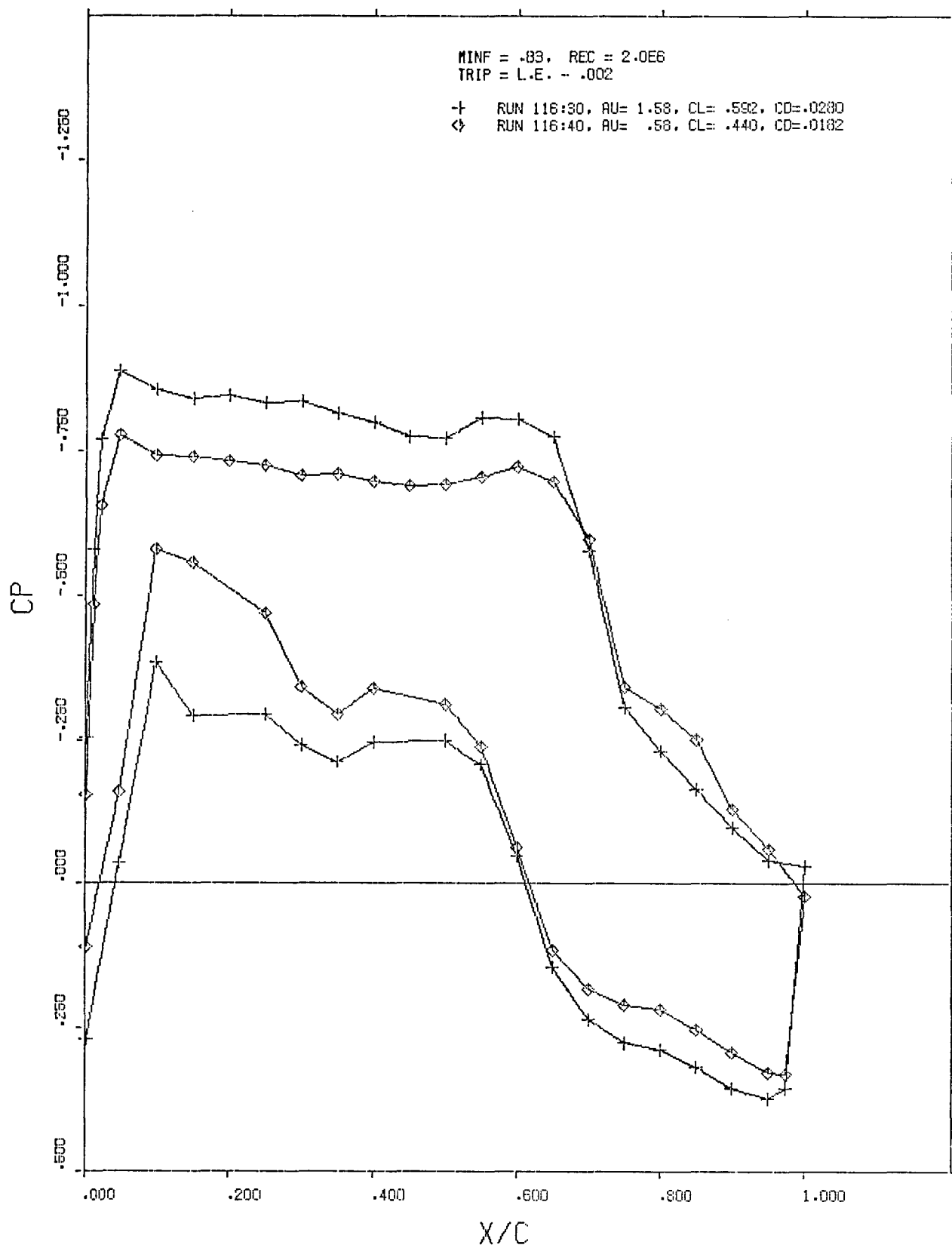




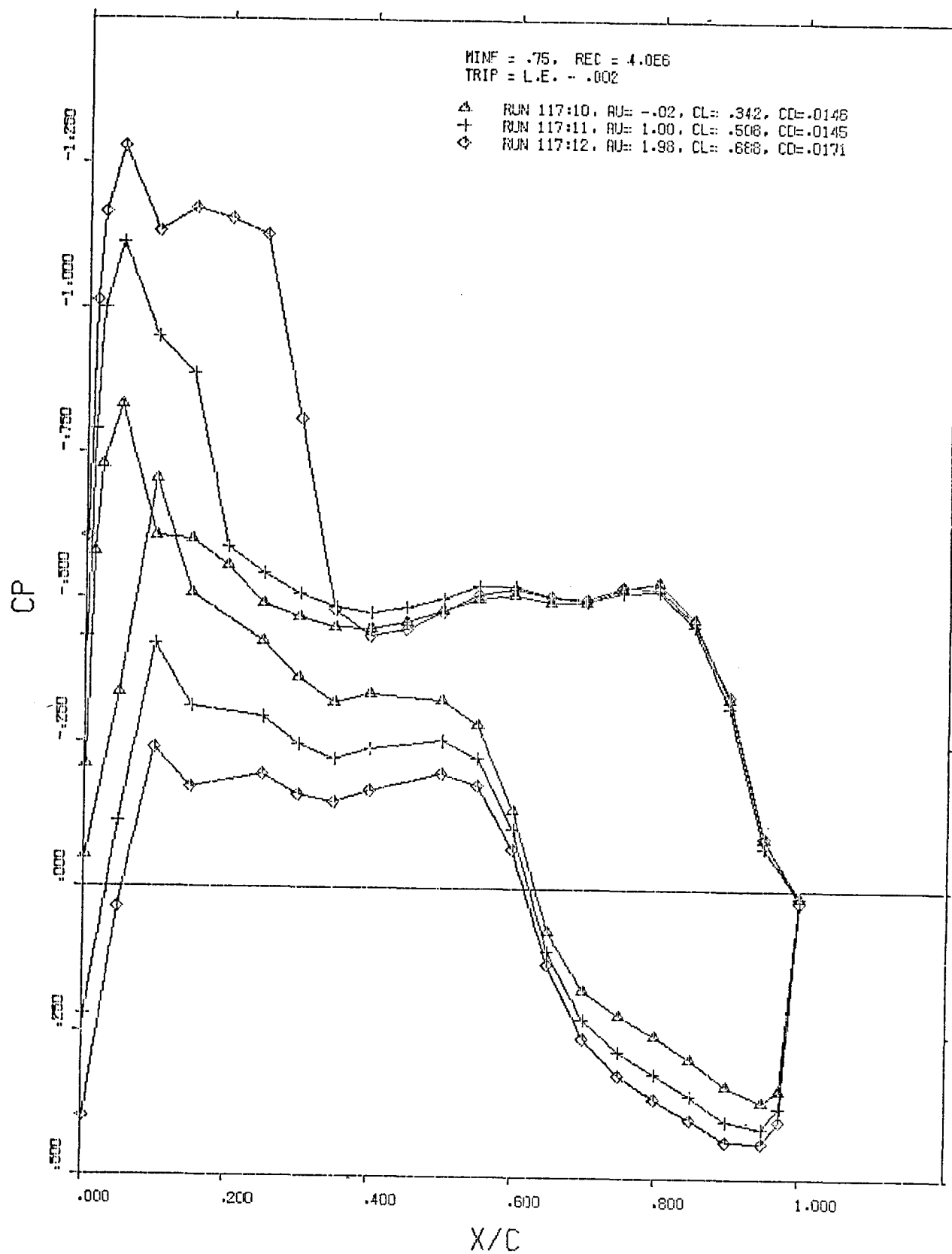


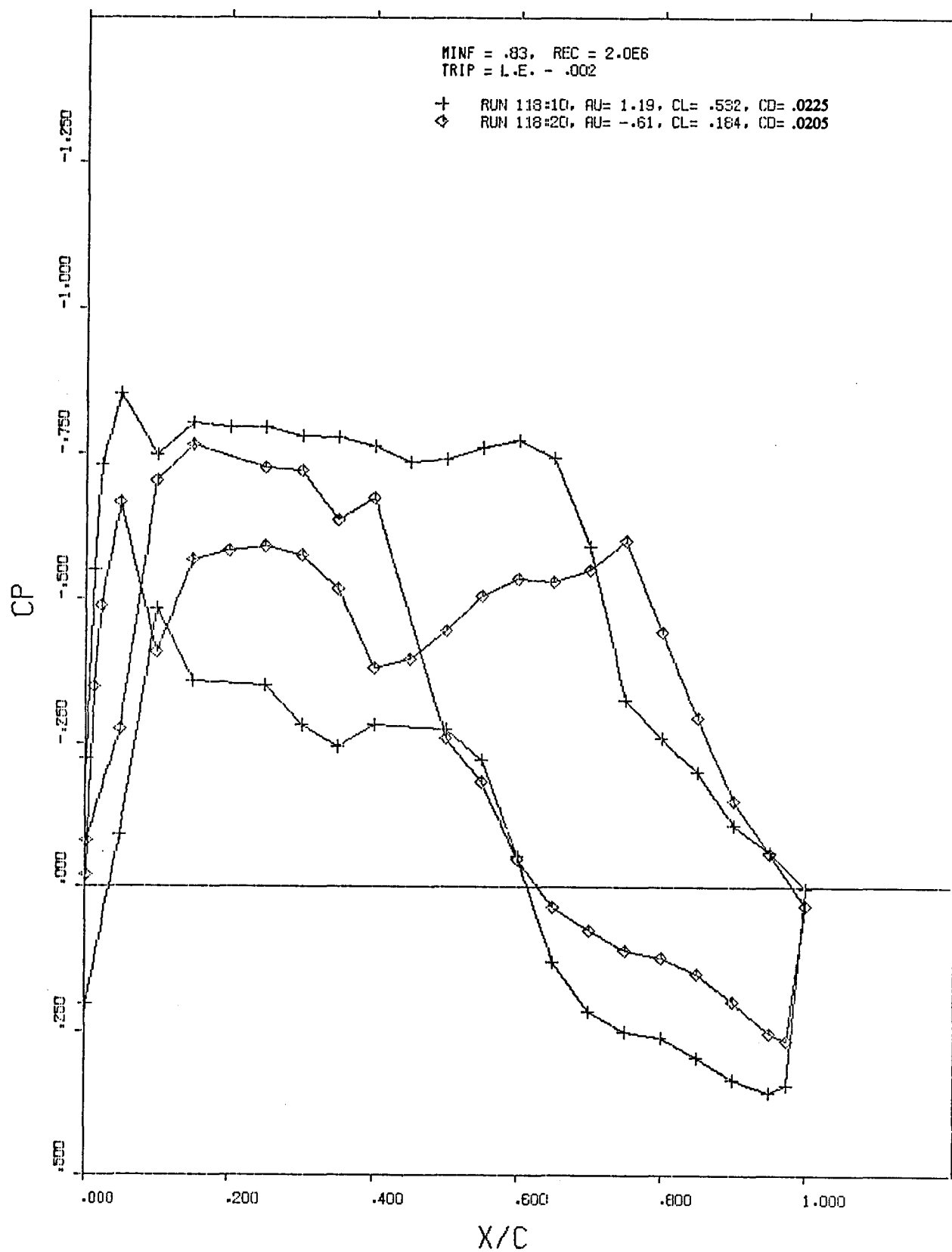


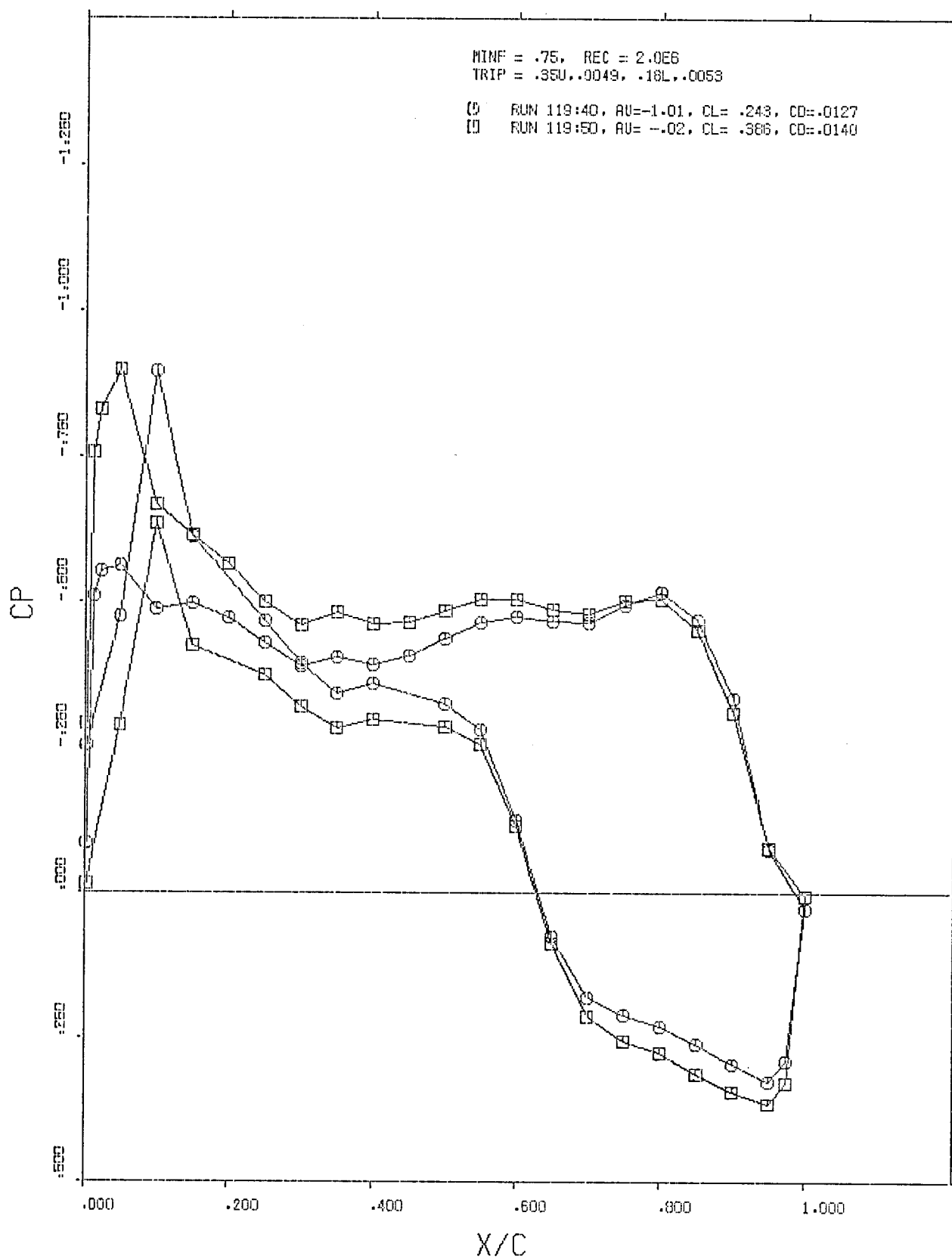


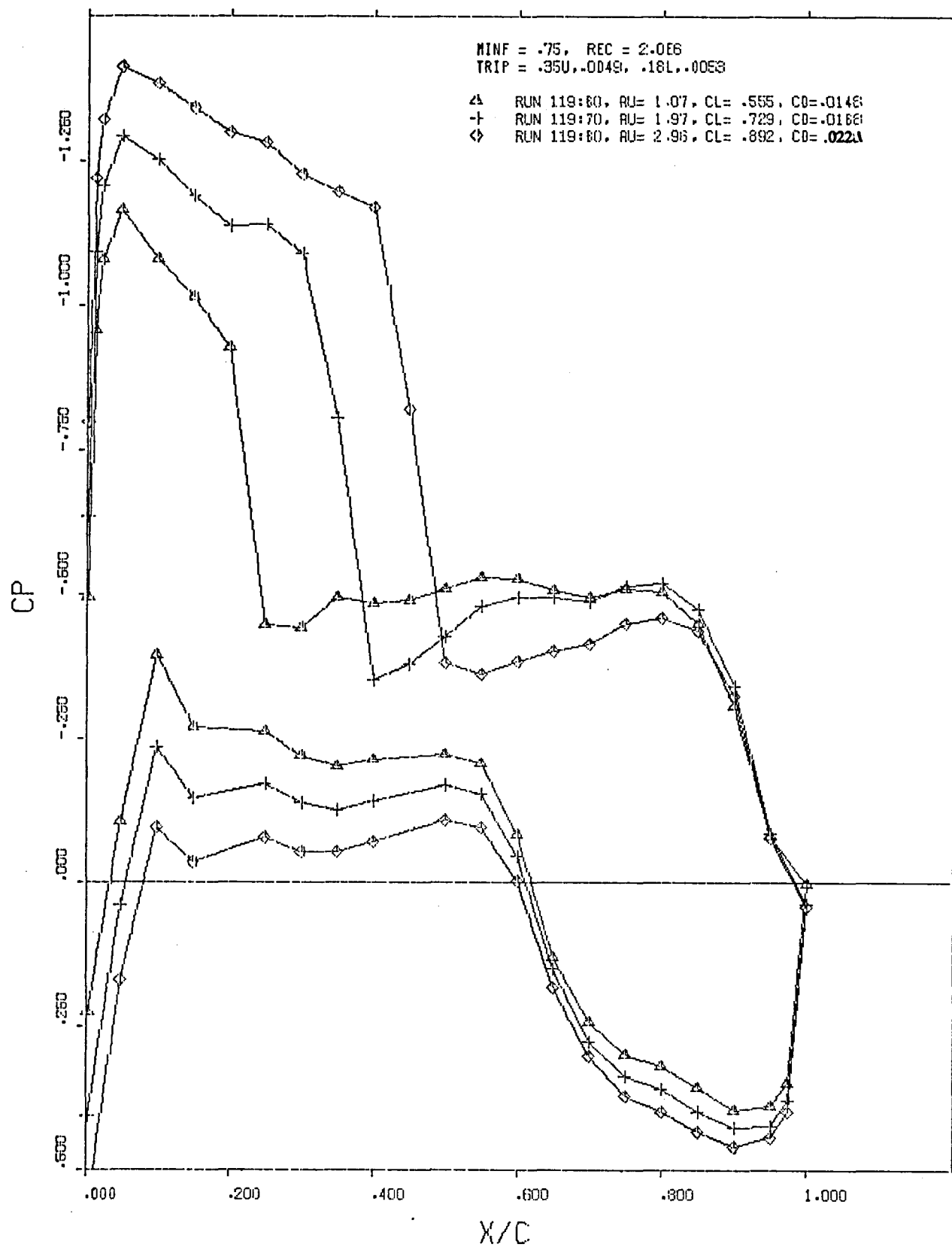


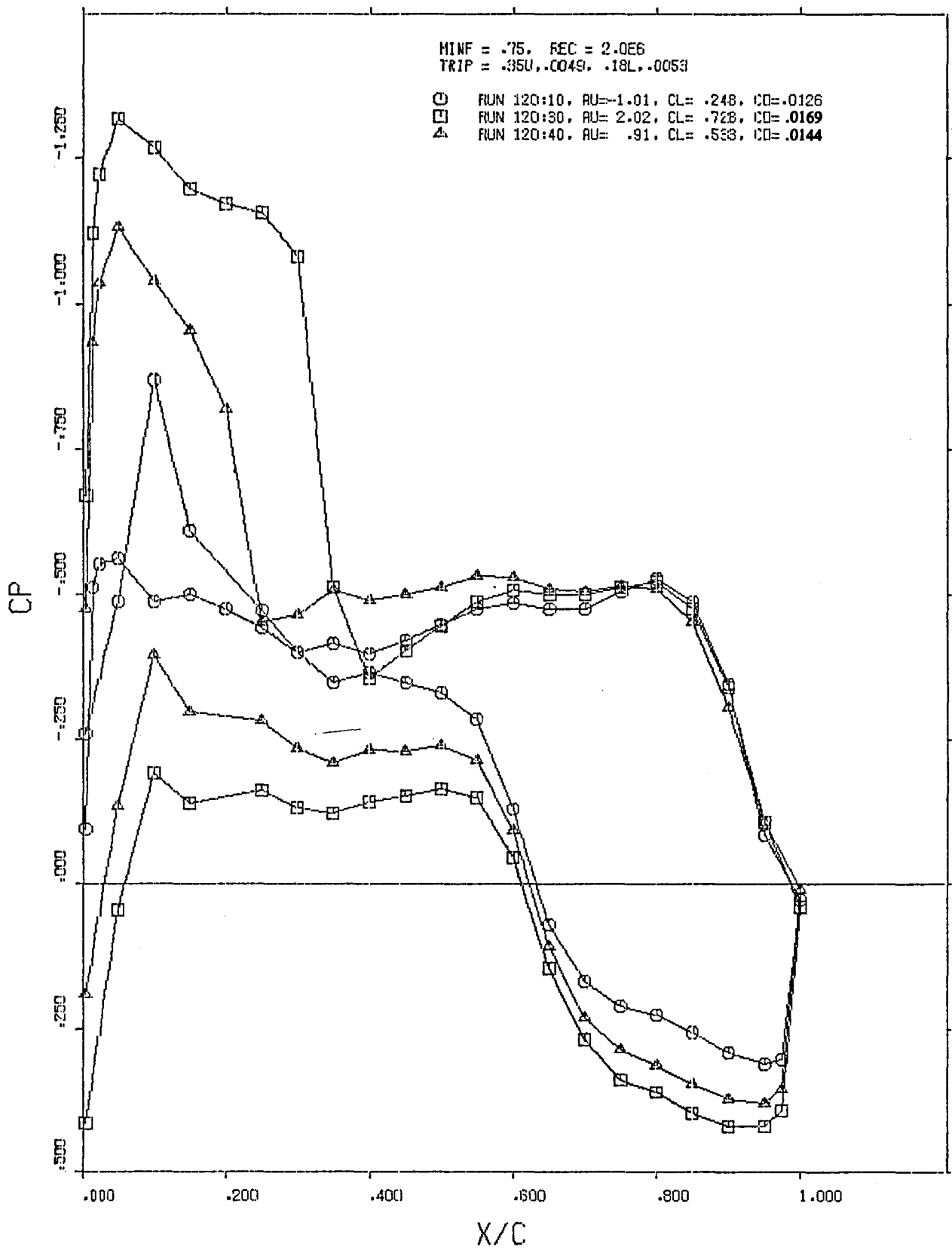


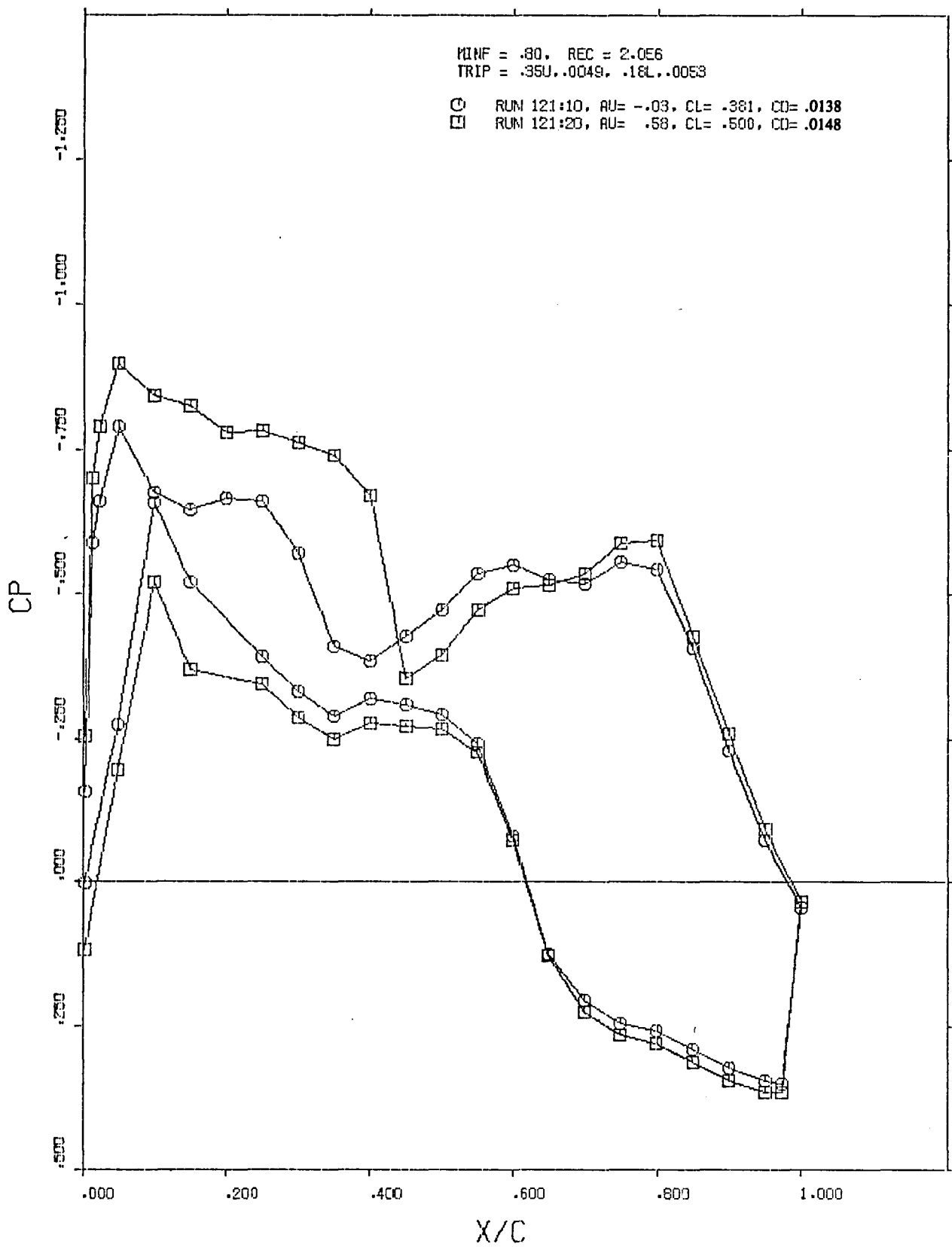


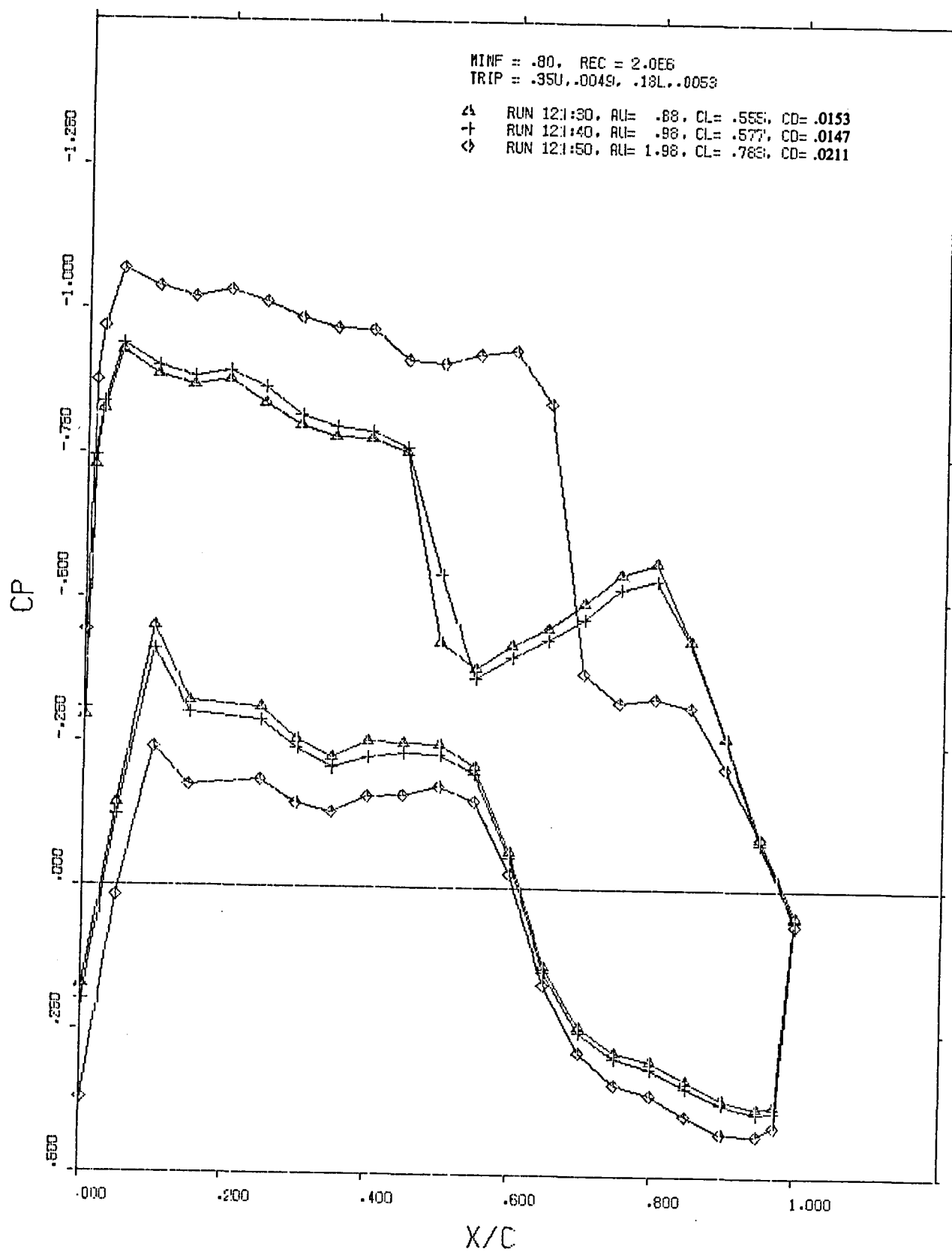


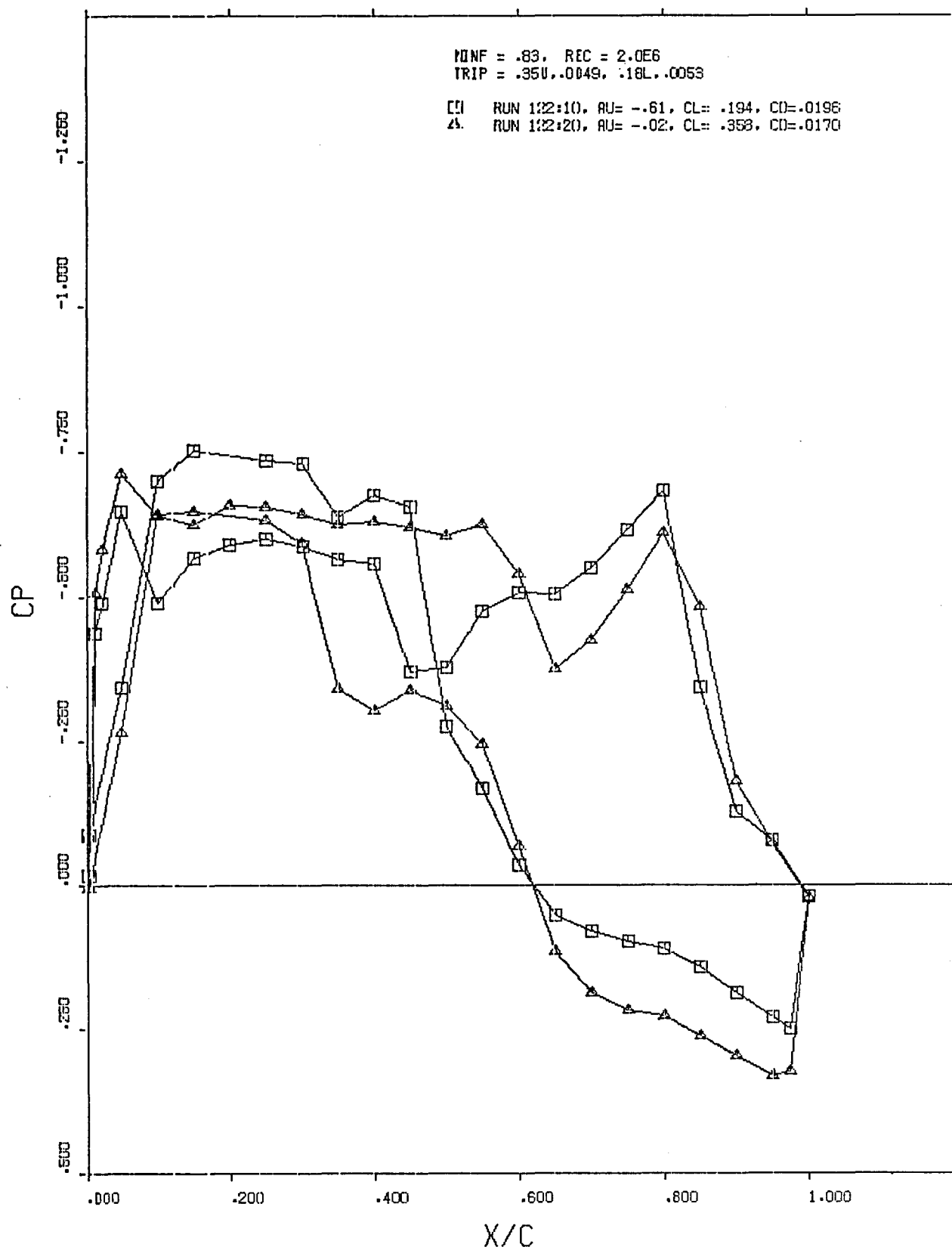




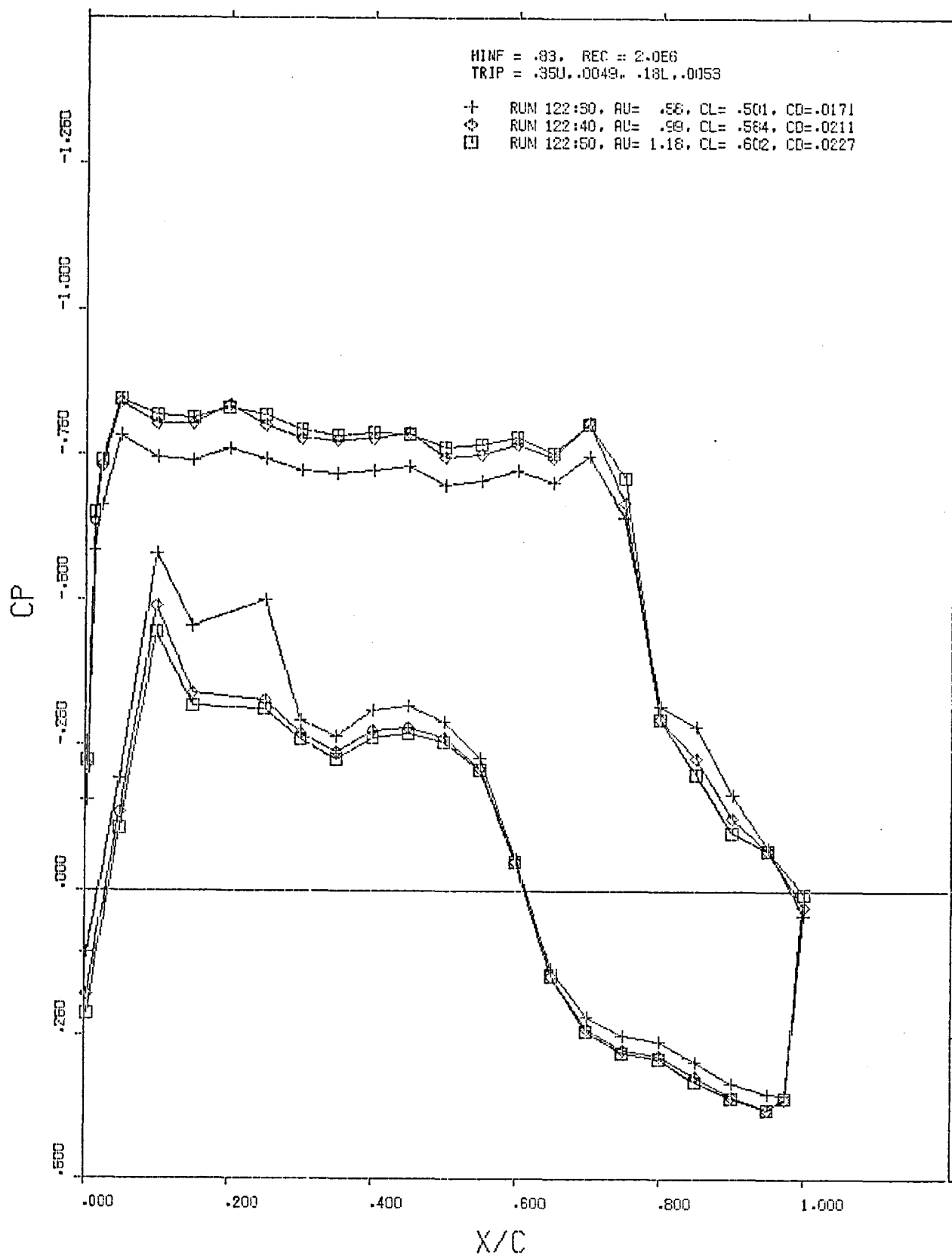


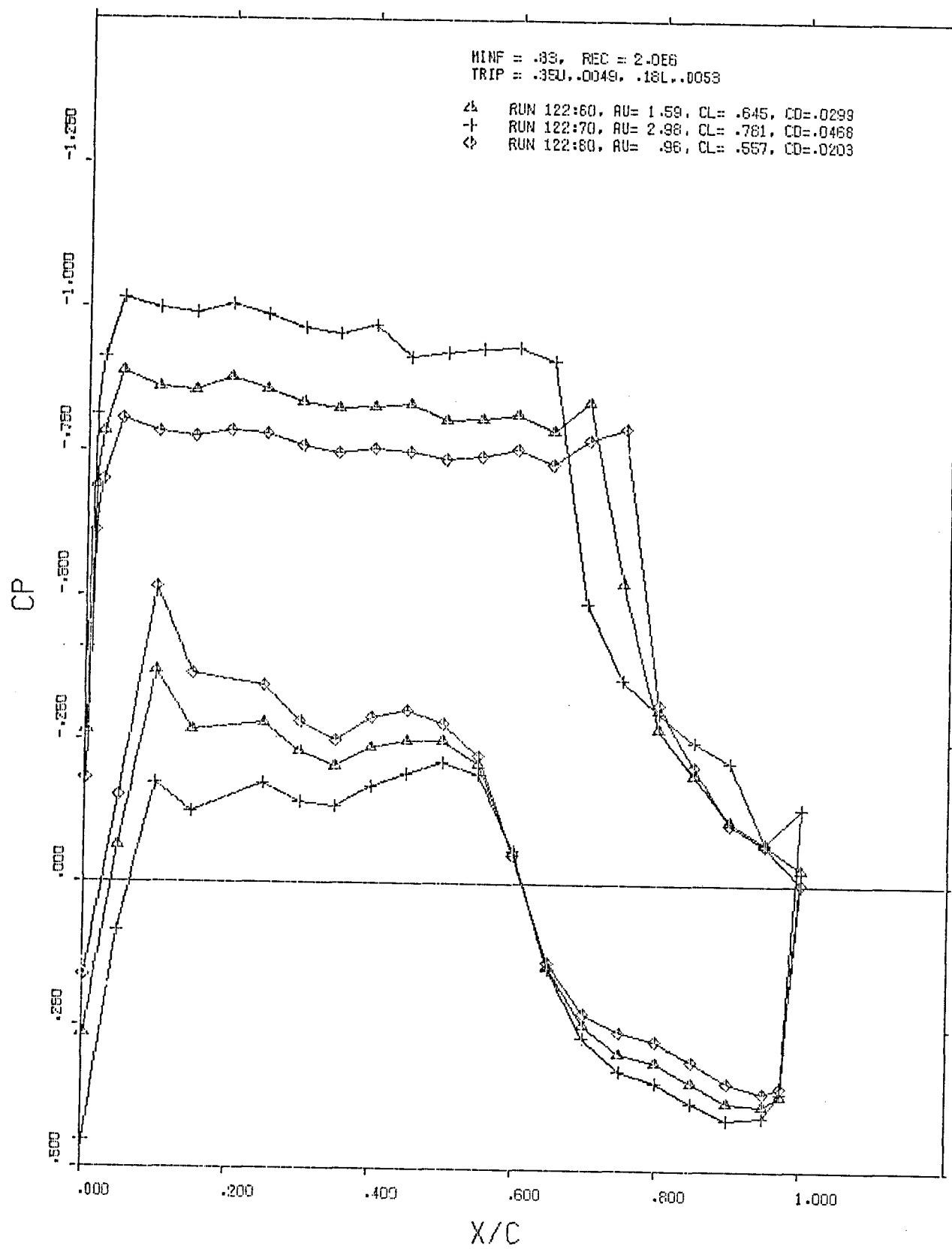


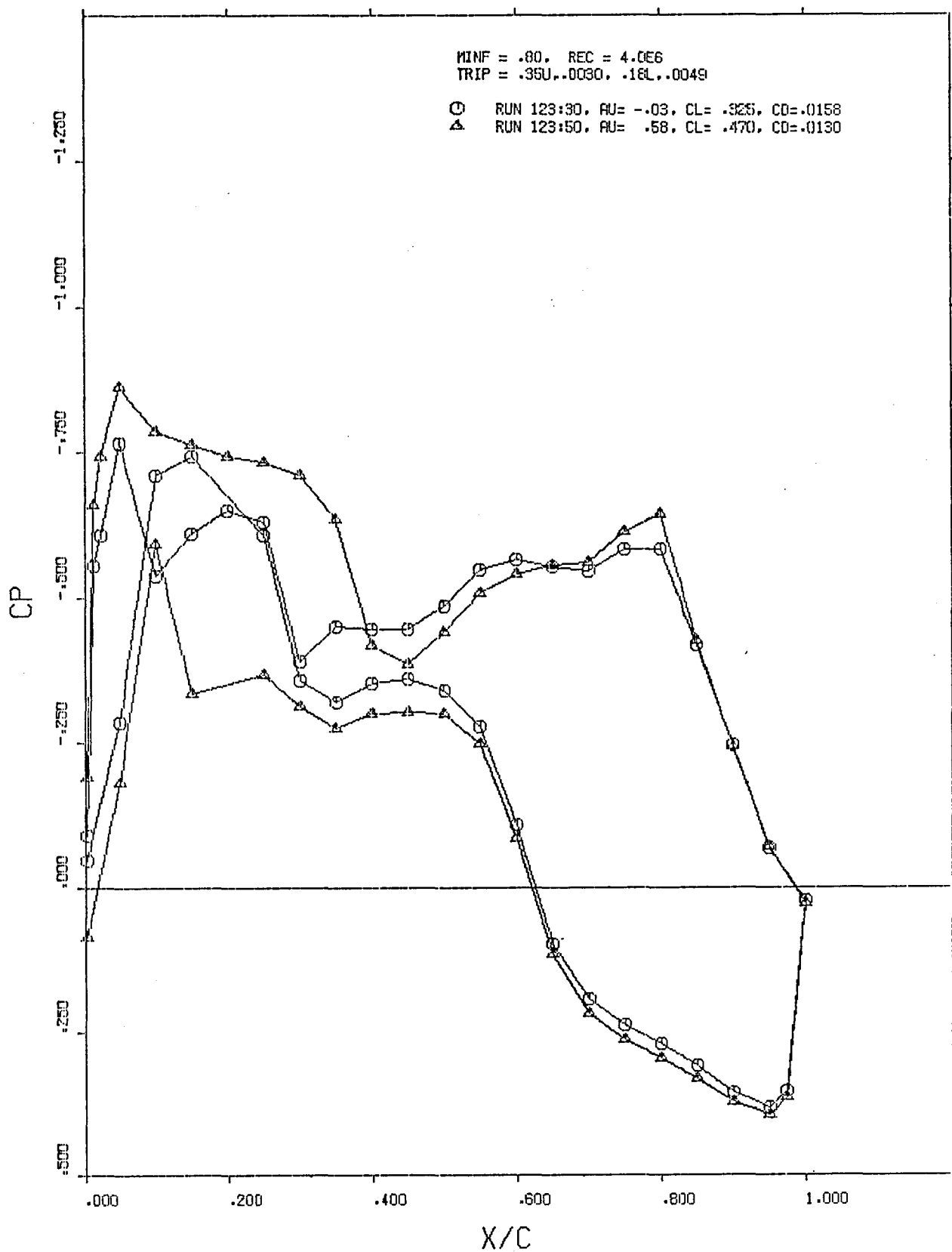


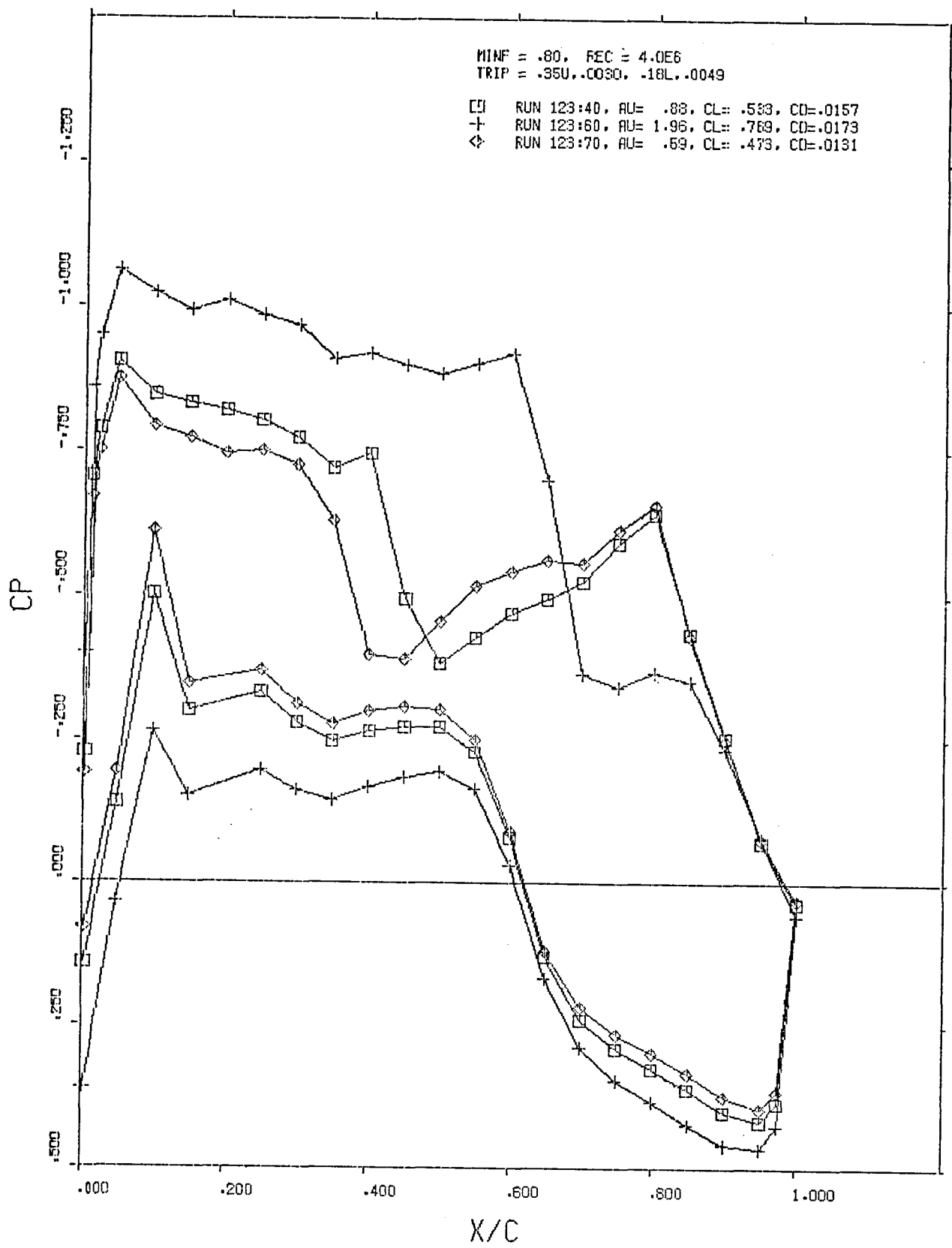


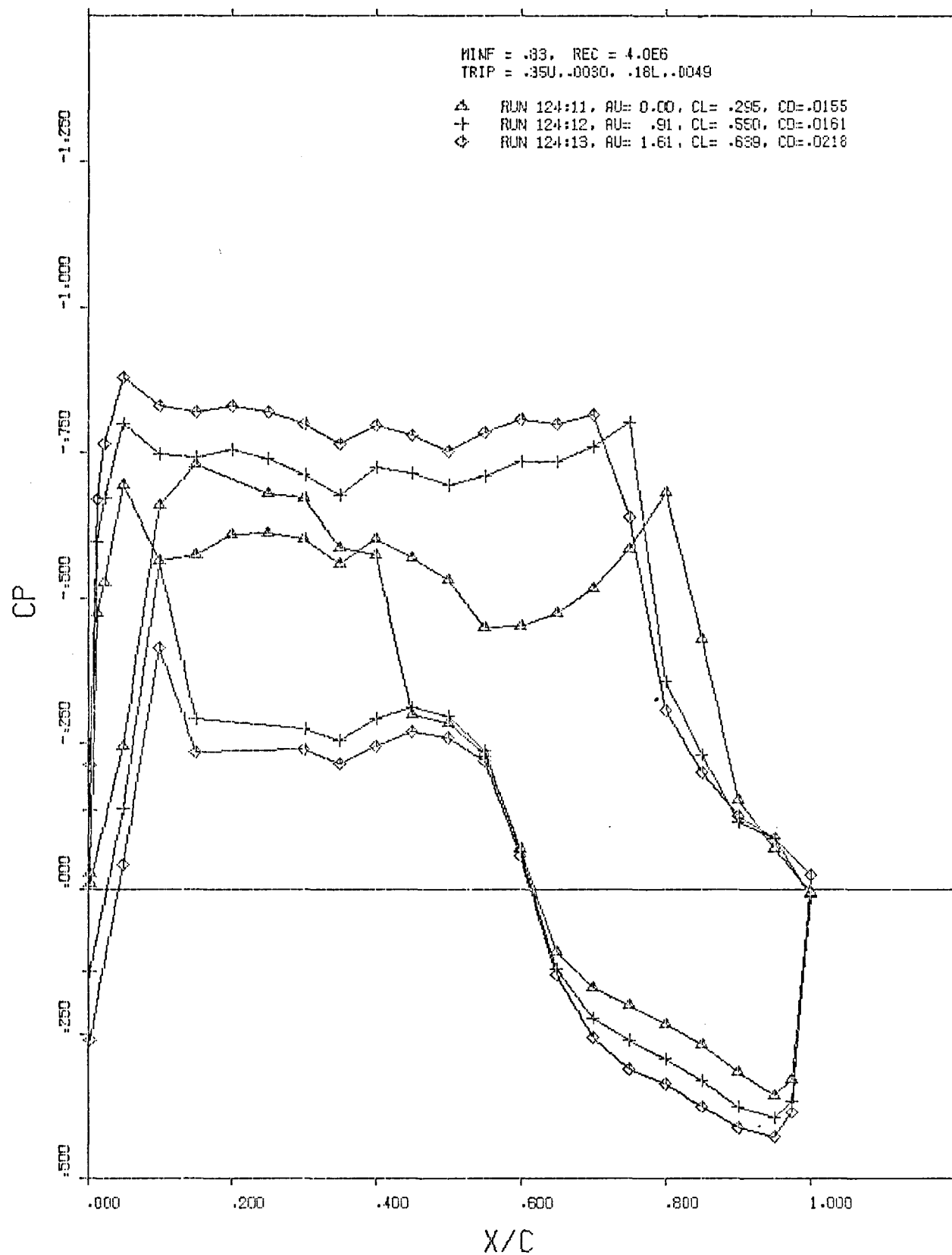


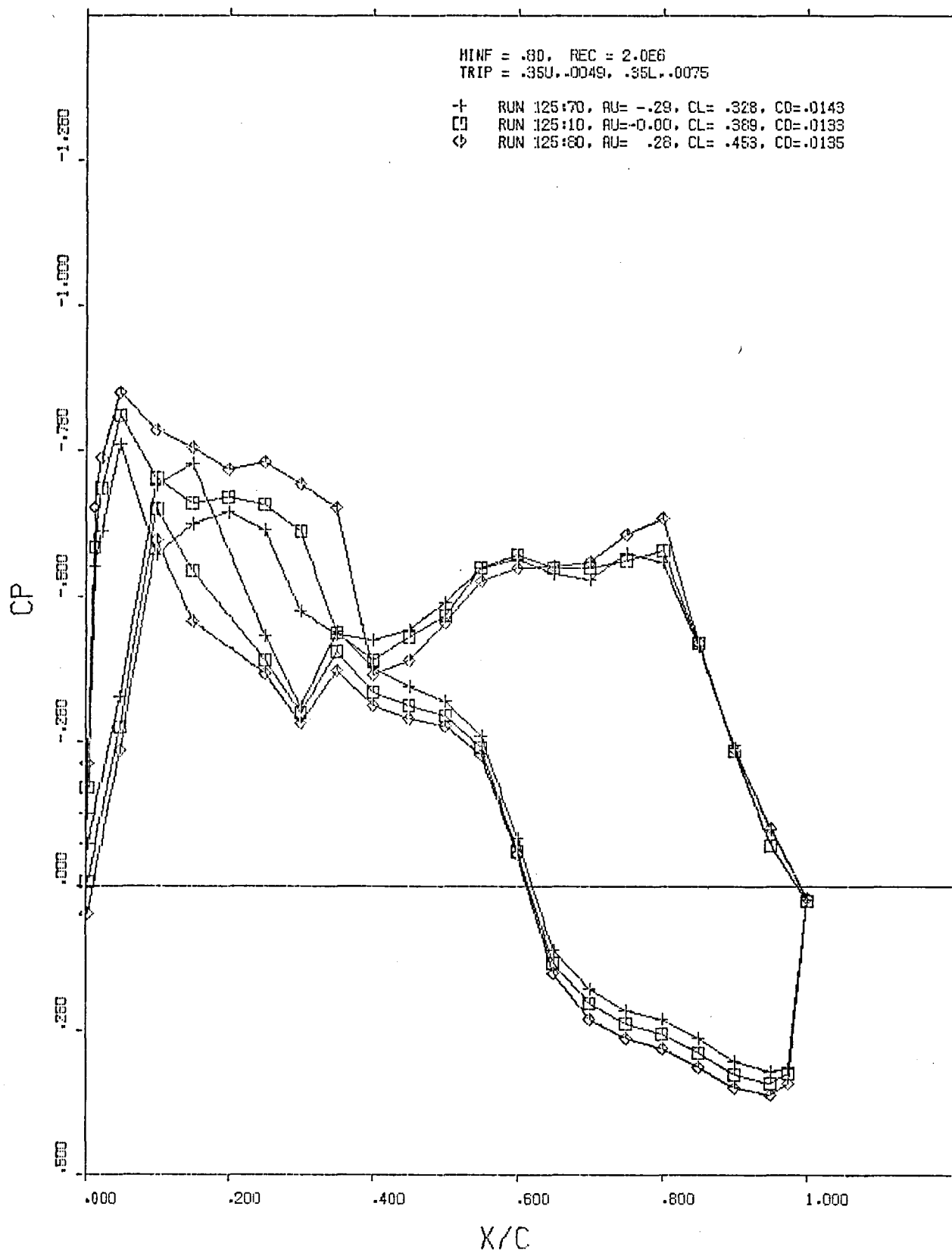


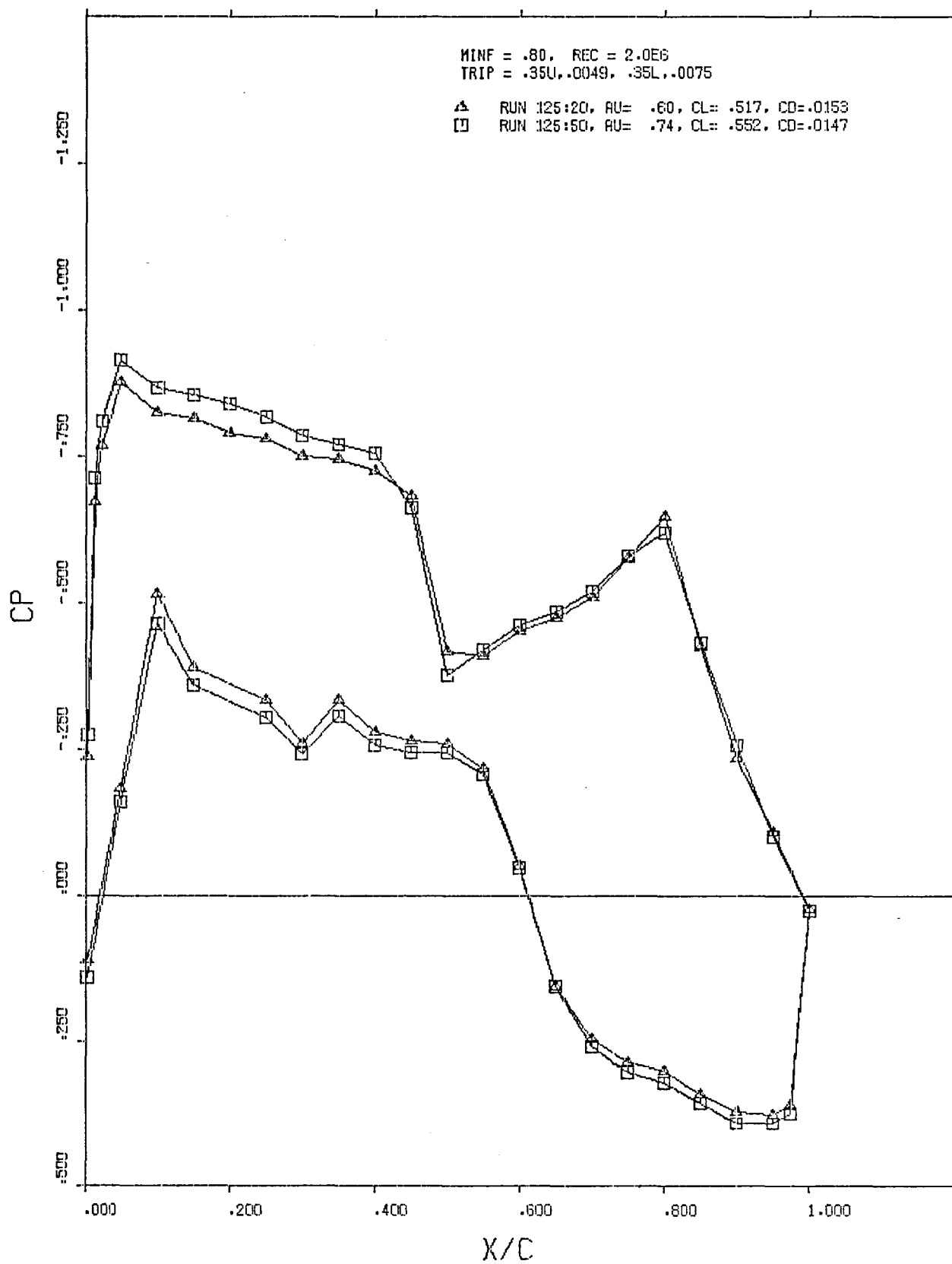


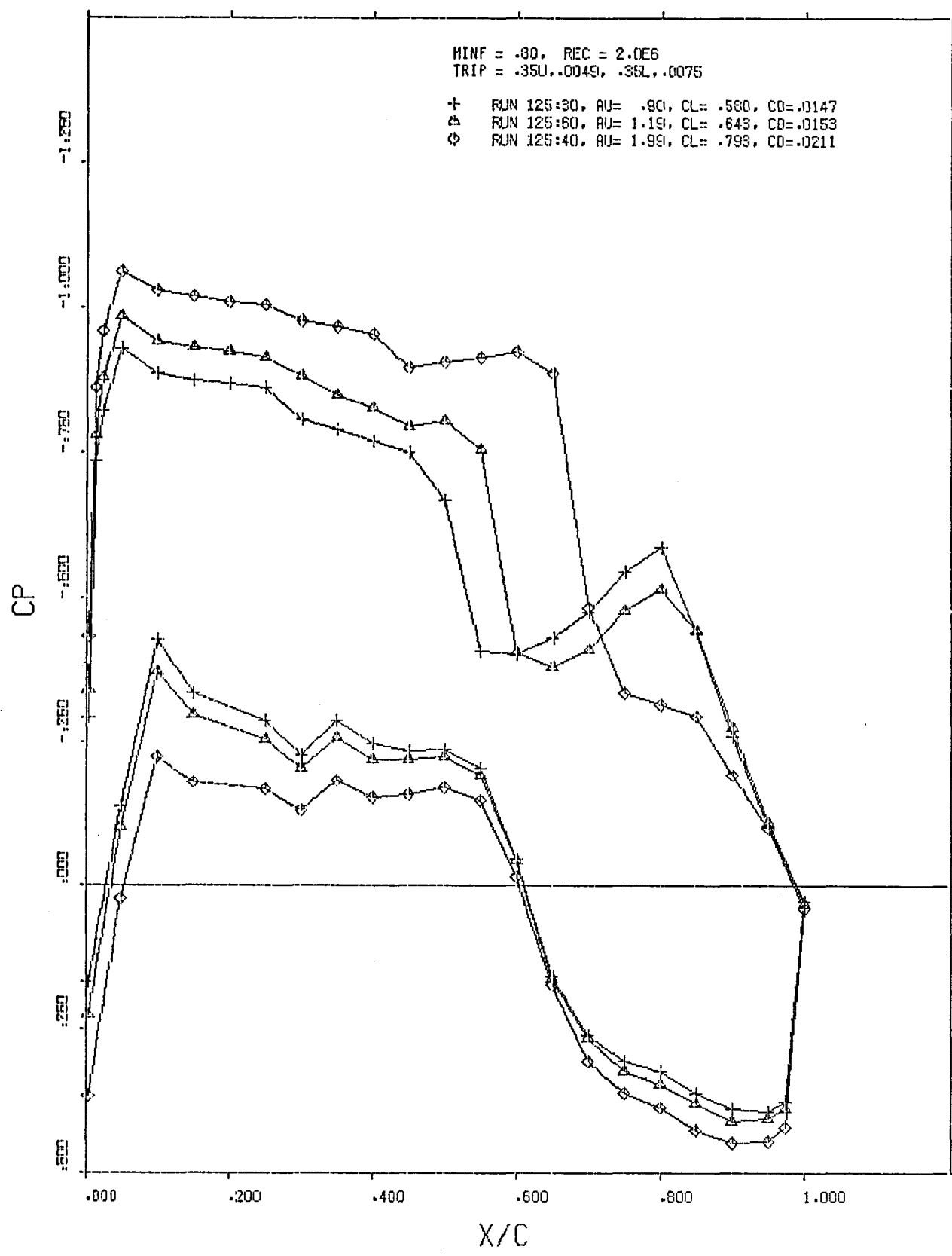




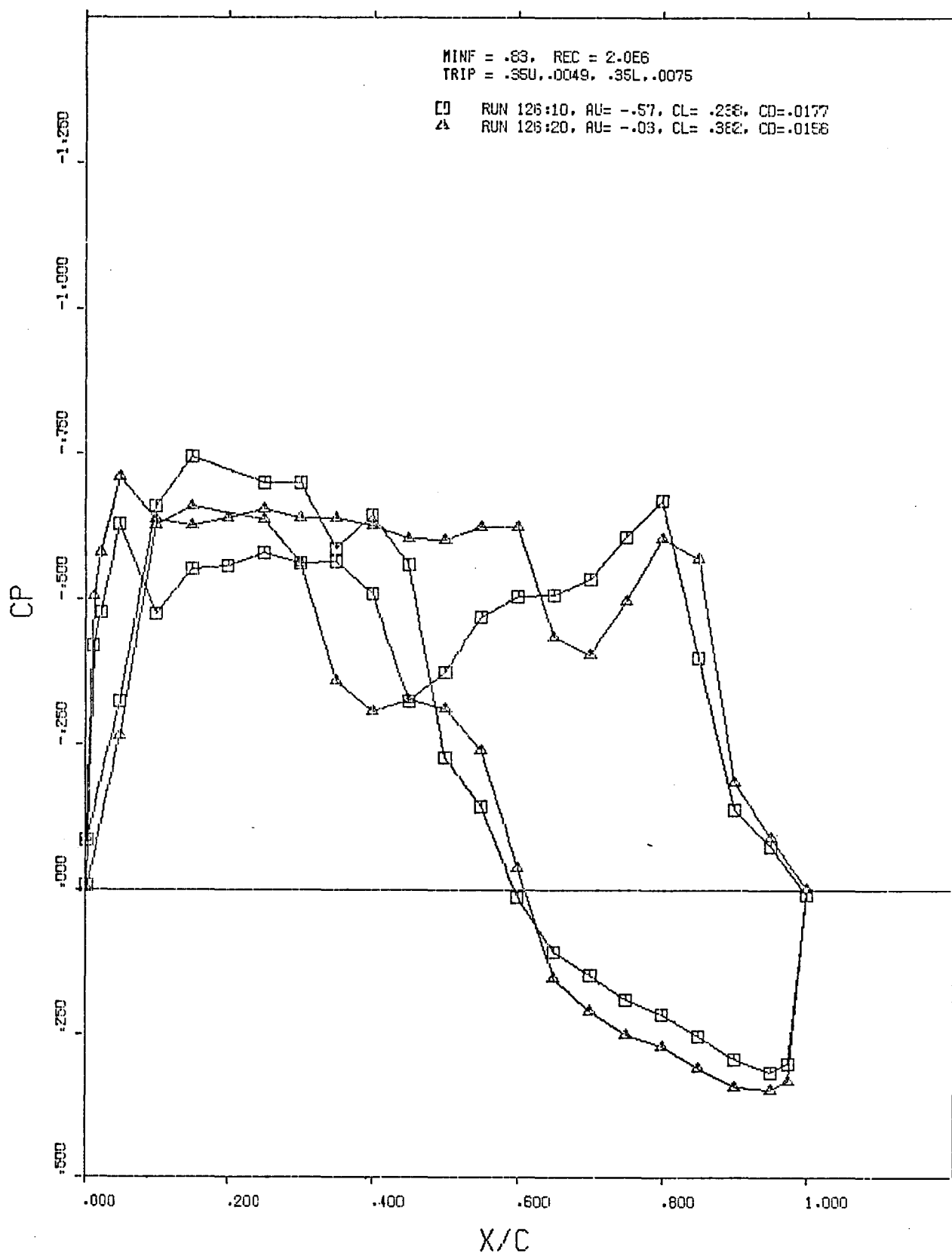


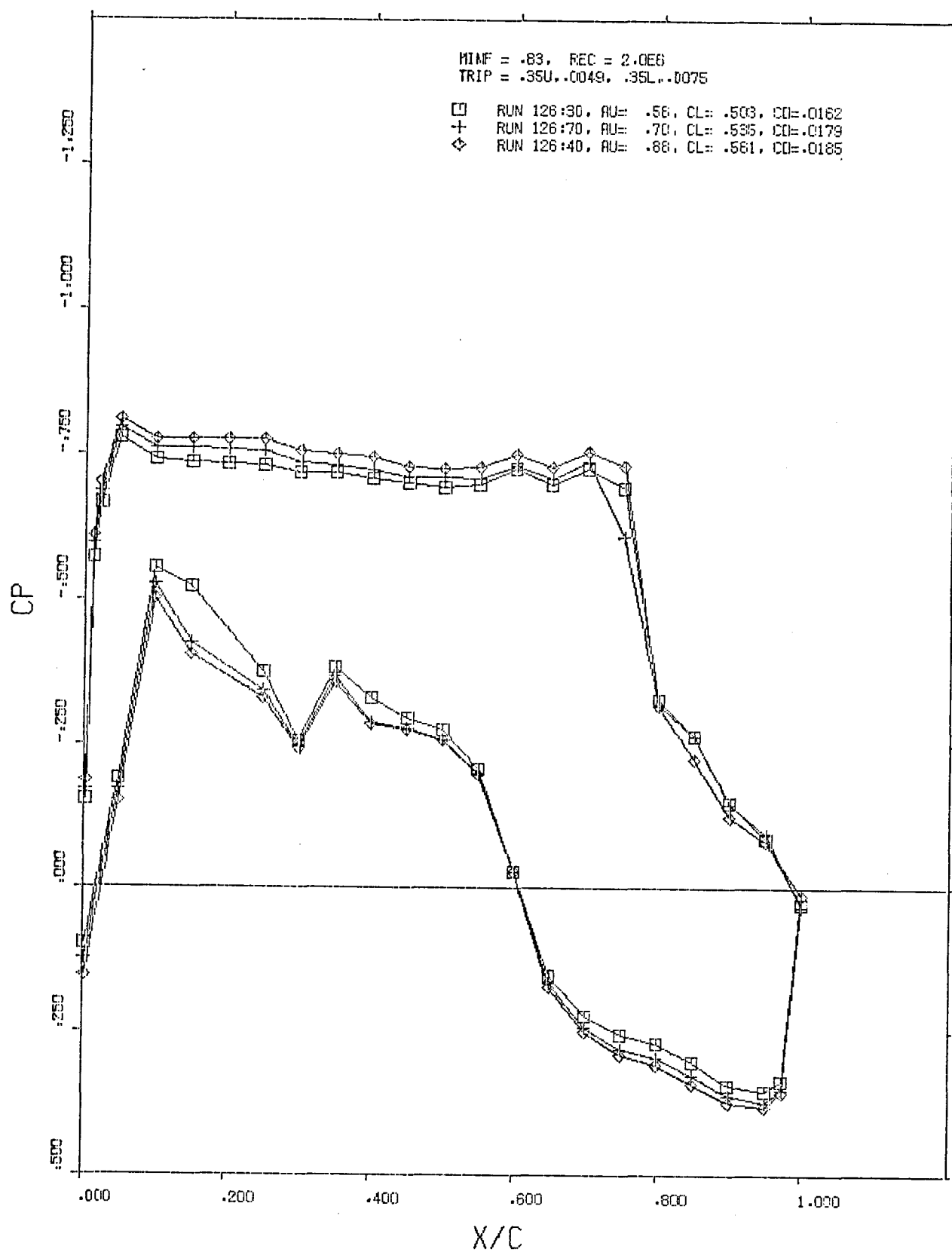


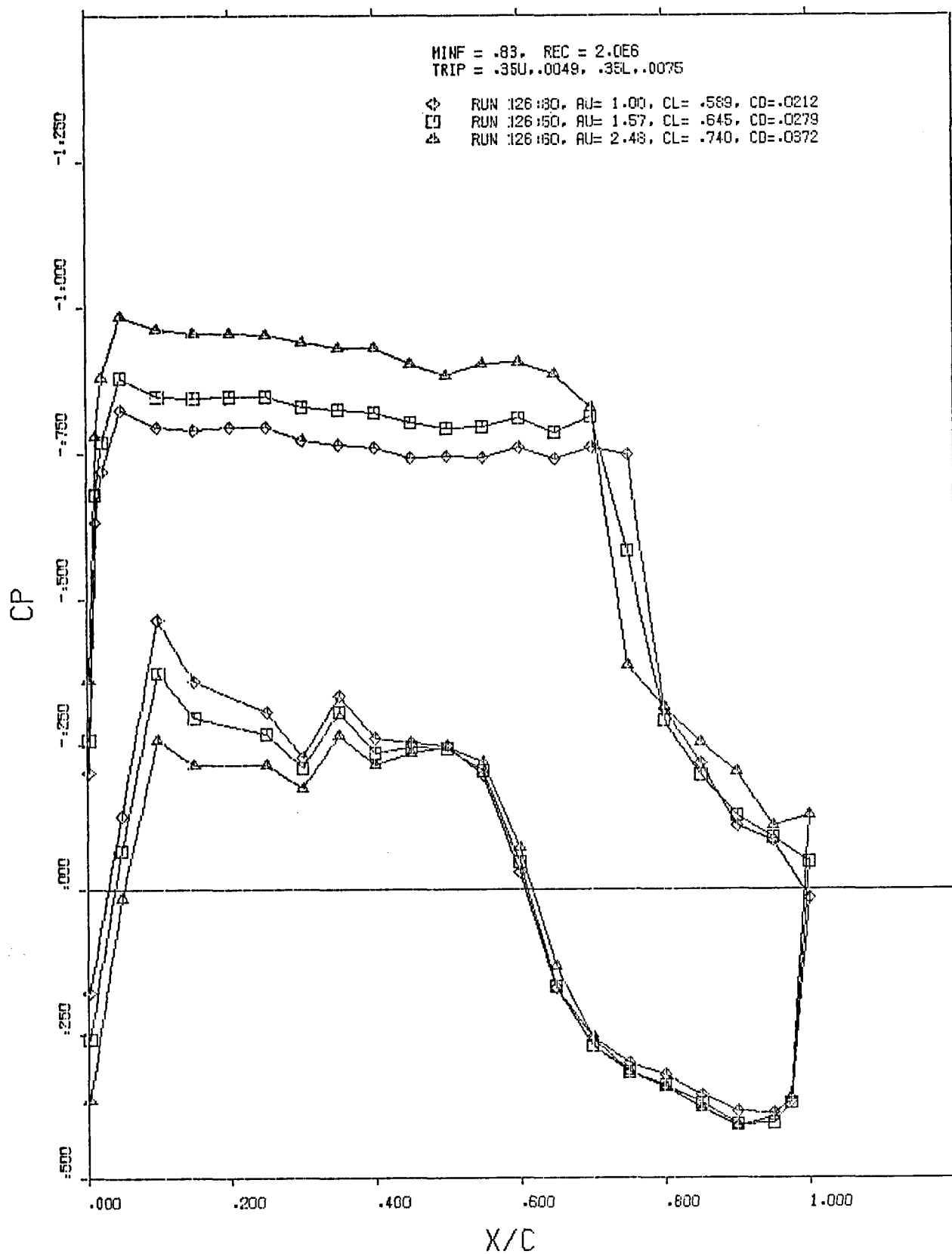


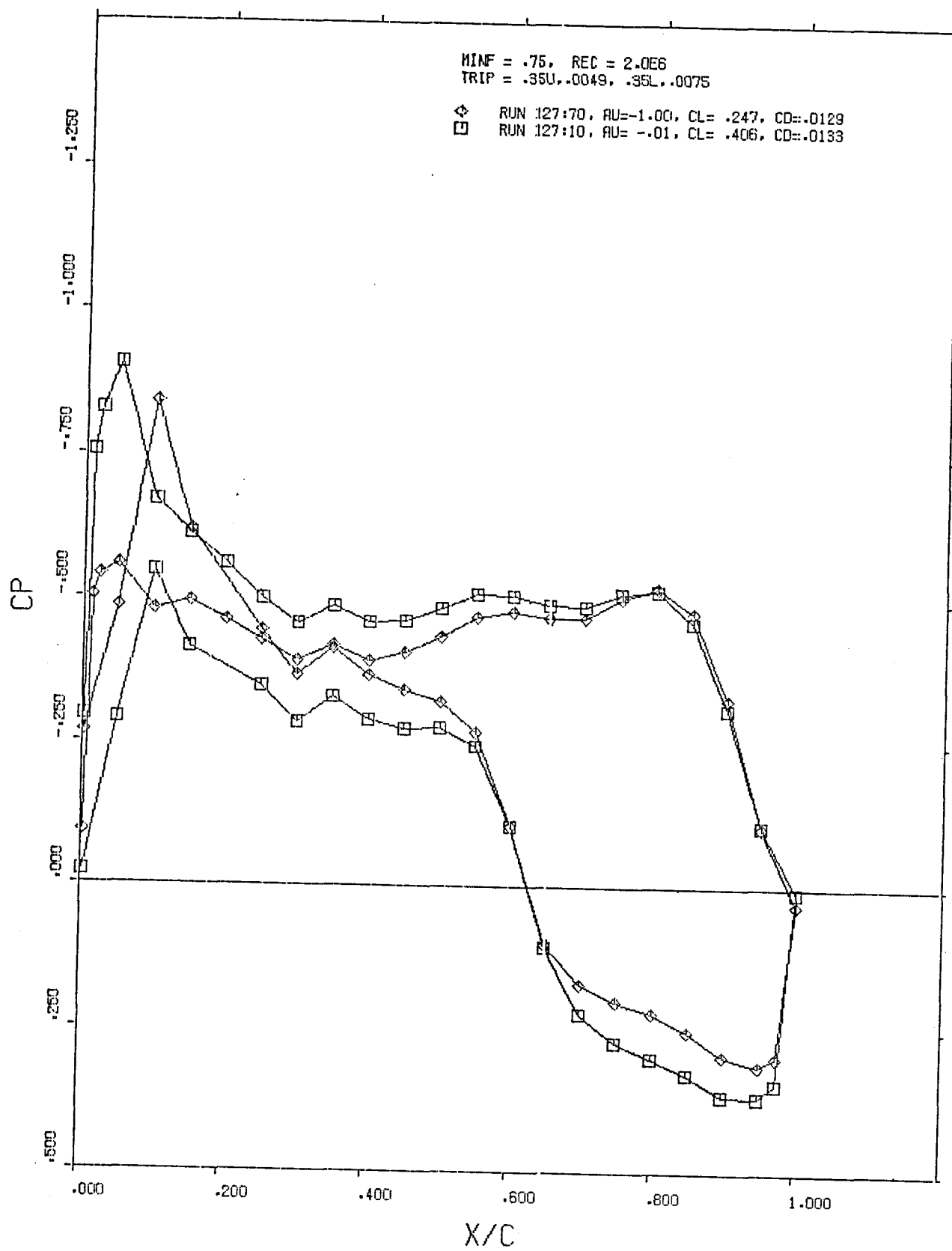


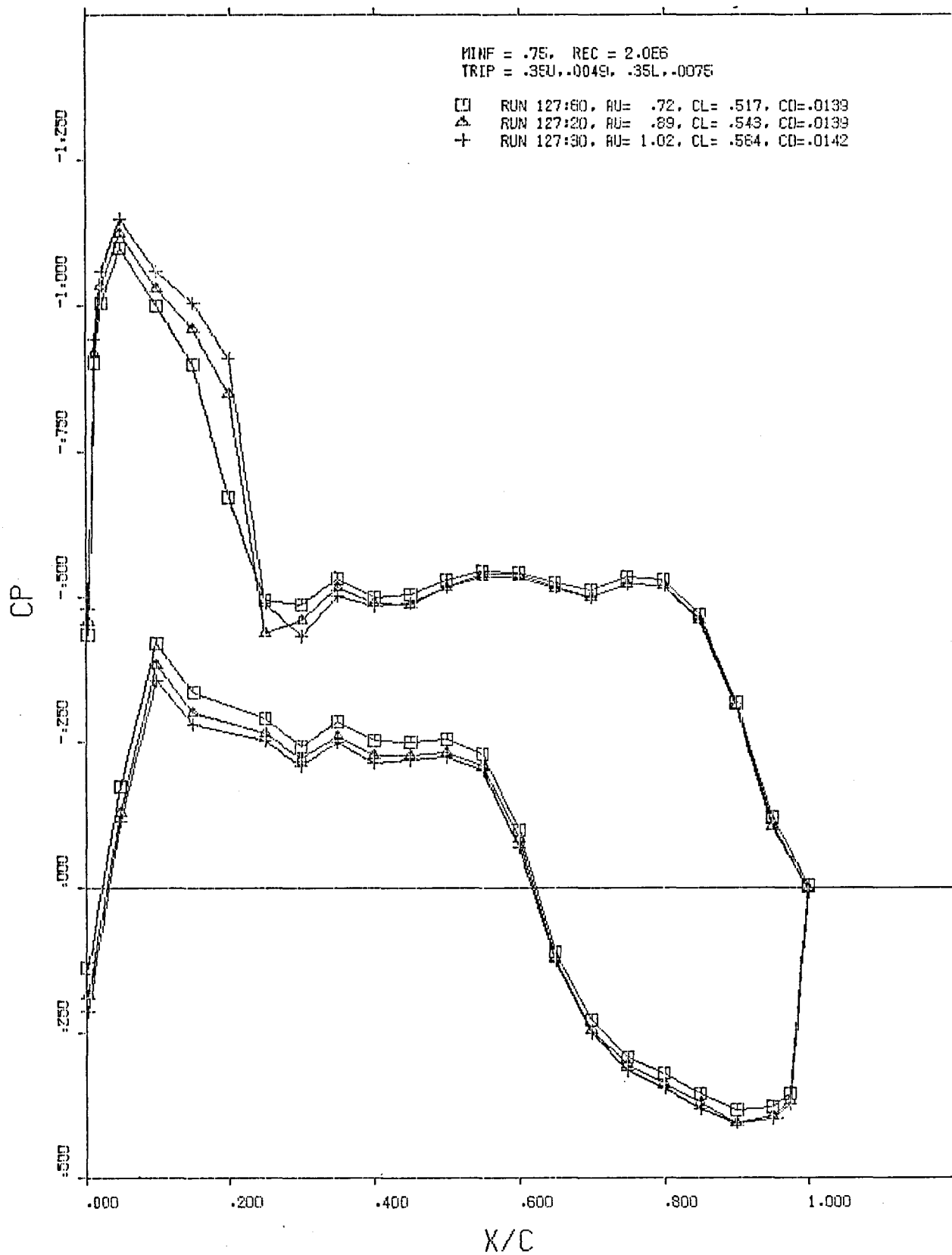




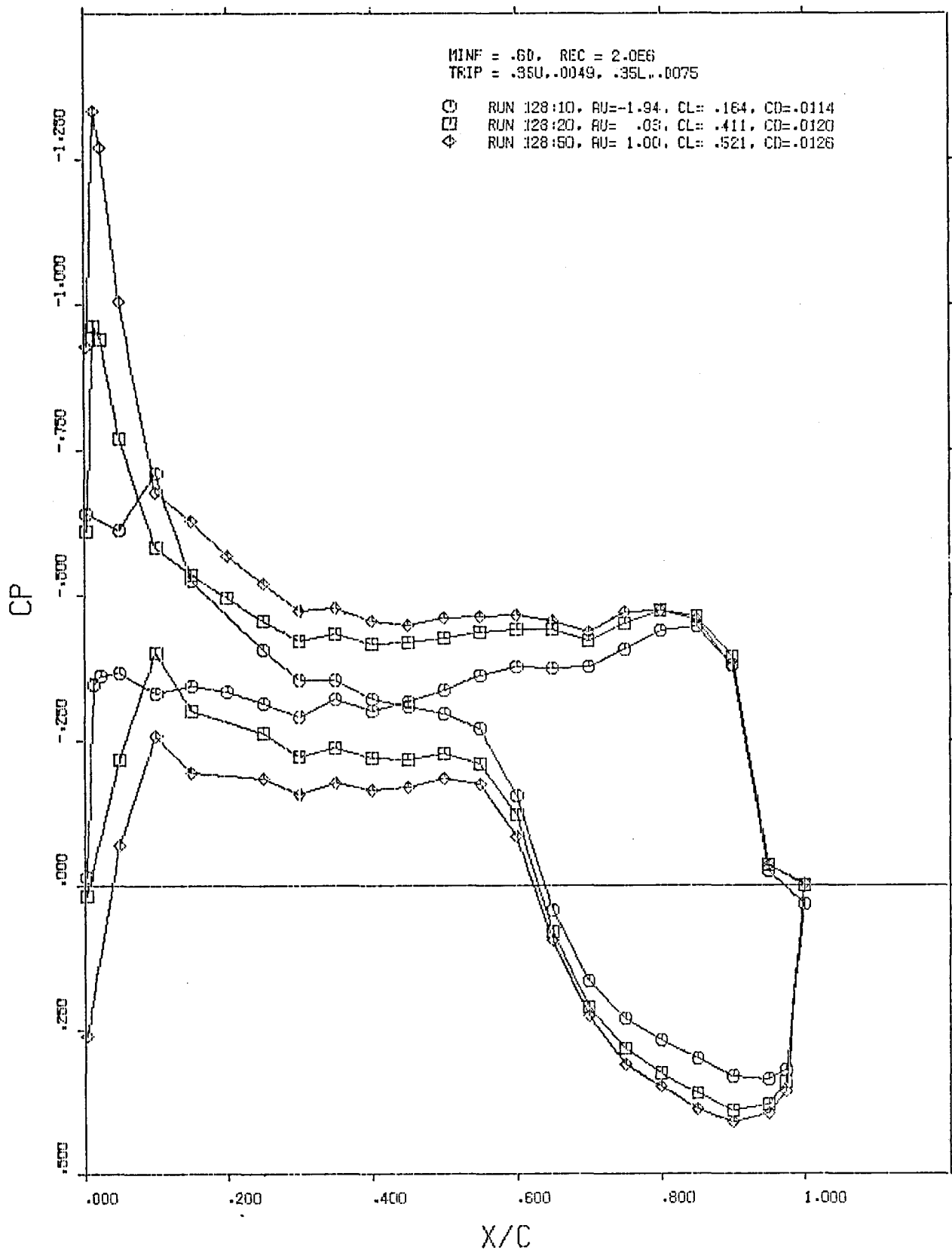


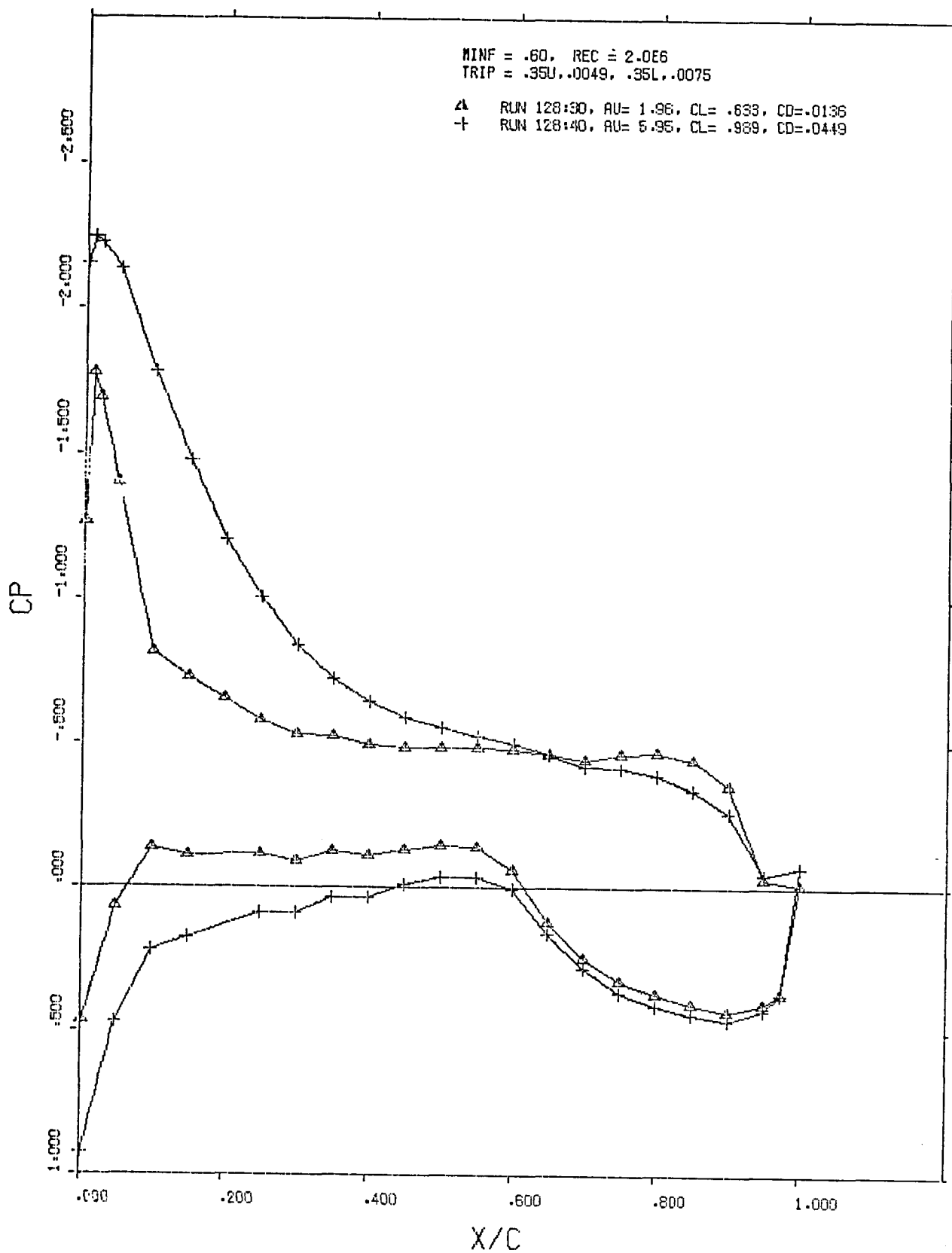




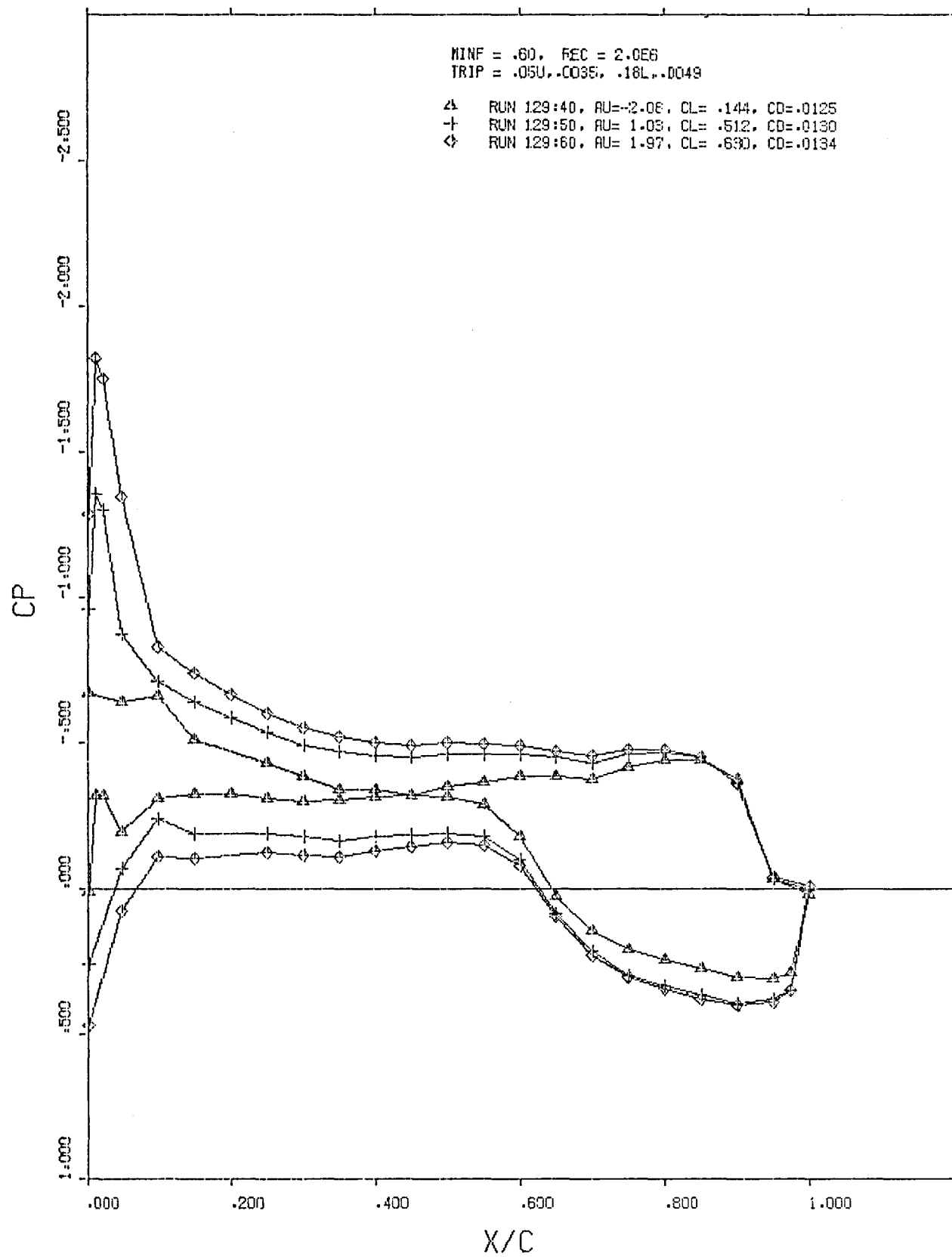


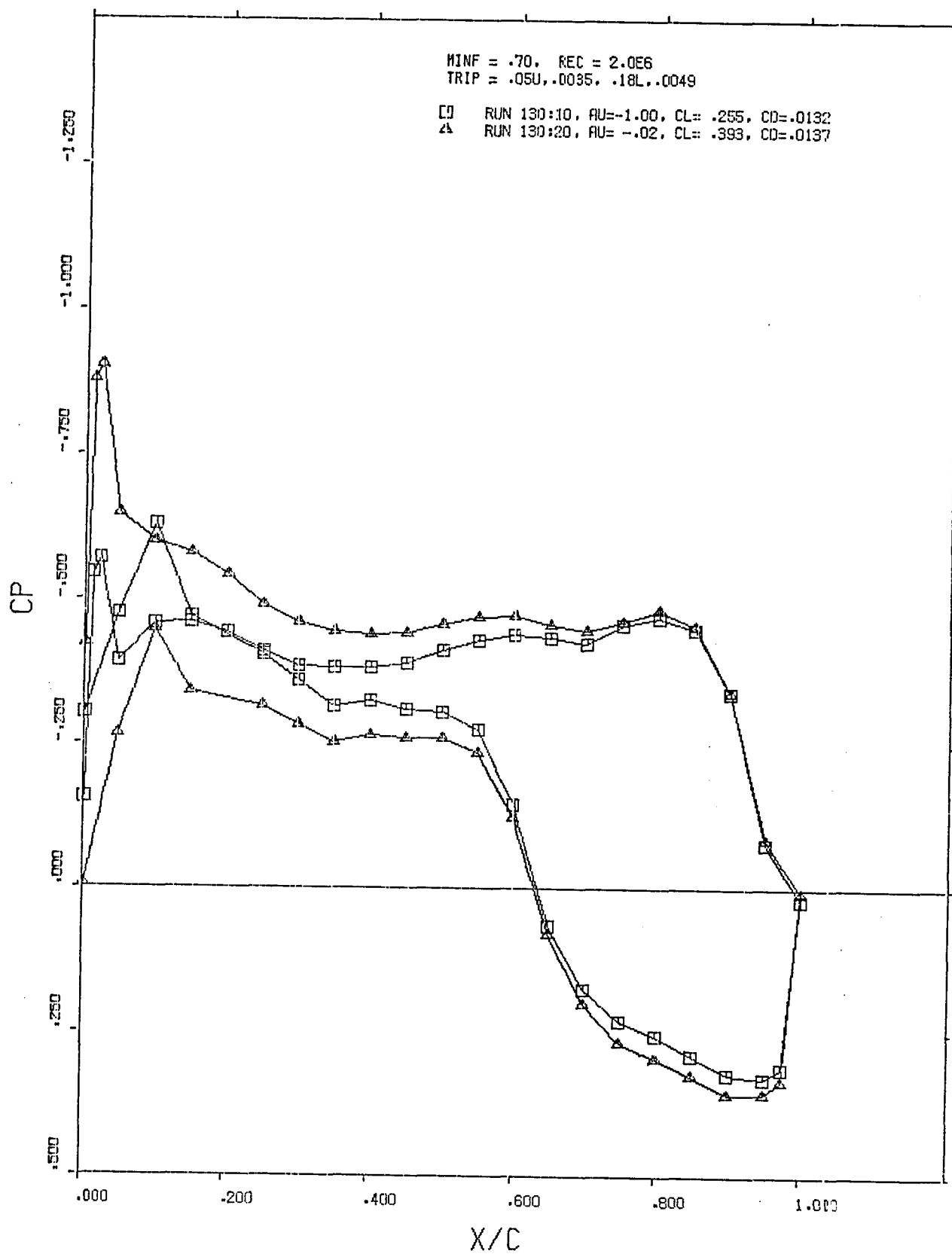


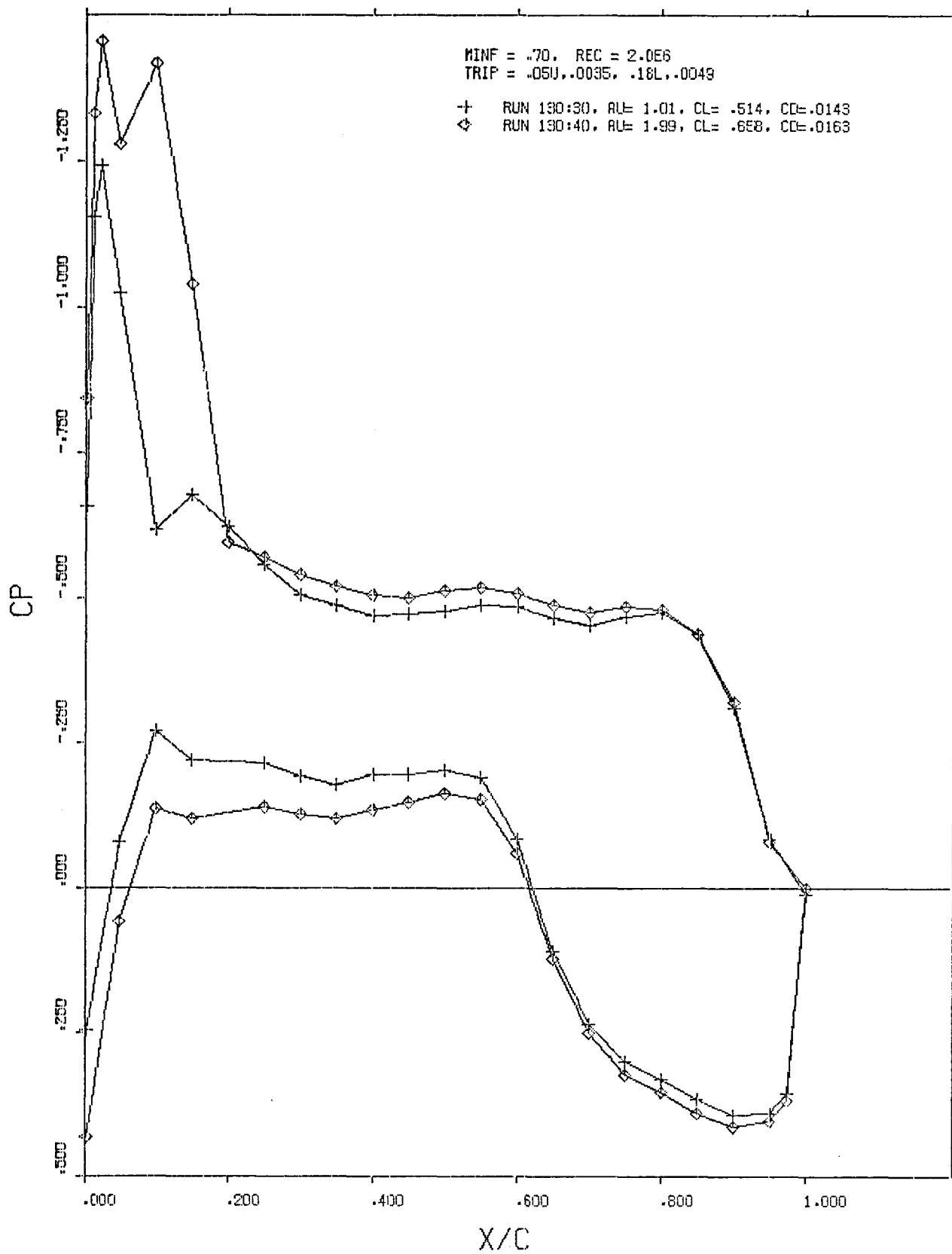


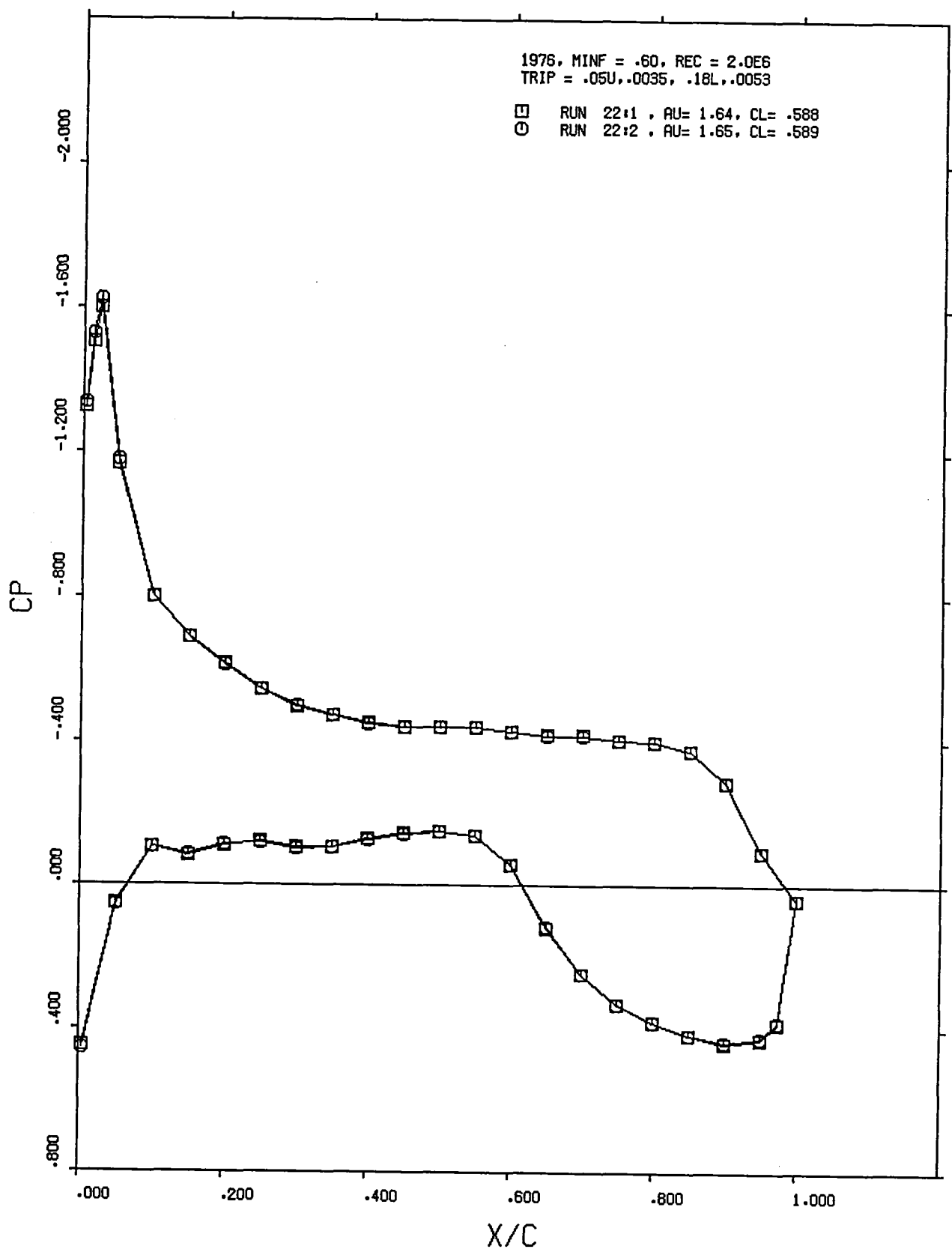


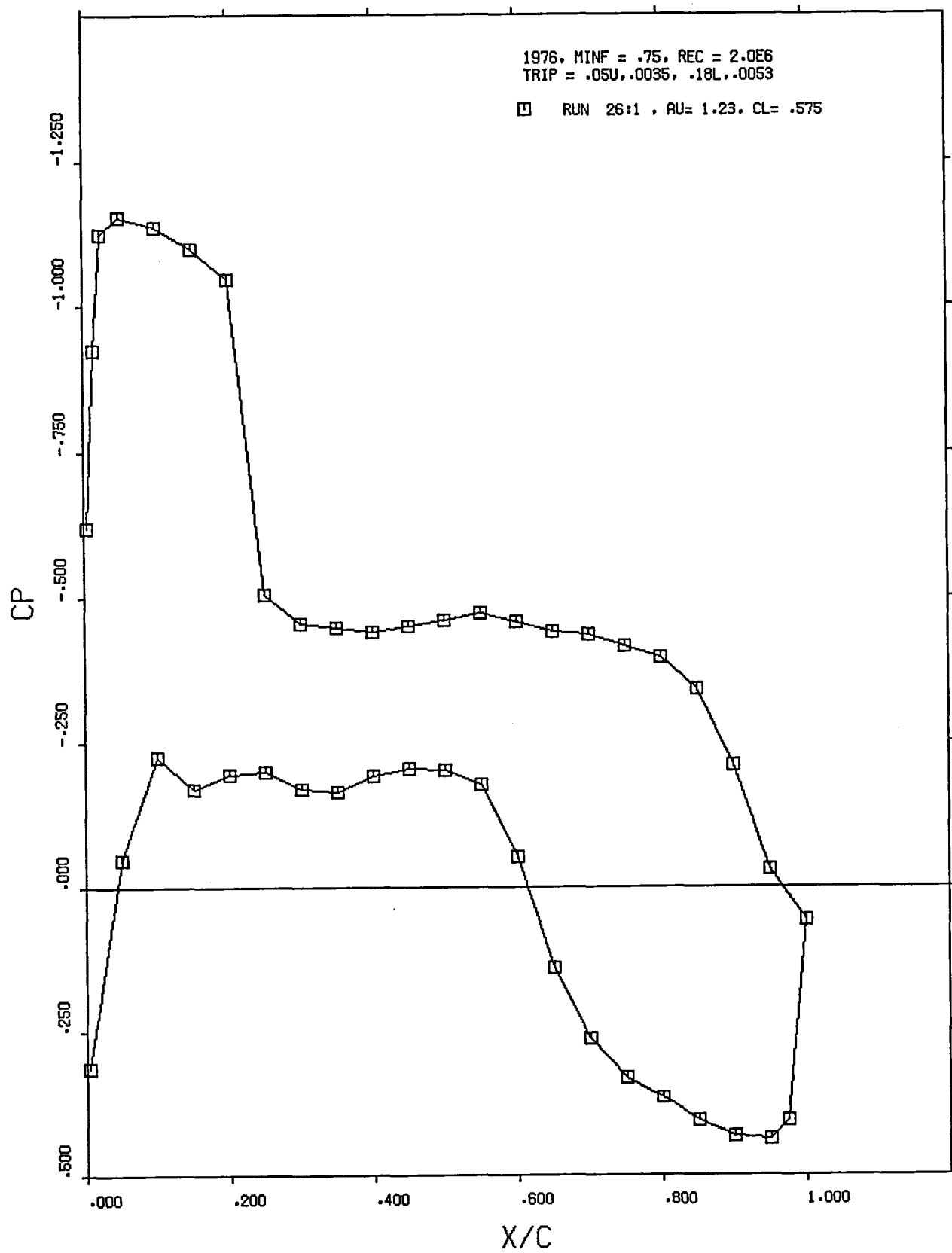


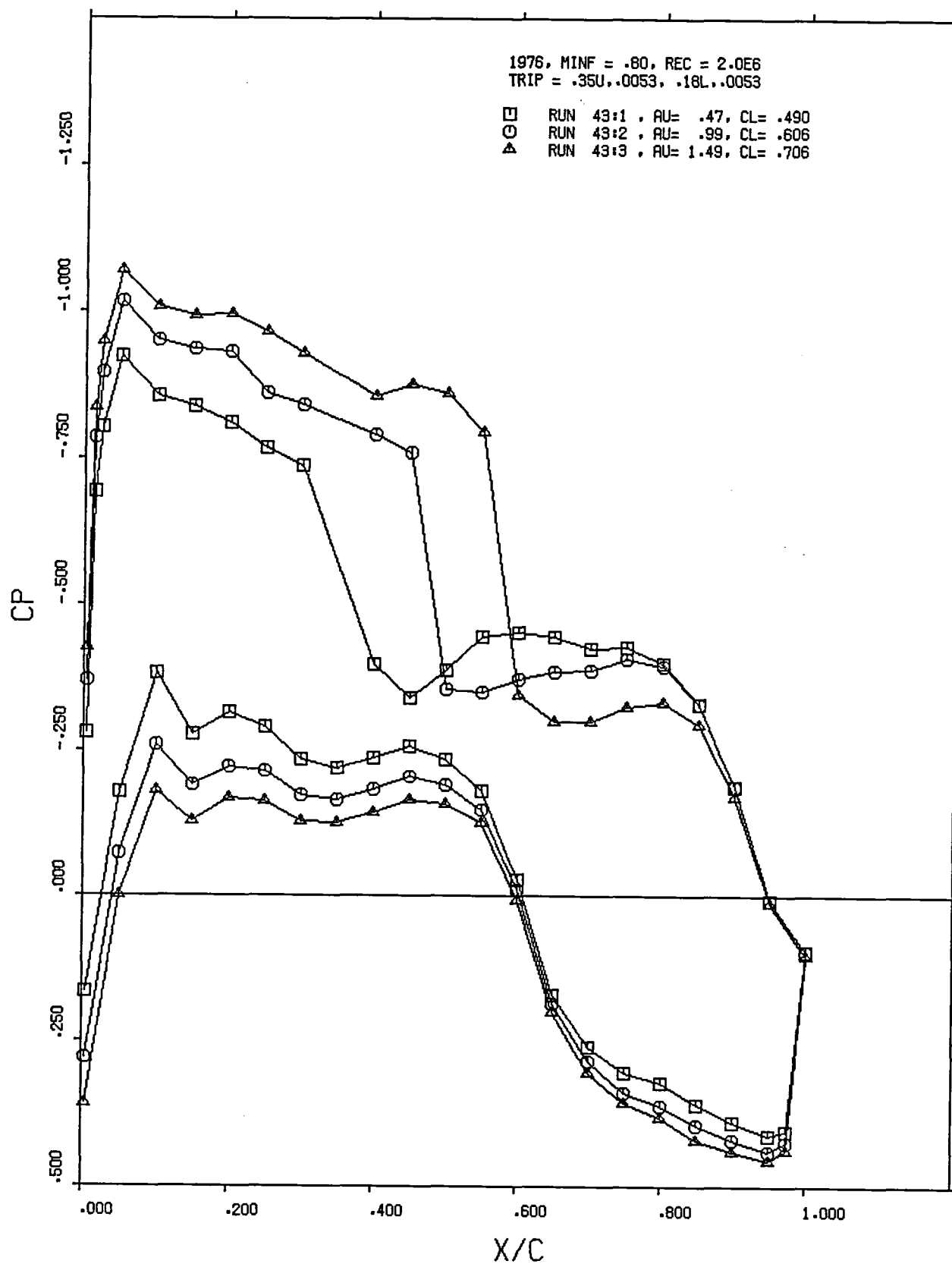


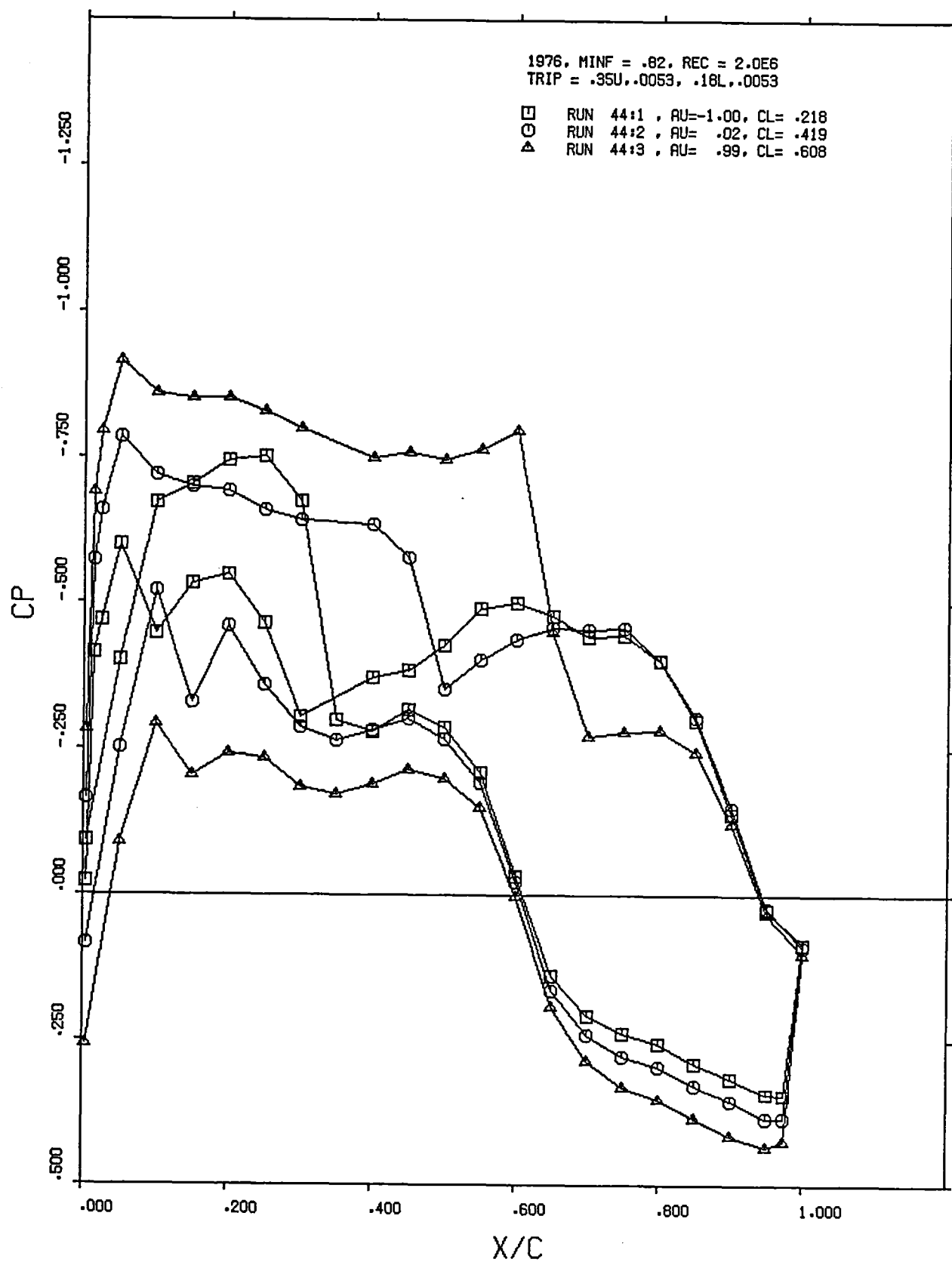


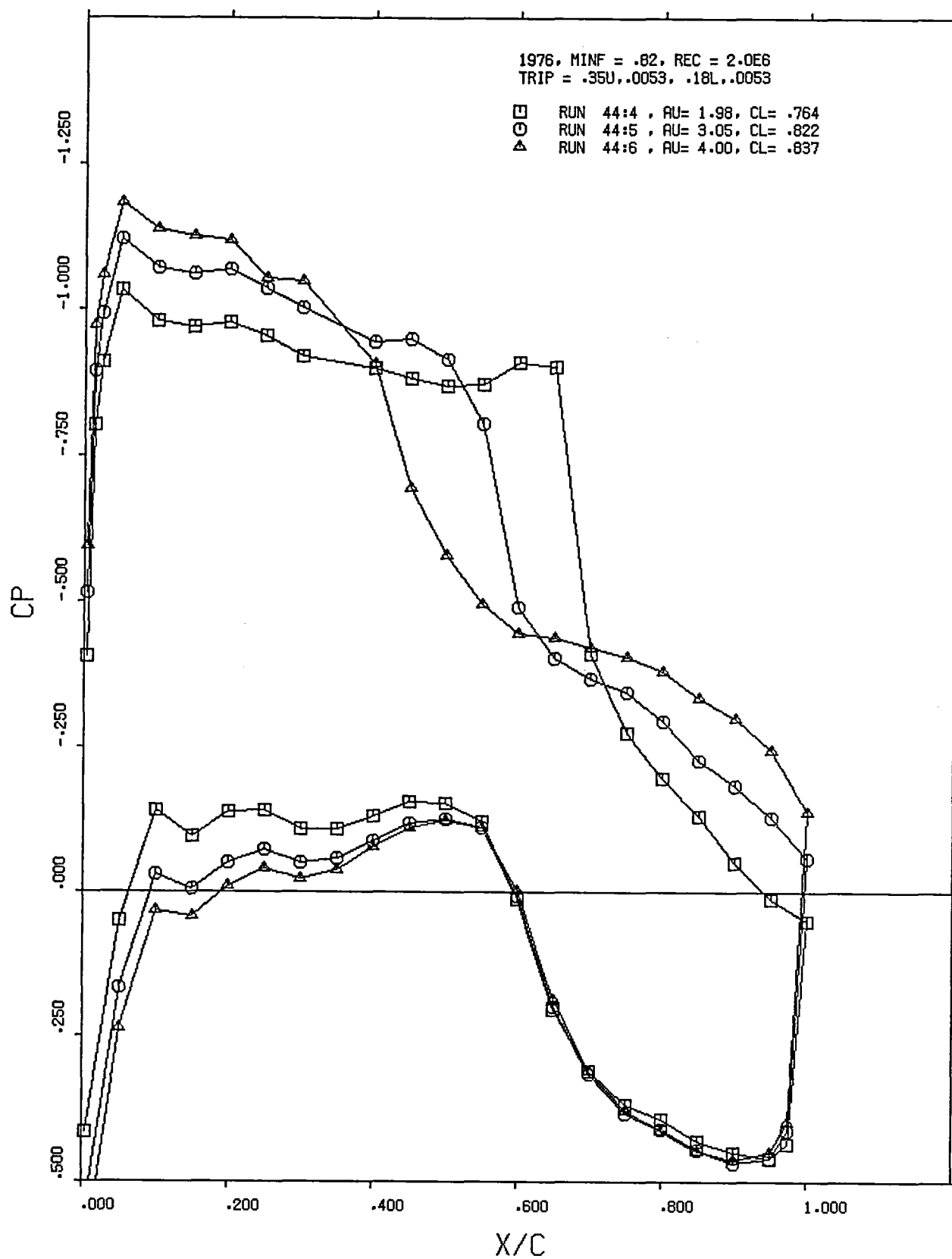




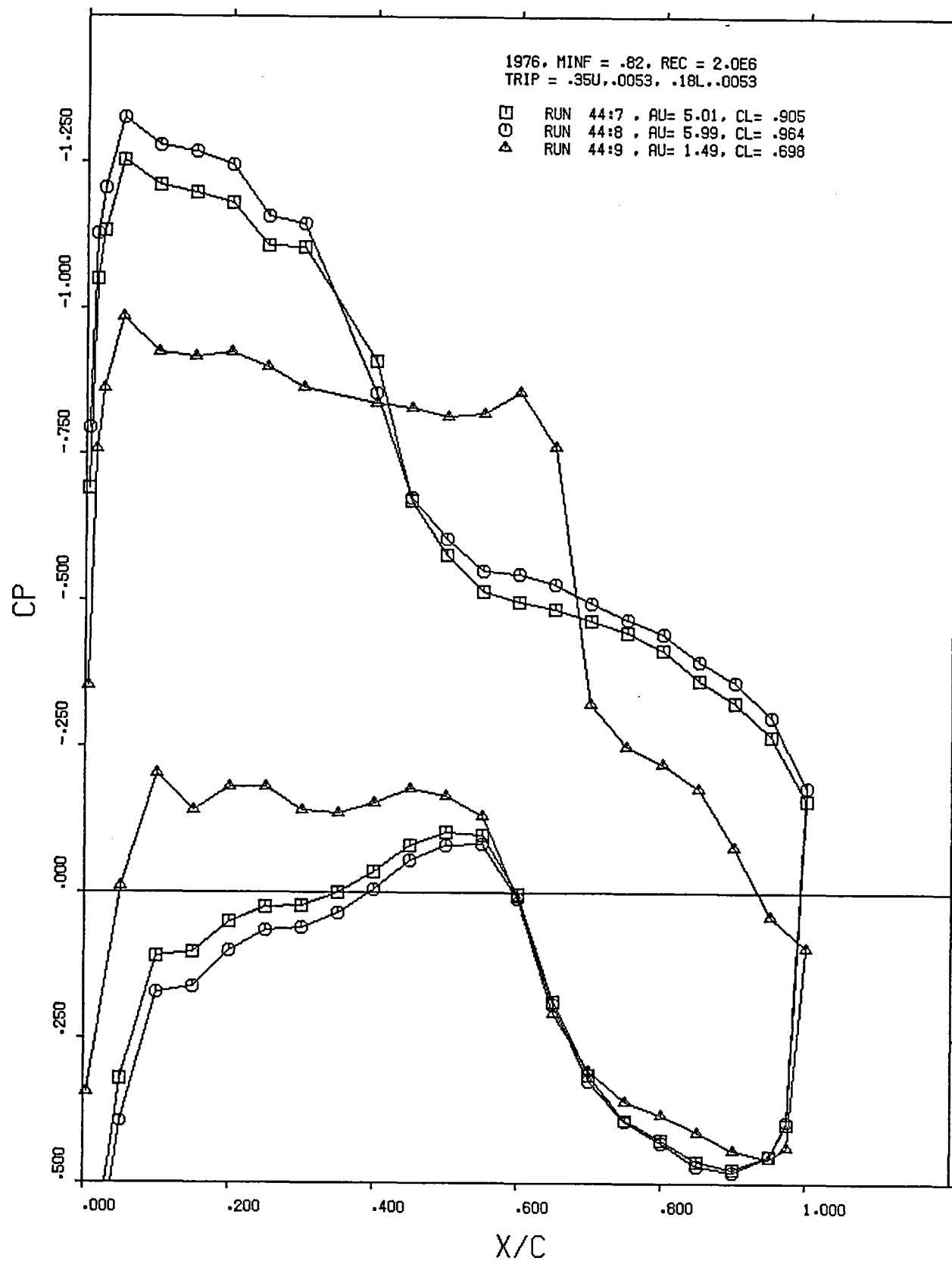


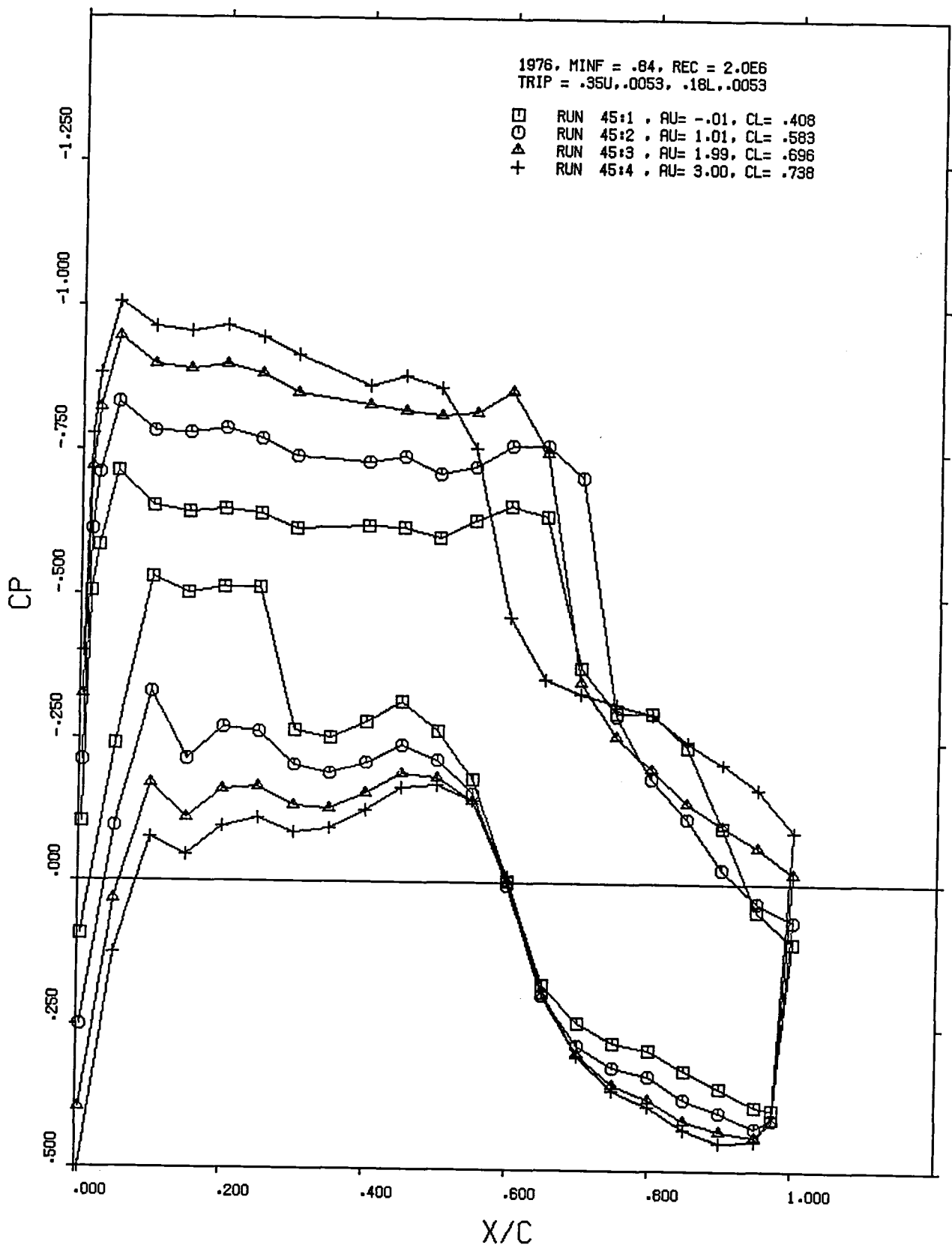


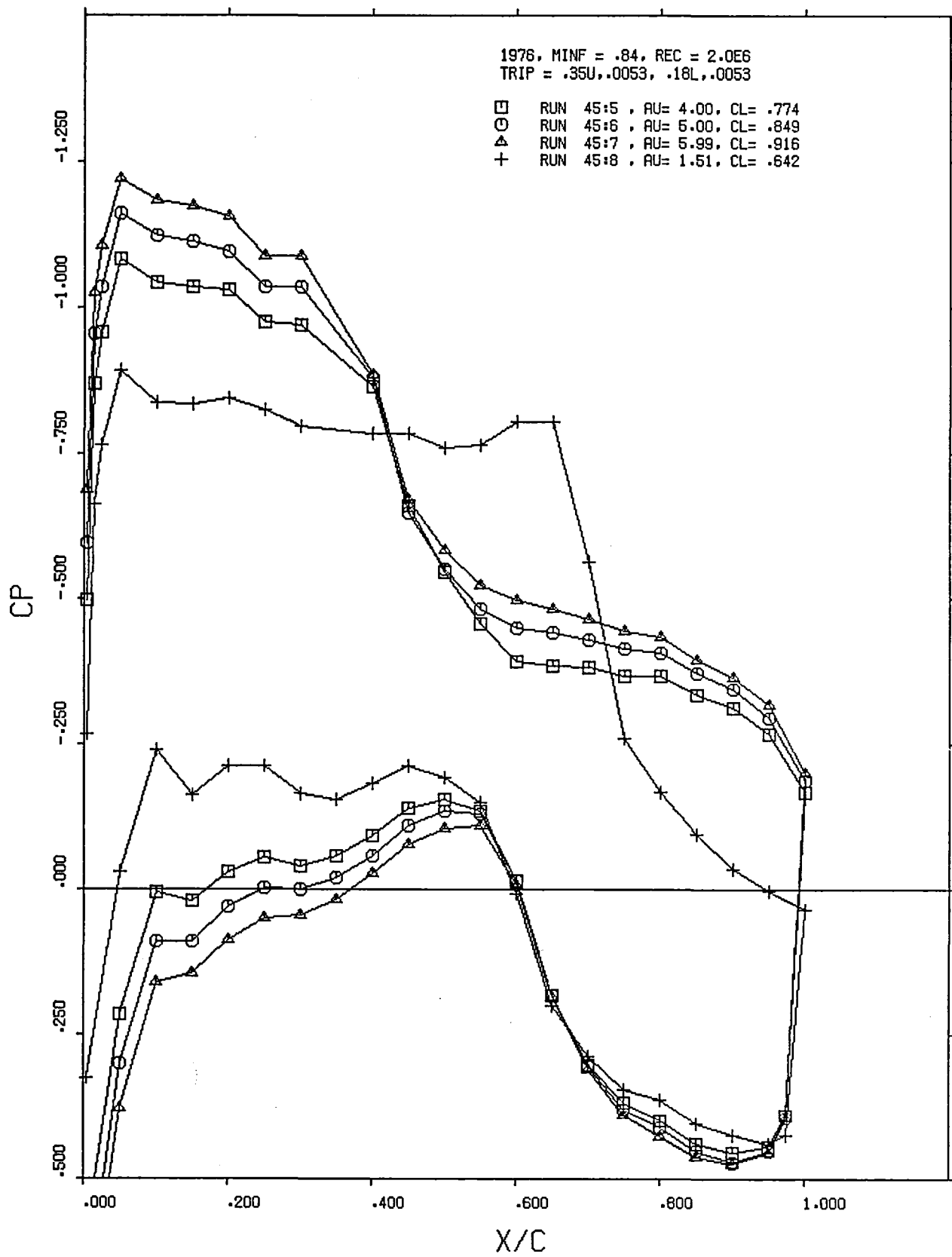


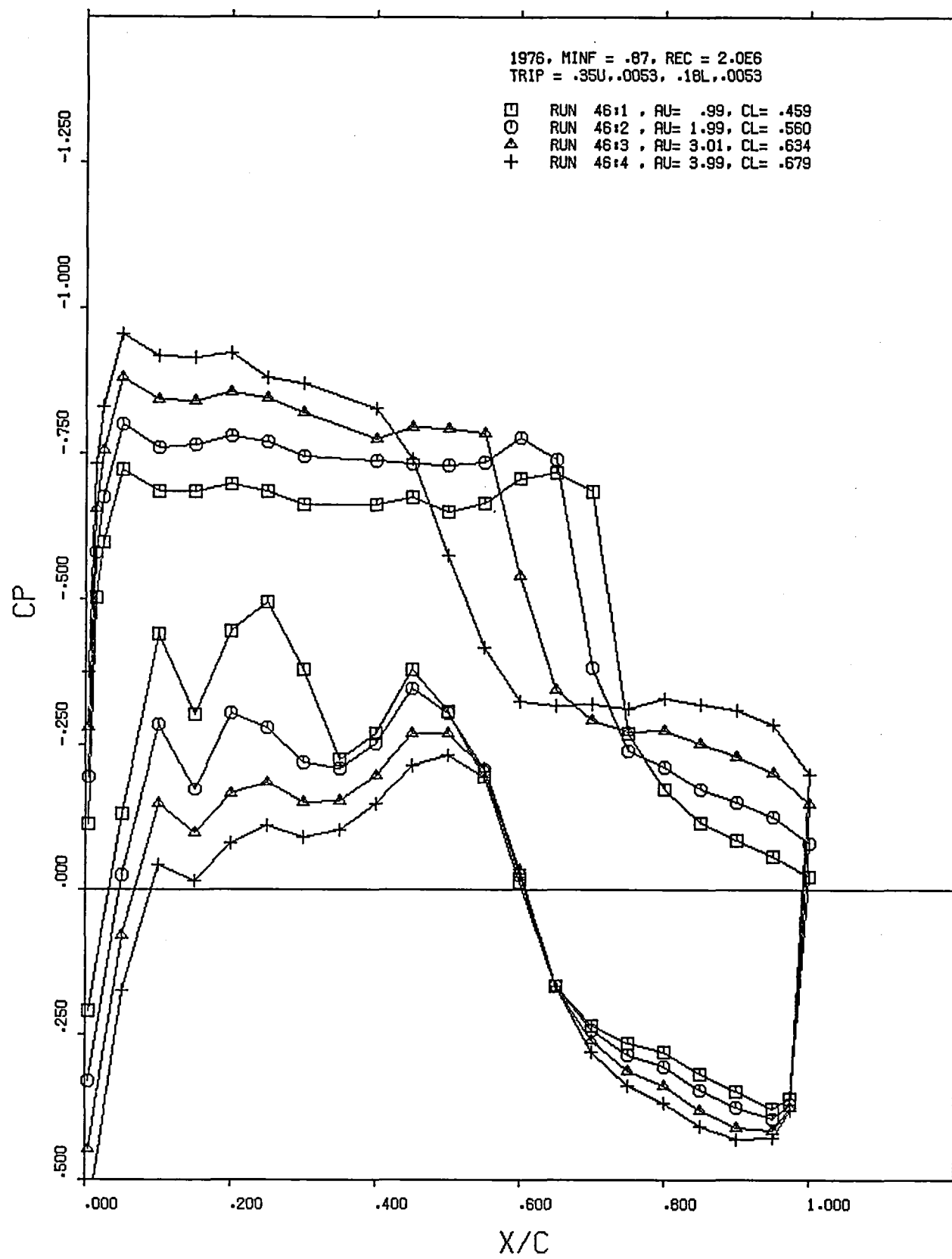


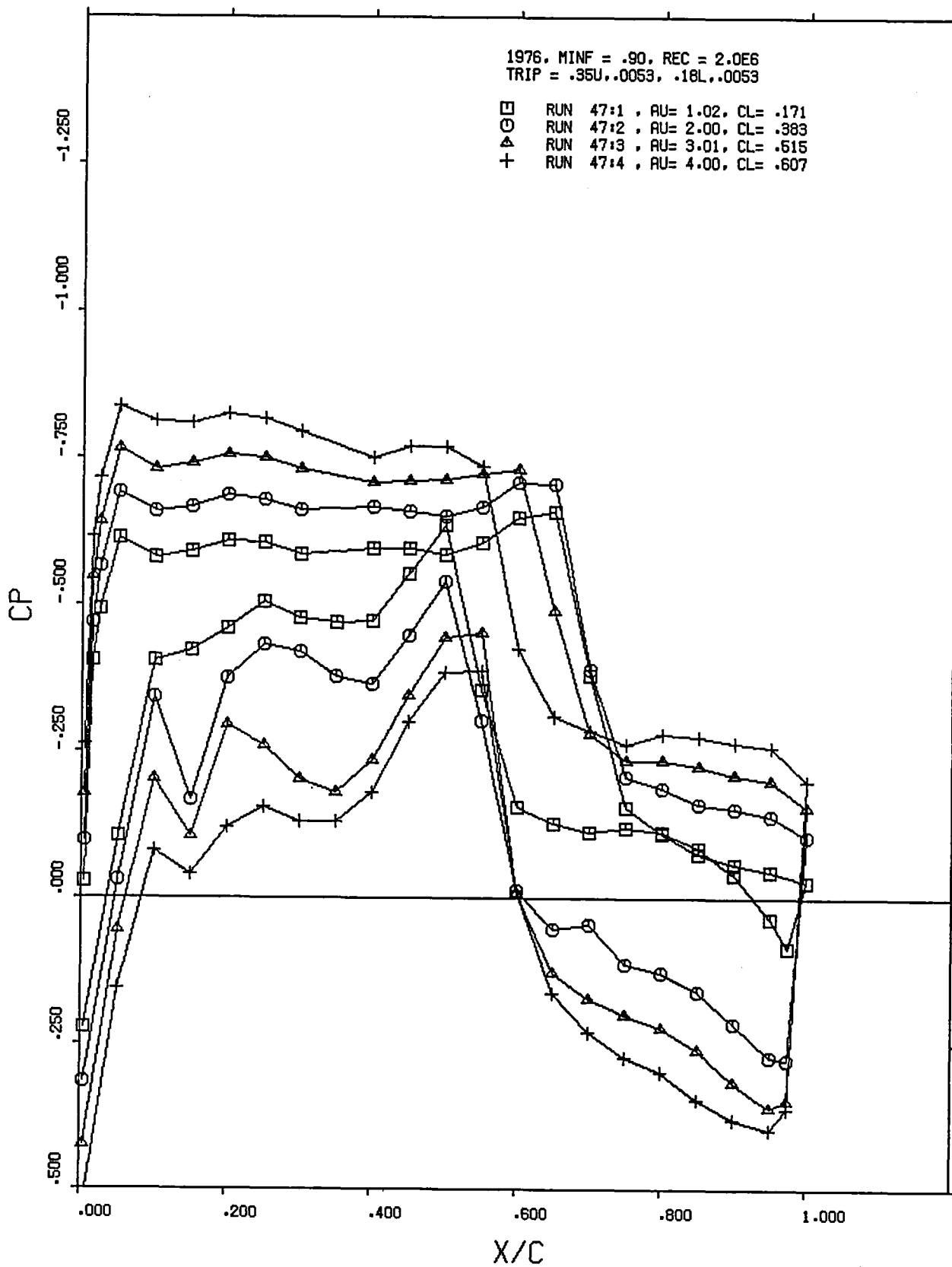


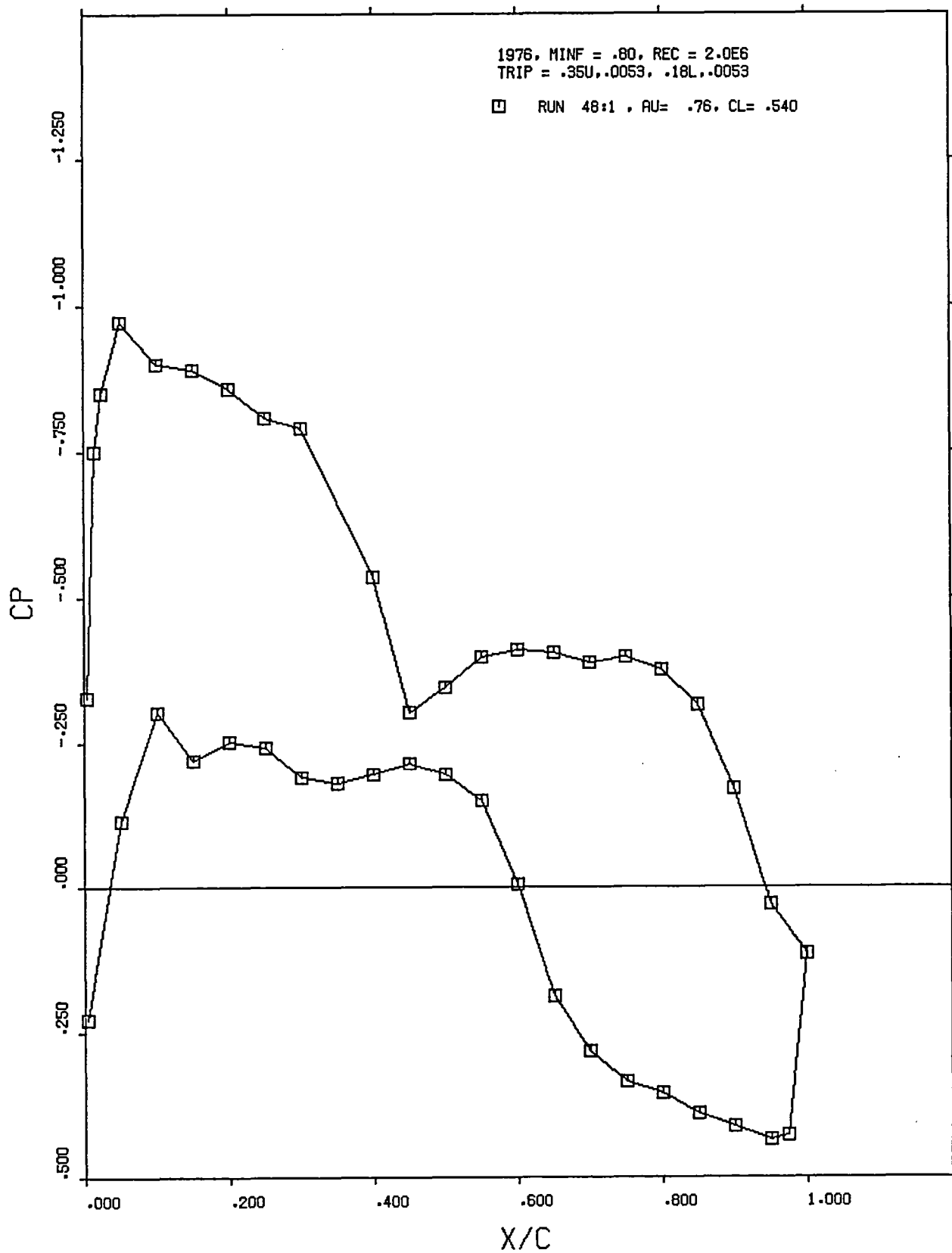


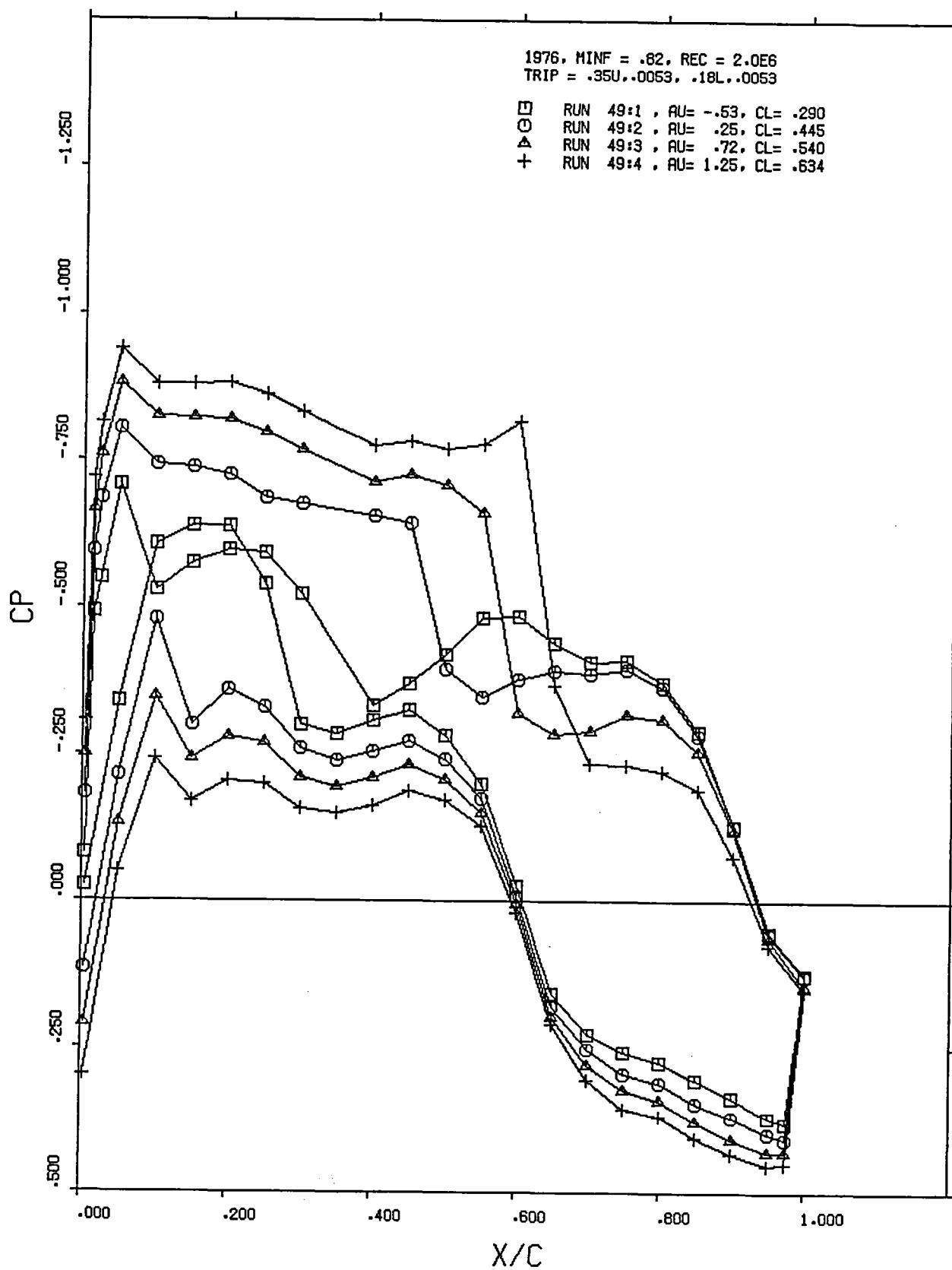


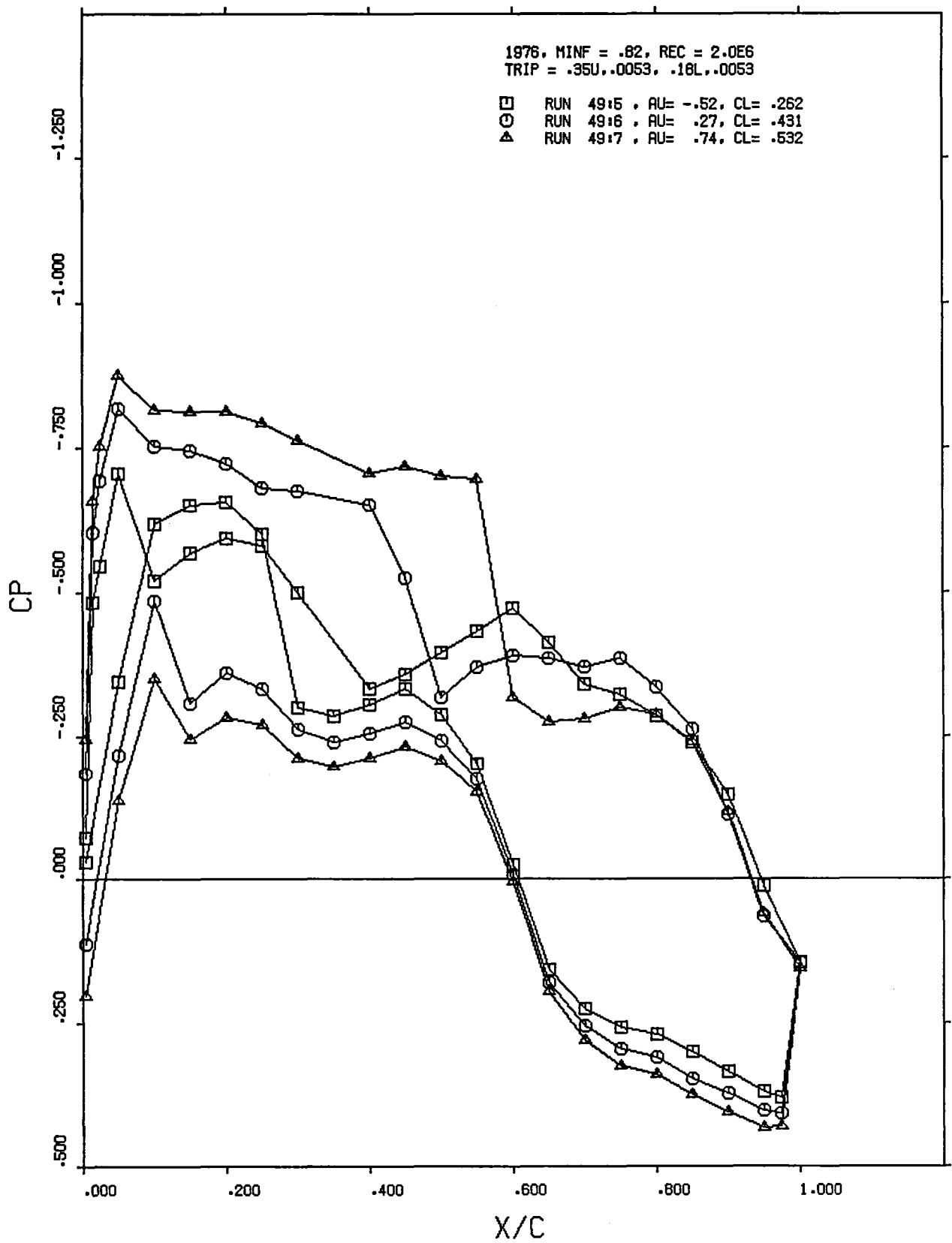




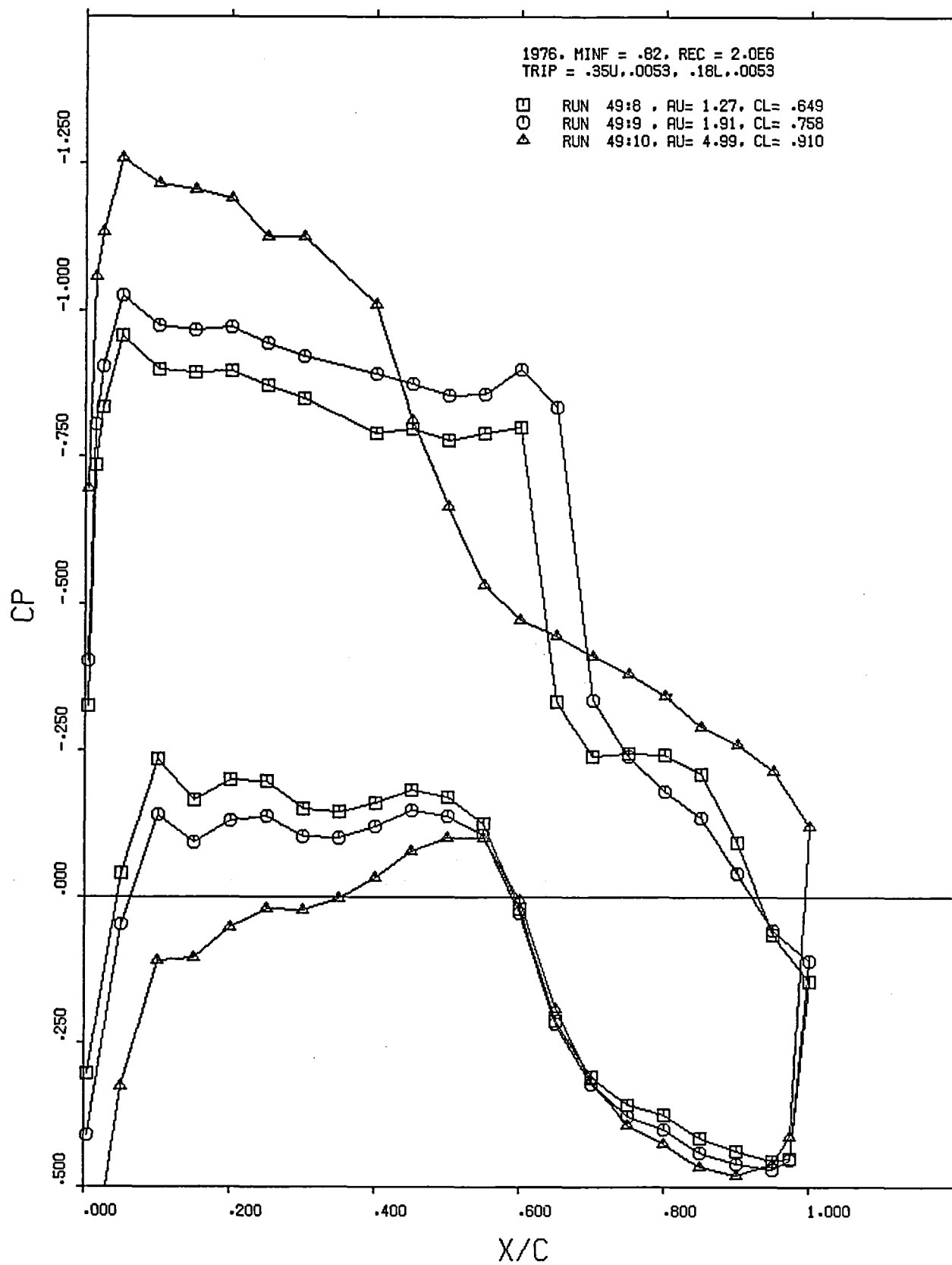


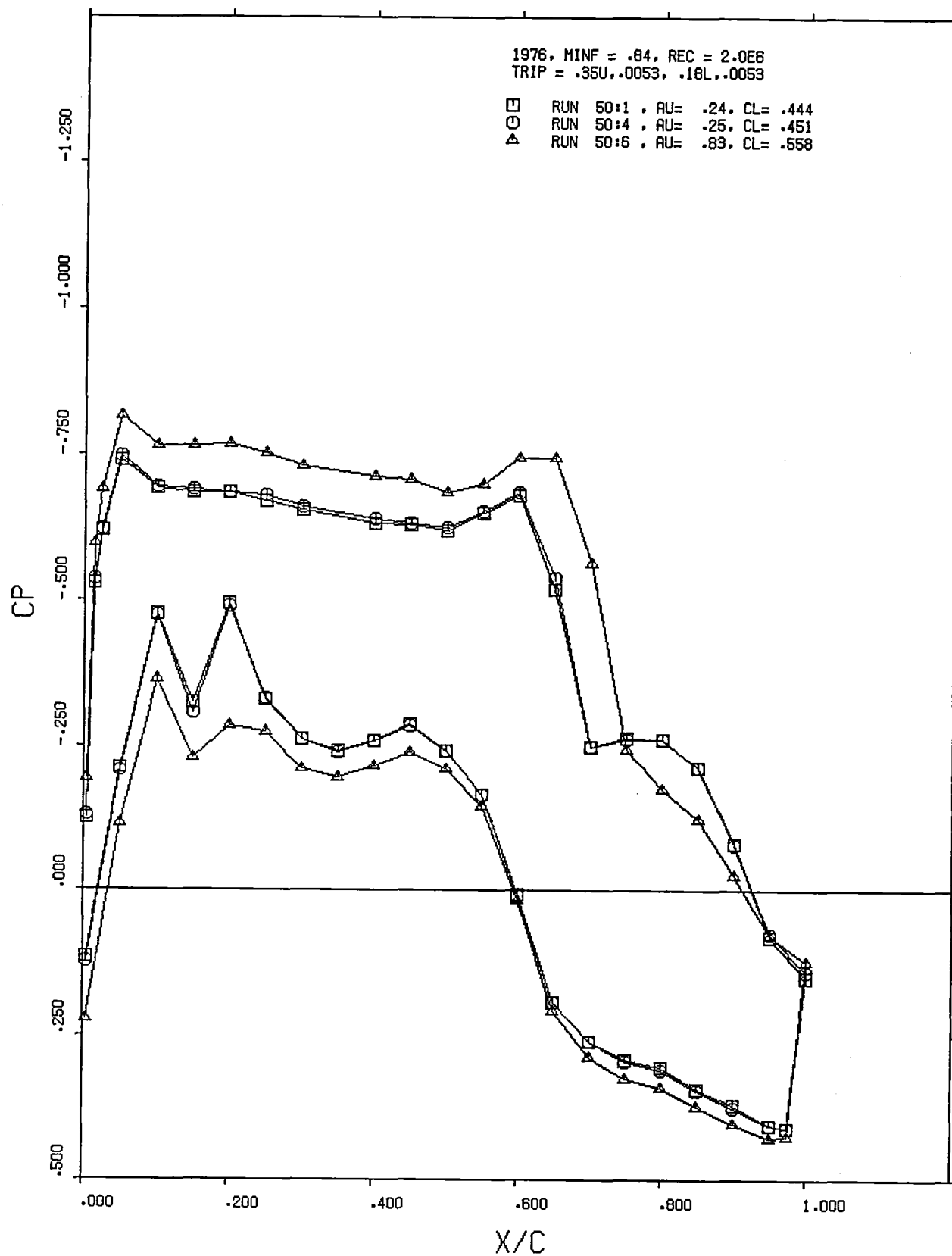


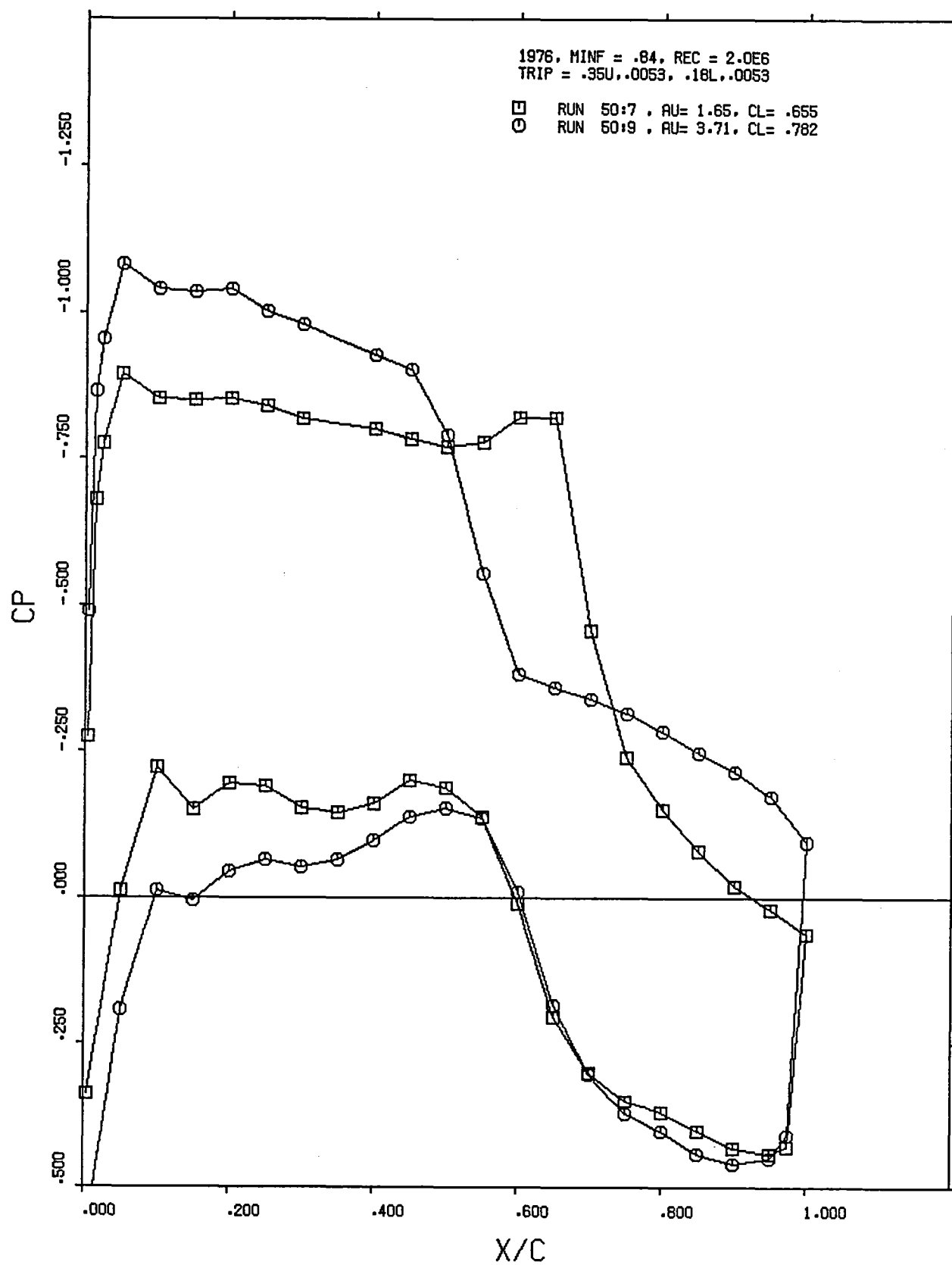


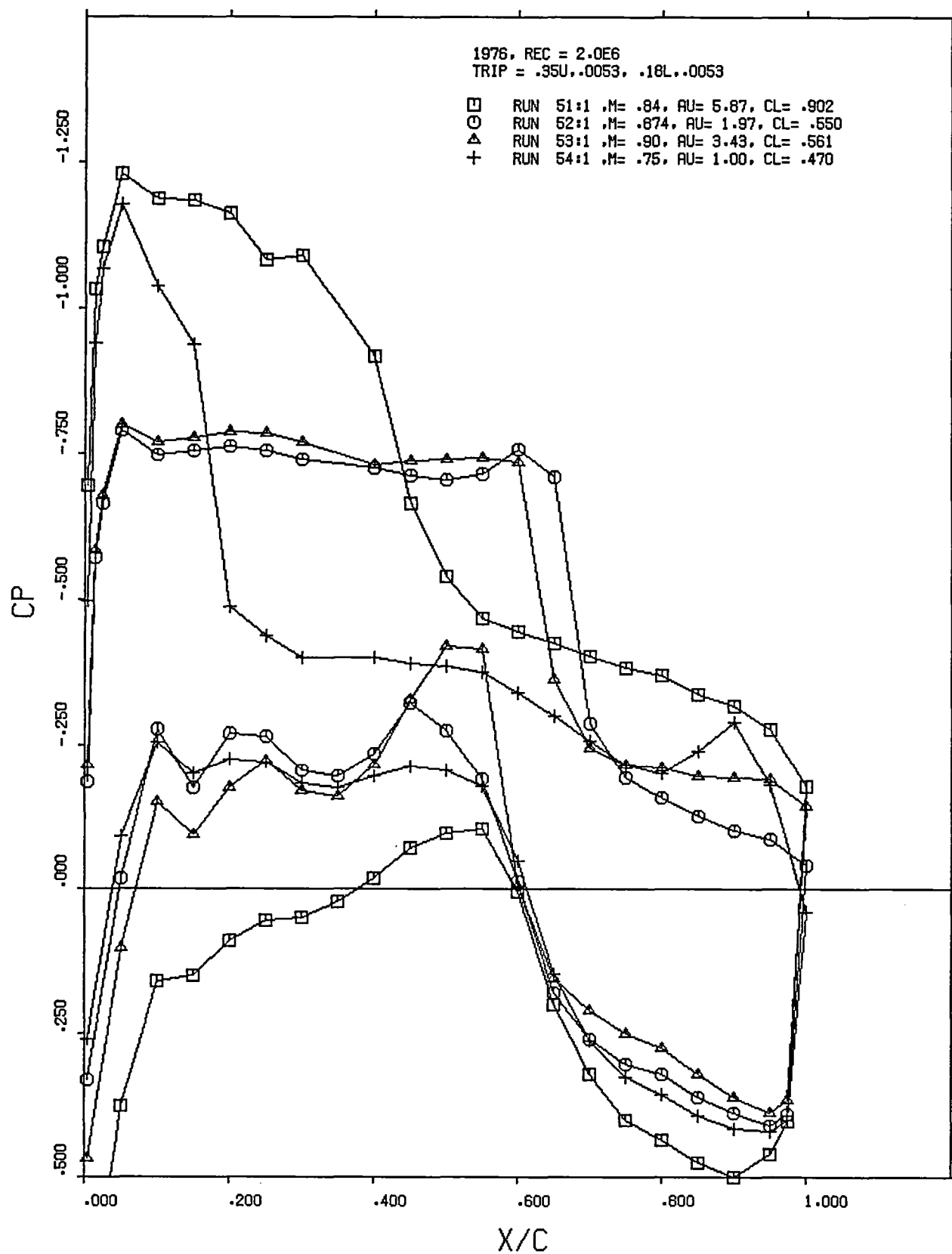


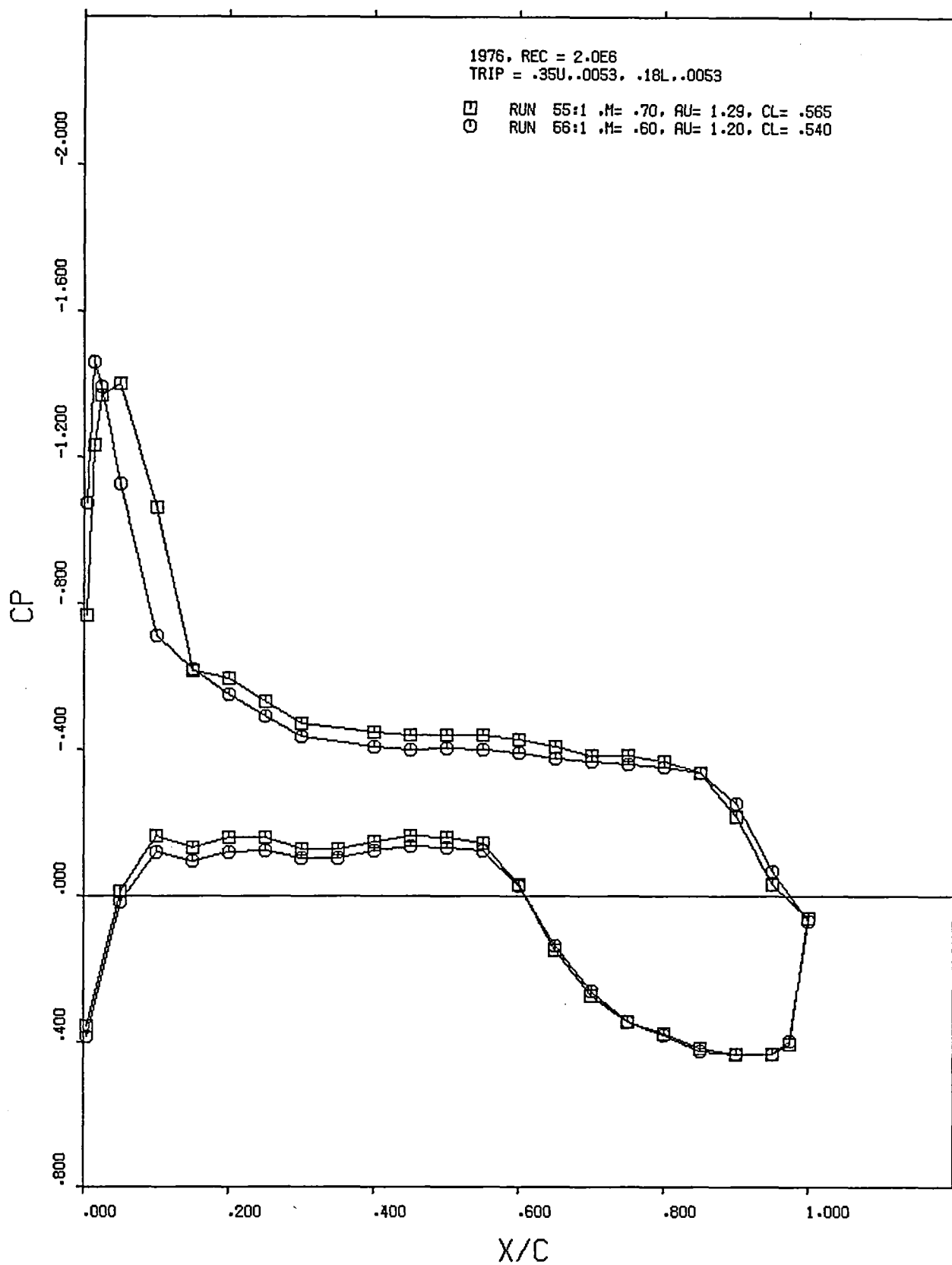


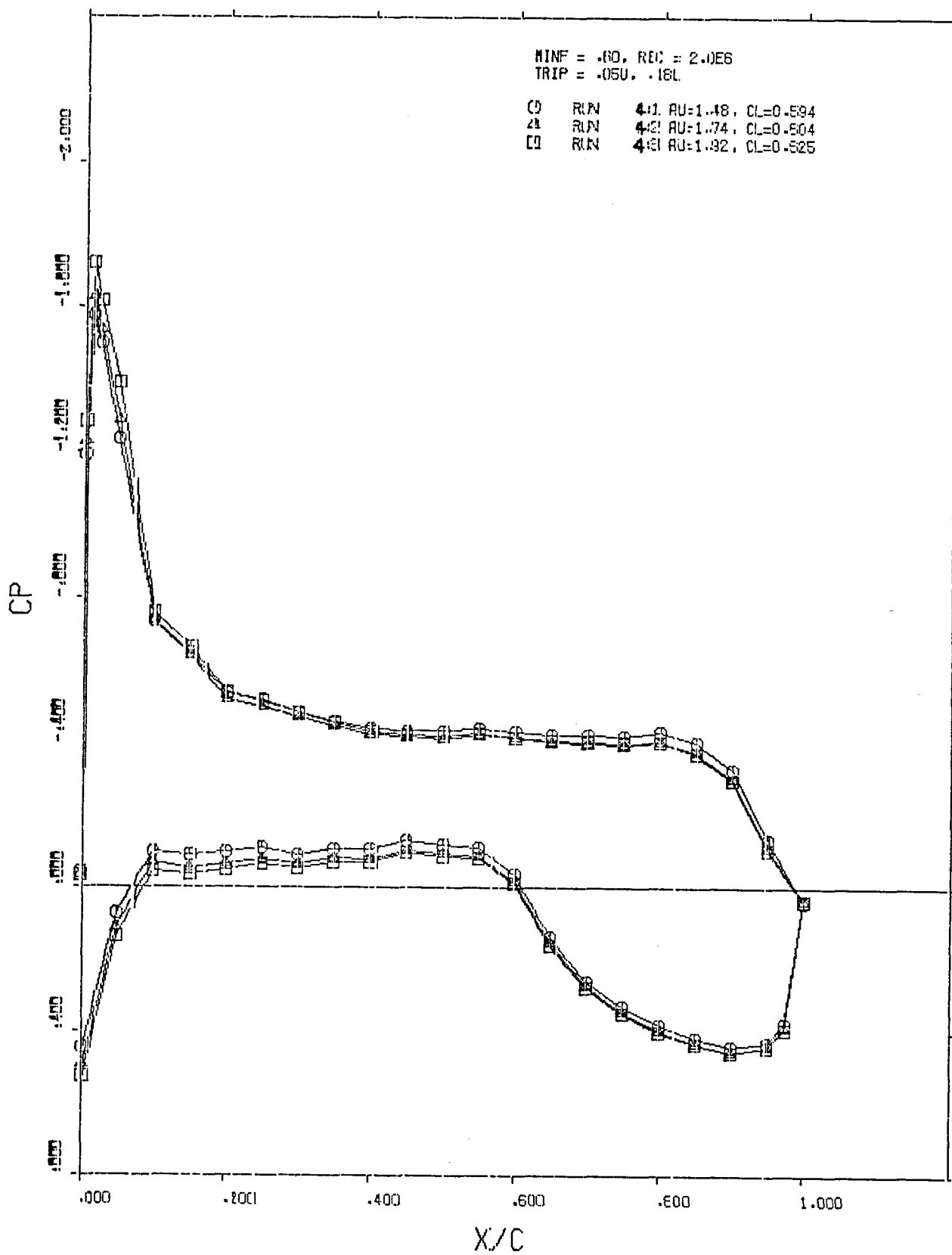


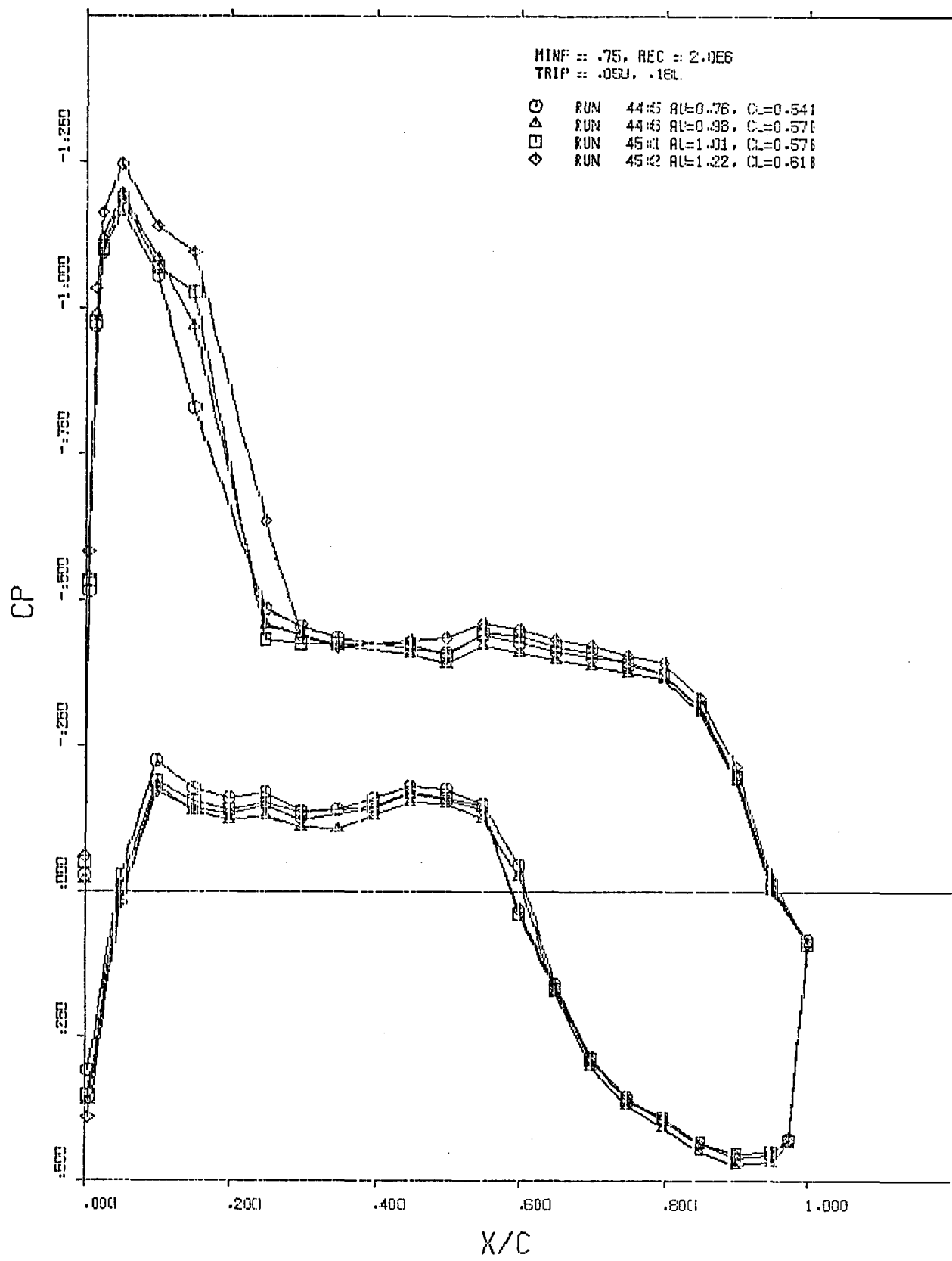


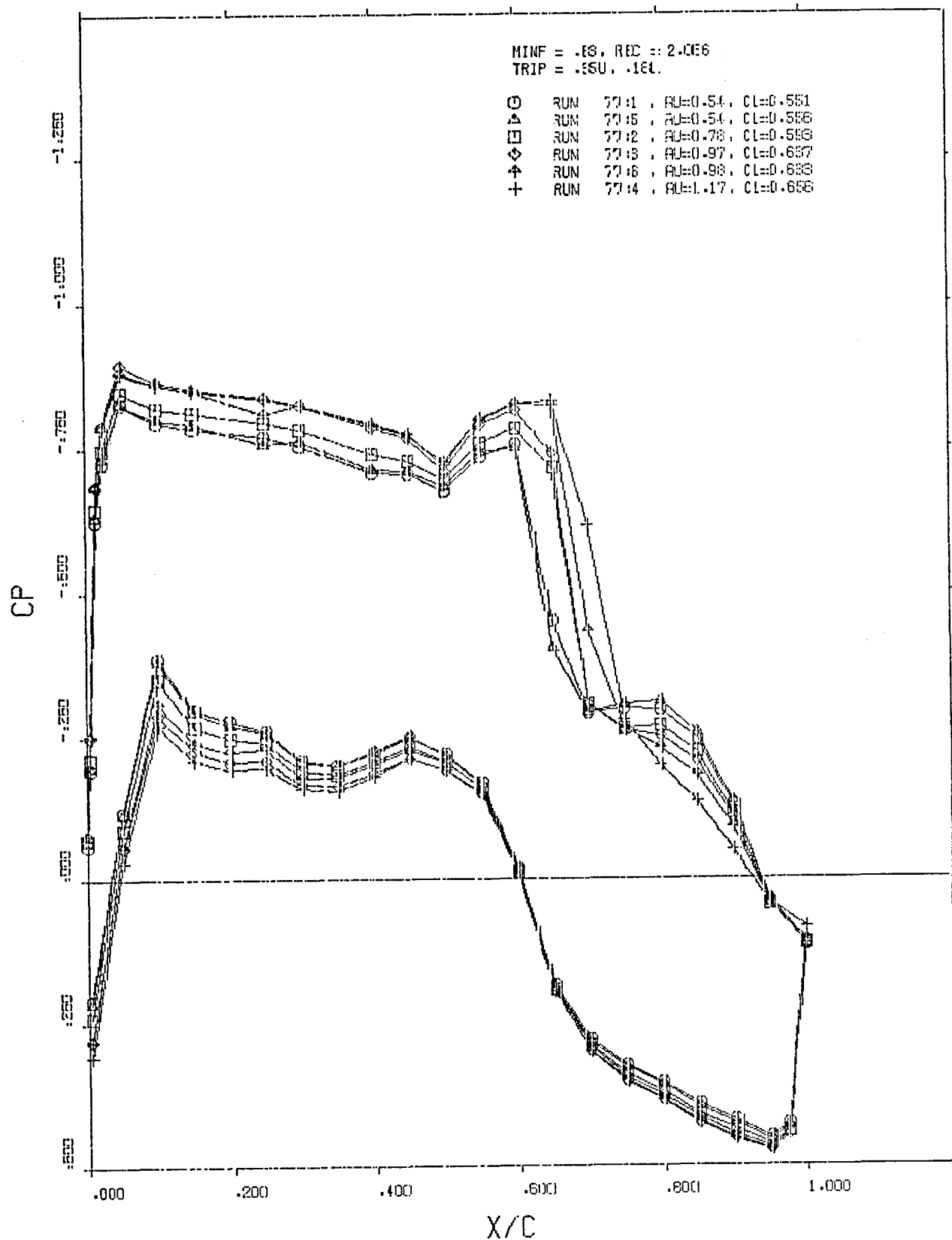




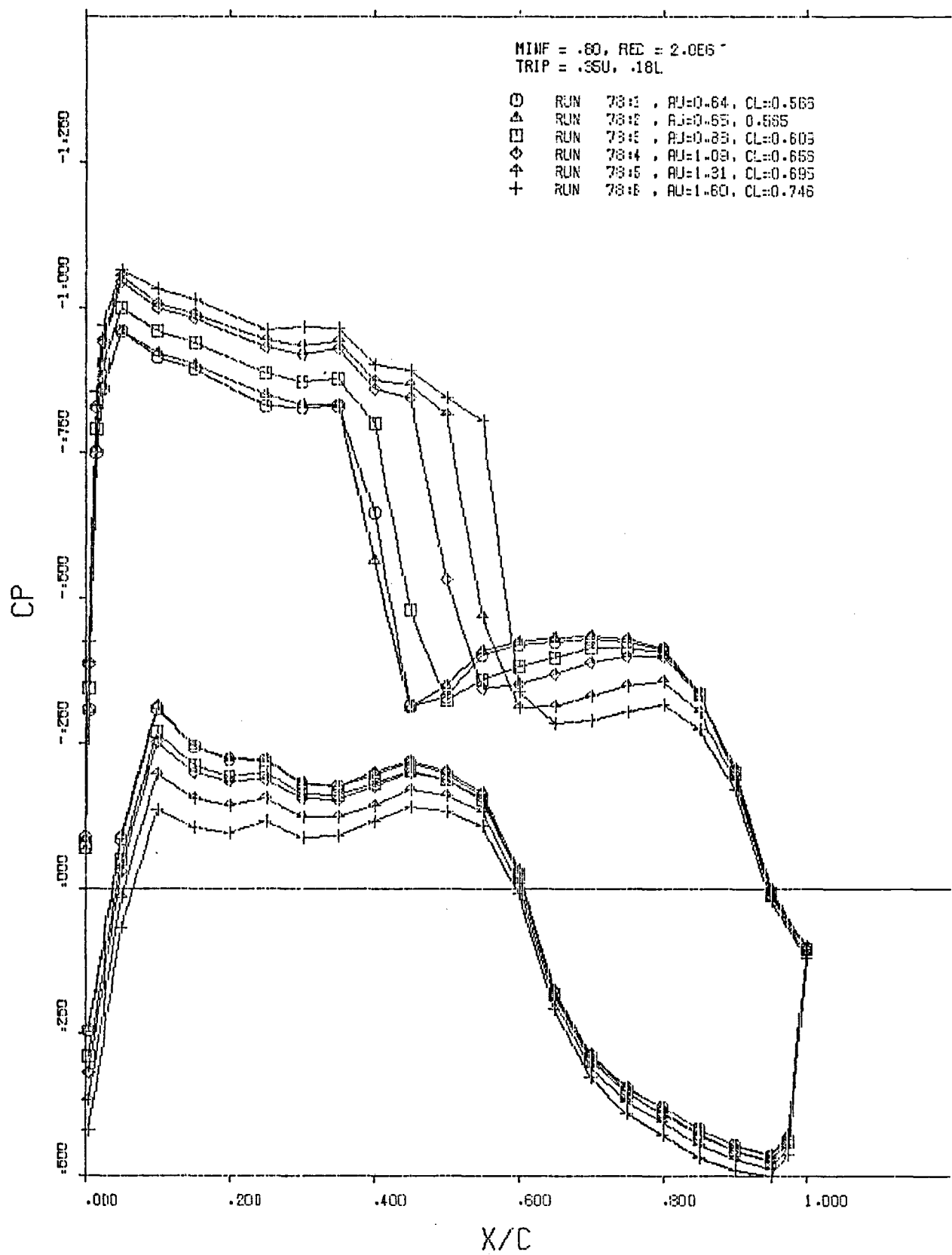


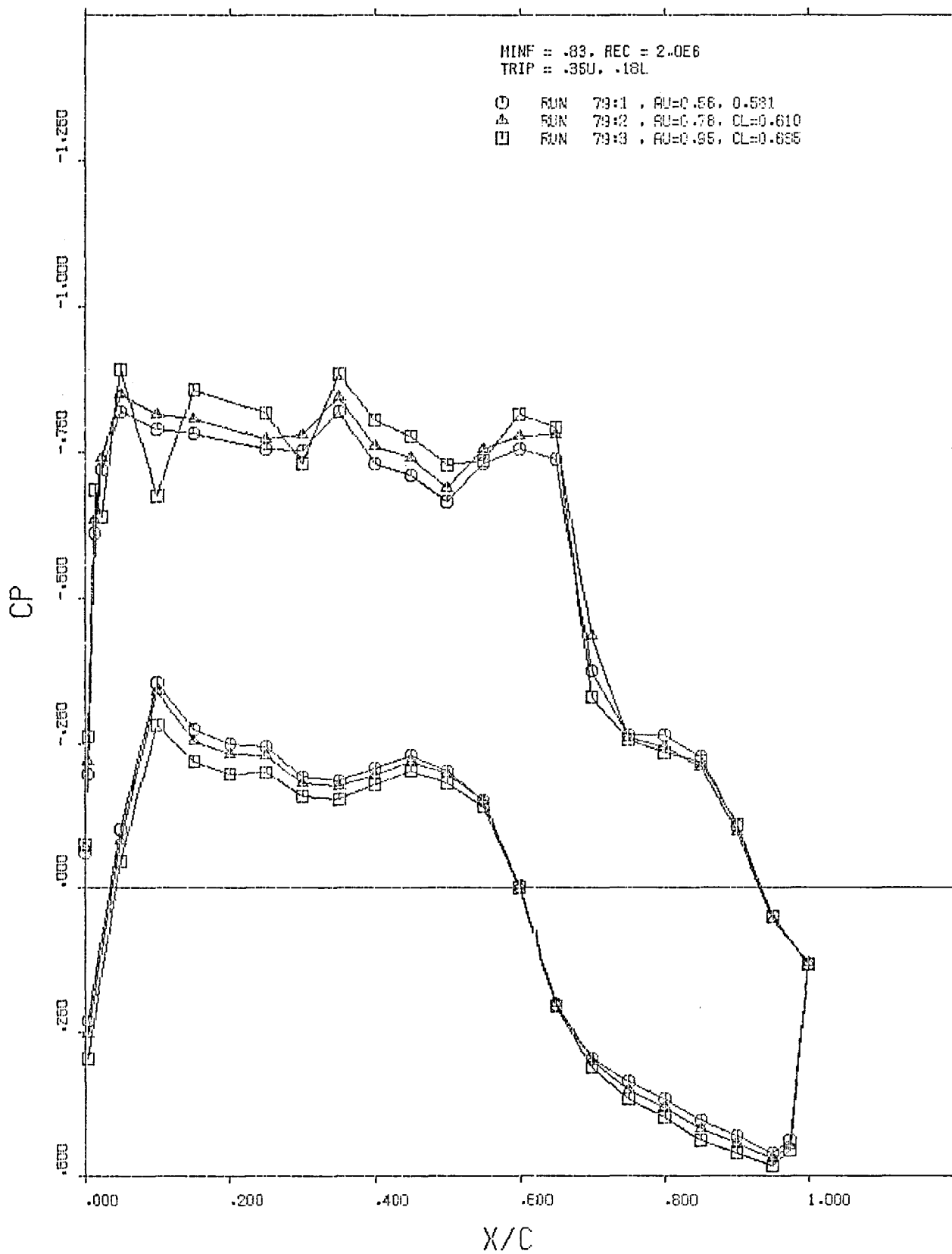


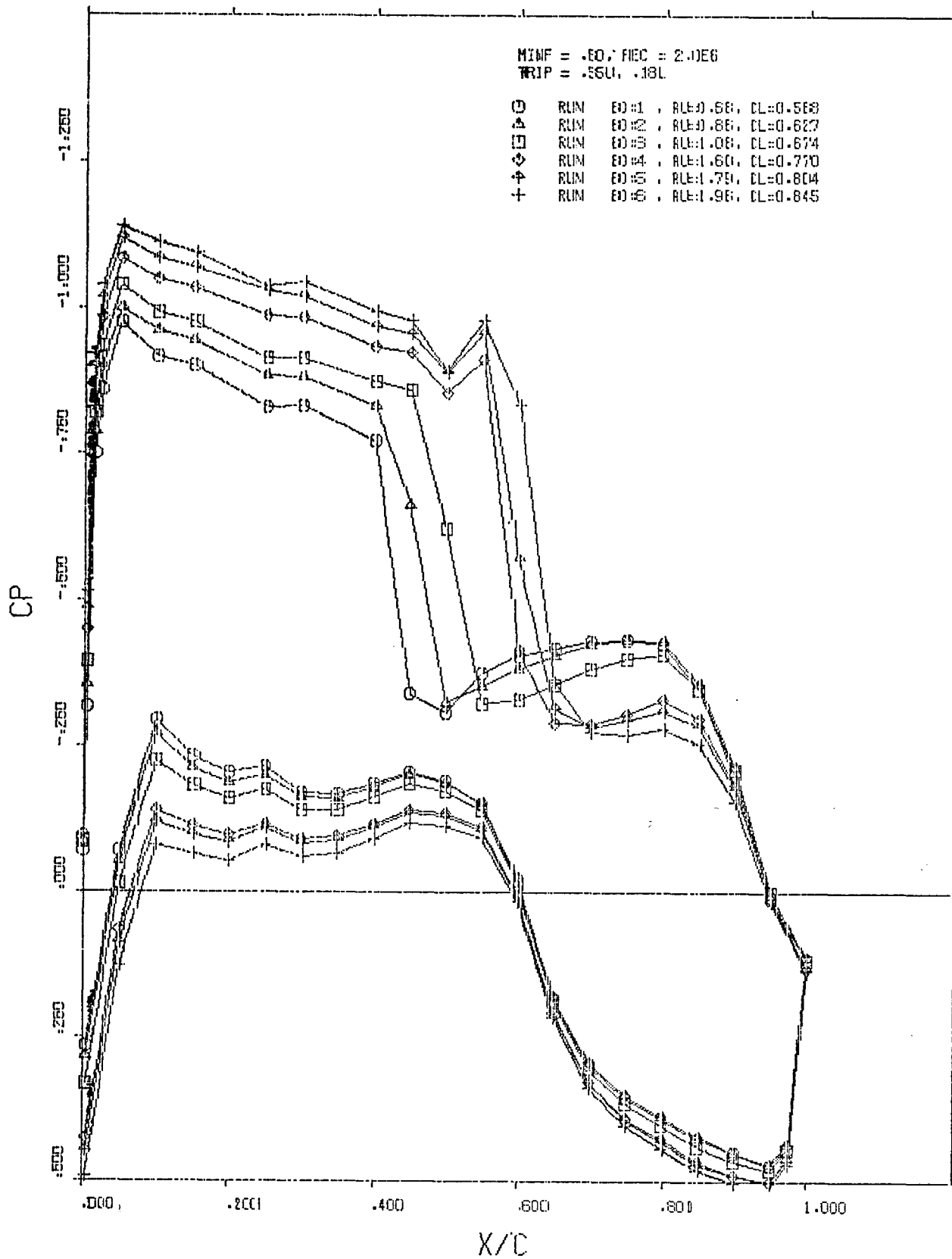












## APPENDIX C

### NACA 0012 MODEL, 1975 AND 1976

The tunnel-occupancy years are given on the plots. The trip configurations were the same on both upper and lower surfaces. The 1975 data have run numbers 131-140, and the 1976 data have run numbers 57-65.

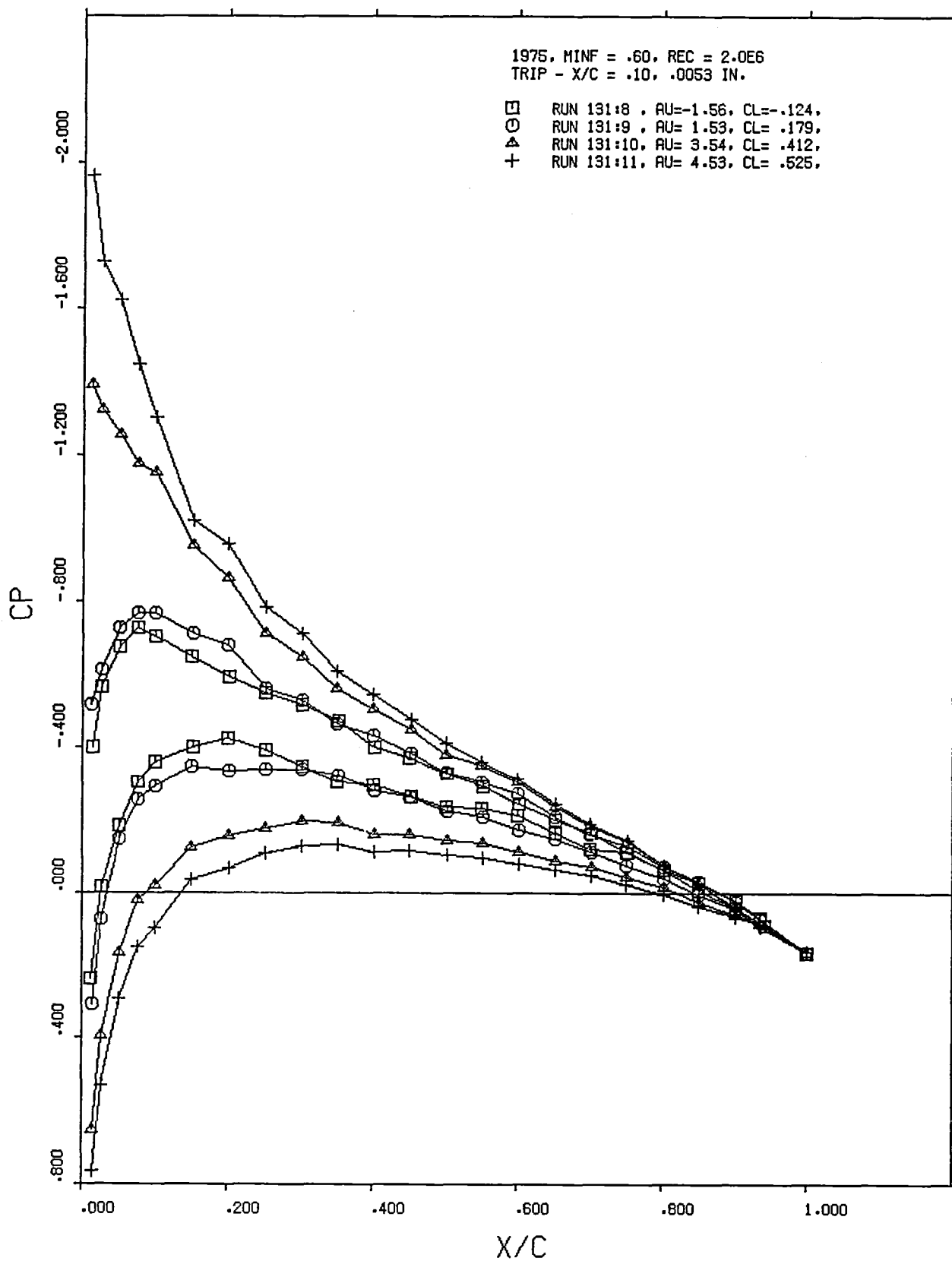
TABLE C1. RUN SCHEDULE, NACA 0012 MODEL,  $Re_c = 2 \times 10^6$

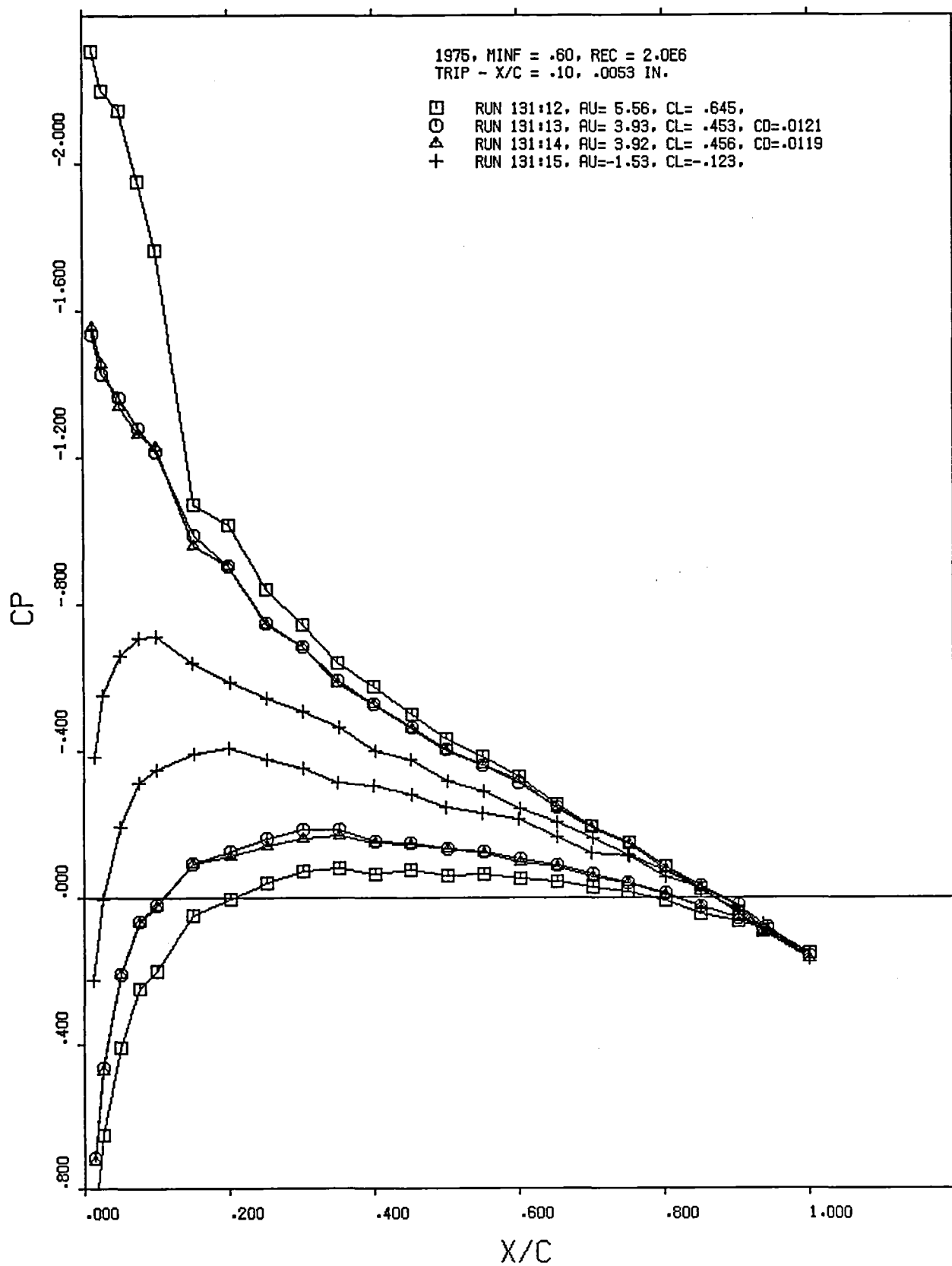
(1975 data)  
Boundary-Layer Trip  
 $x/c = 0.10$ ,  $T = 0.0053$  in.

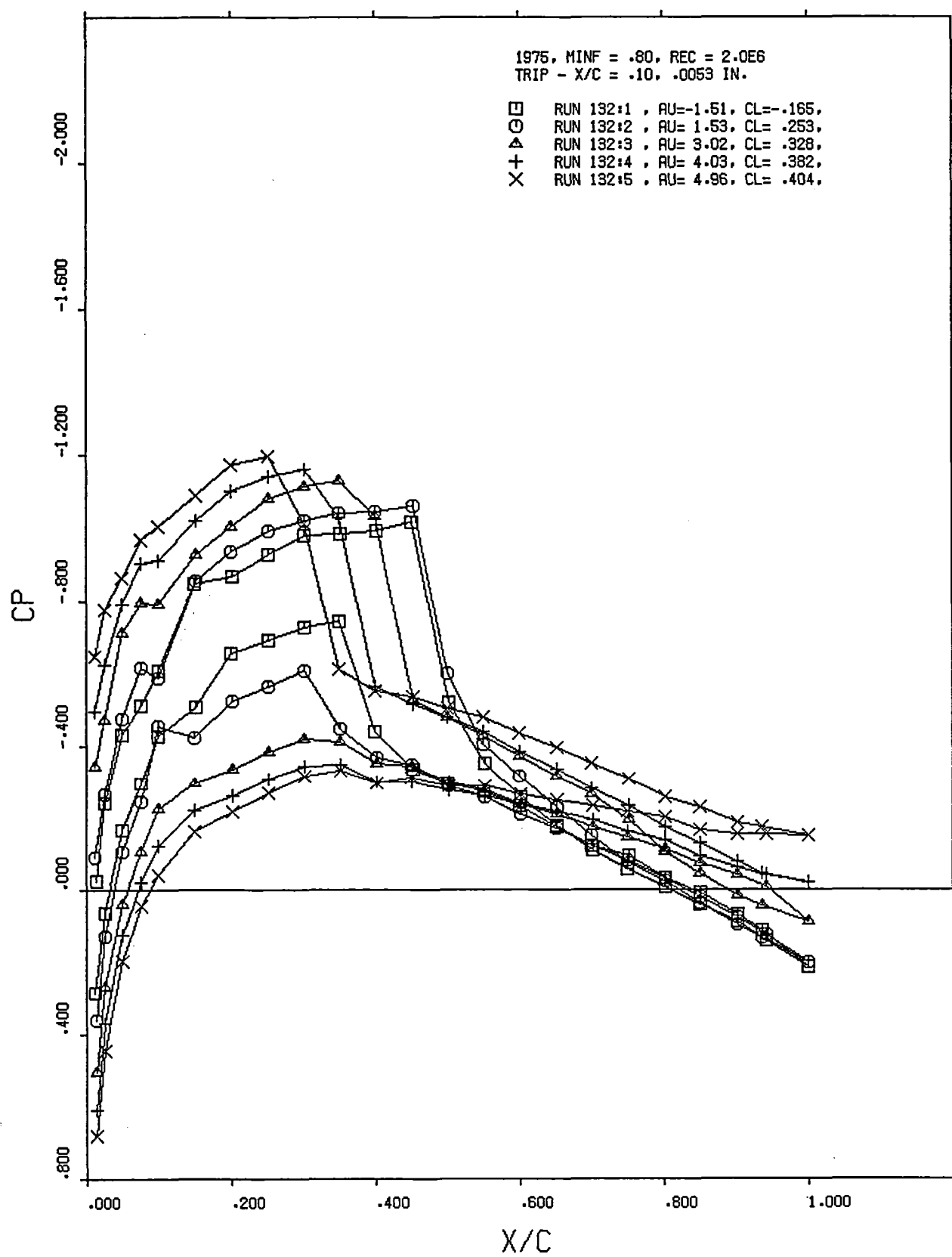
Run no.	Nominal $M_\infty$
131	0.60
132	0.80
133	0.74
134	0.65
135, 136	0.68
137	0.71
138	0.77
139	0.68
140	0.80

(1976 data)  
Boundary-layer Trip  
 $x/c = 0.18$ ,  $T = 0.0053$  in.

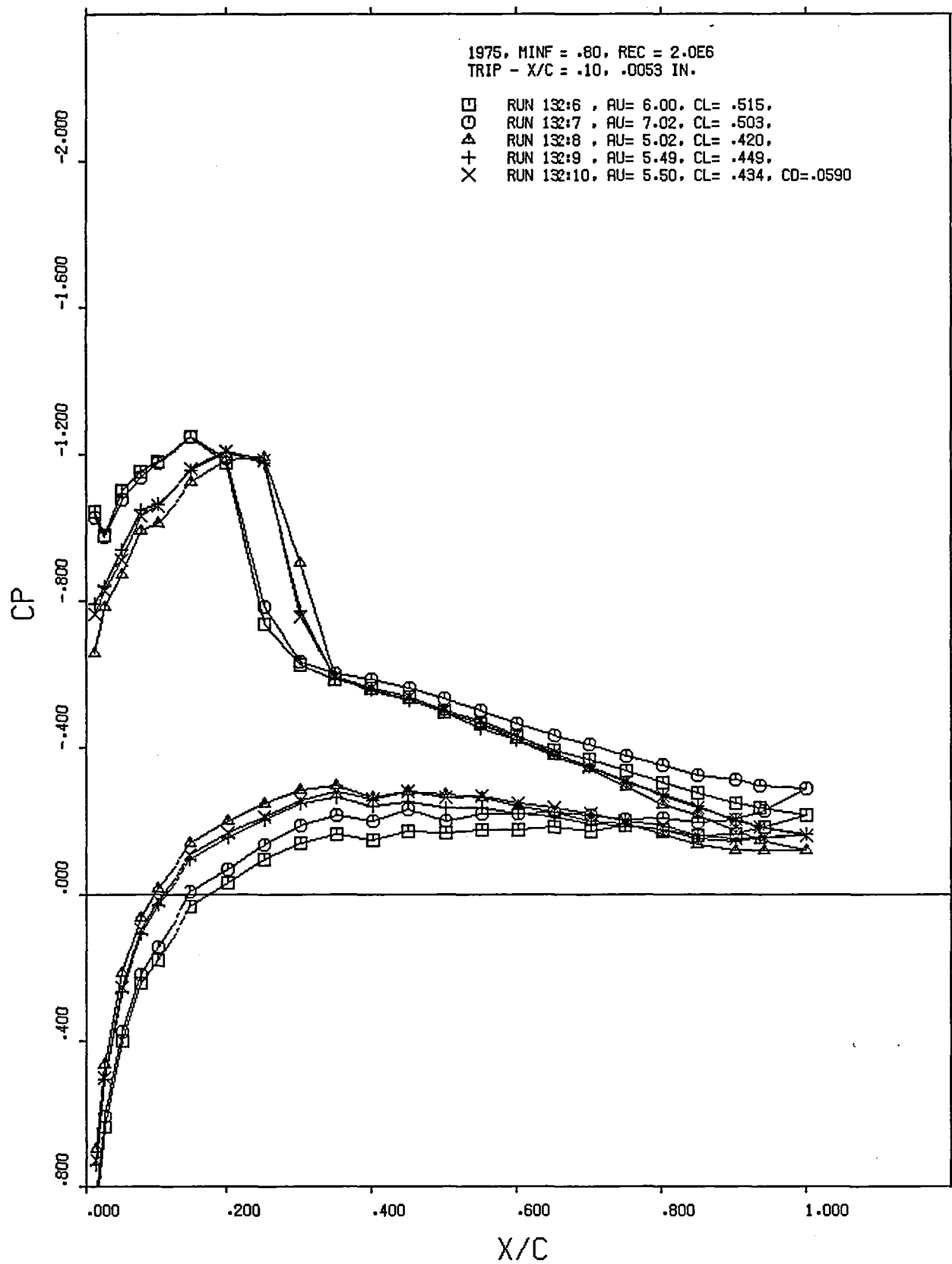
Run no.	Nominal $M_\infty$
57	0.68
58	0.74
59	0.80
60	0.77
61	0.71
62	0.65
63	0.60
64	0.68
65	0.71

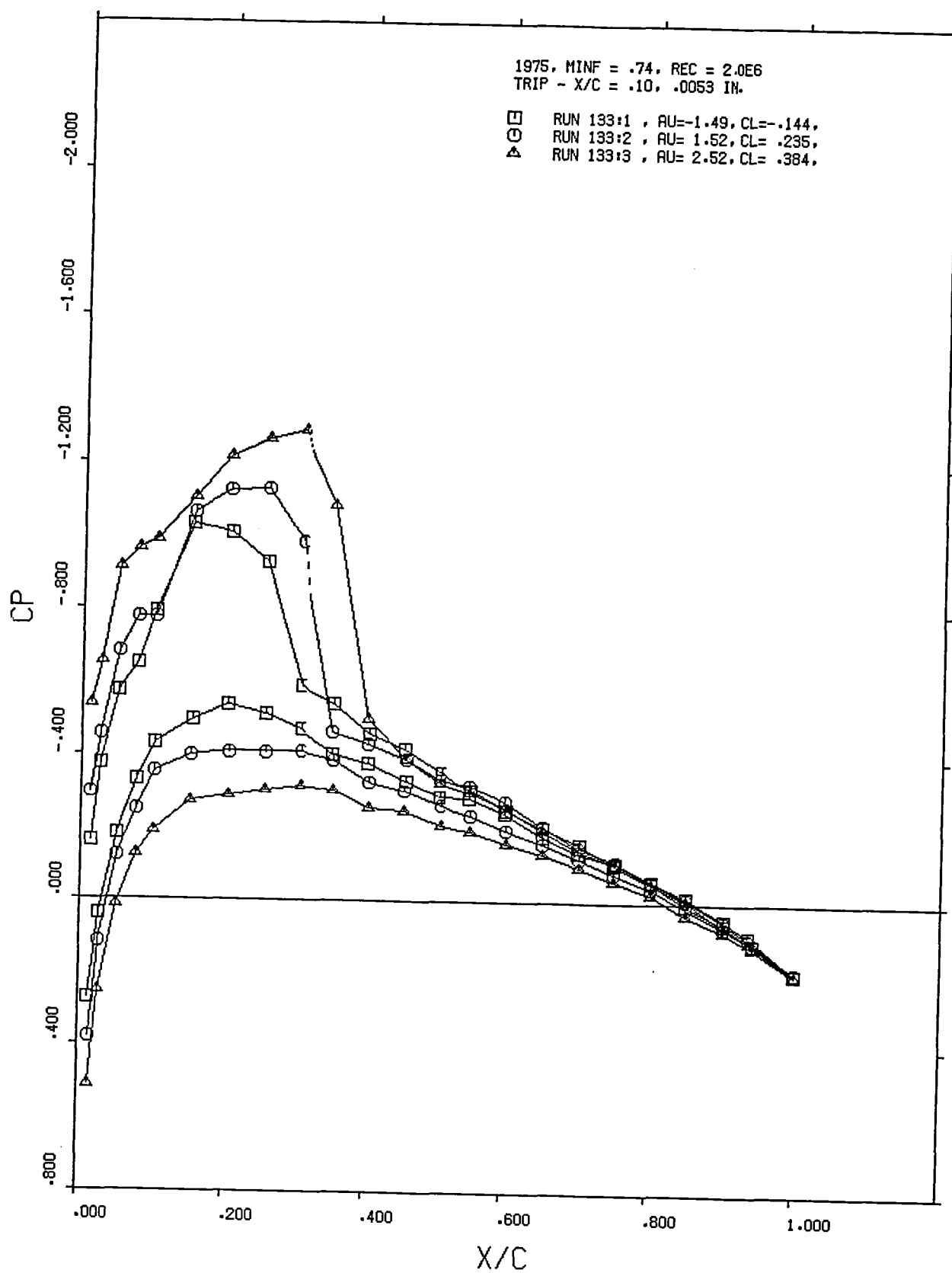


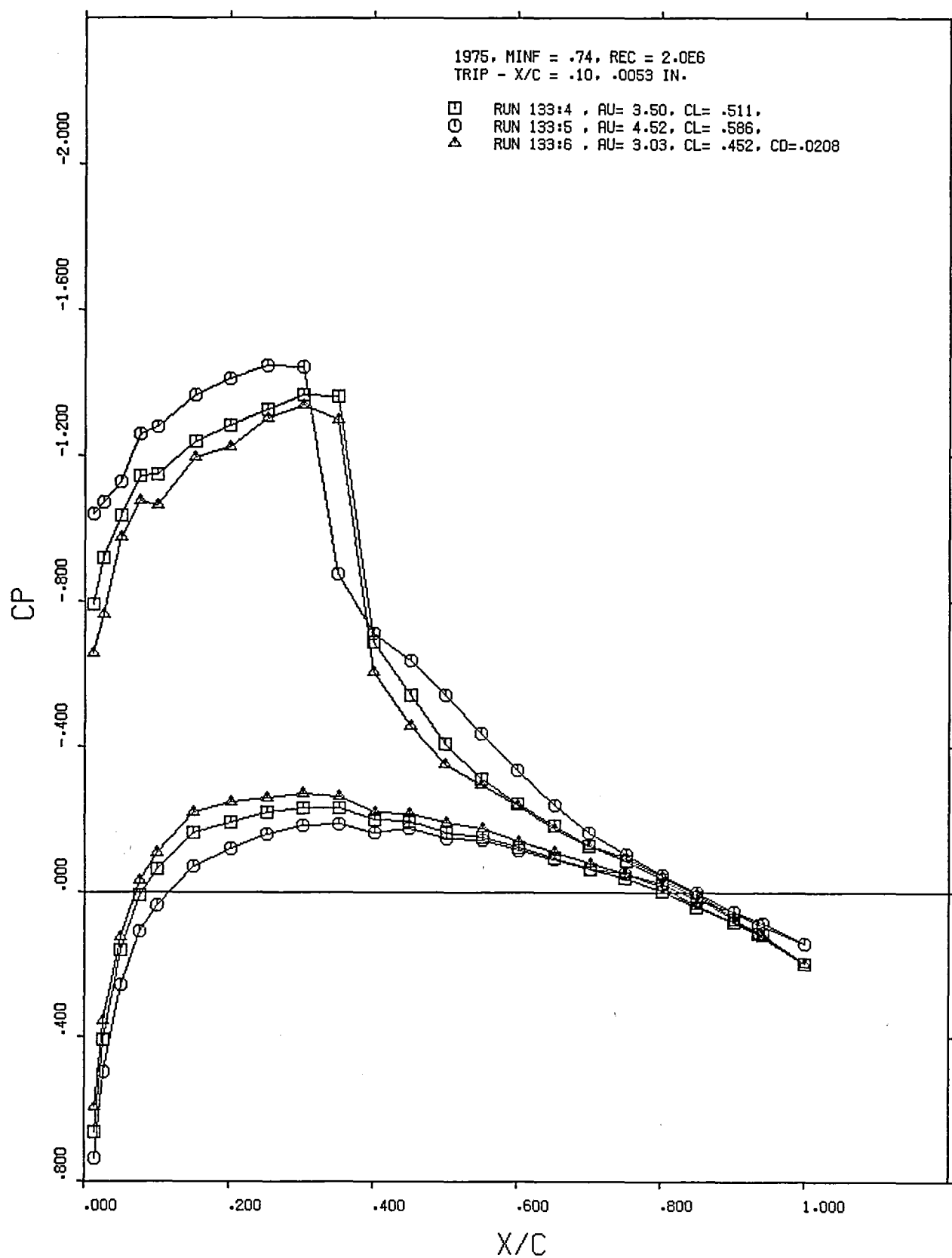


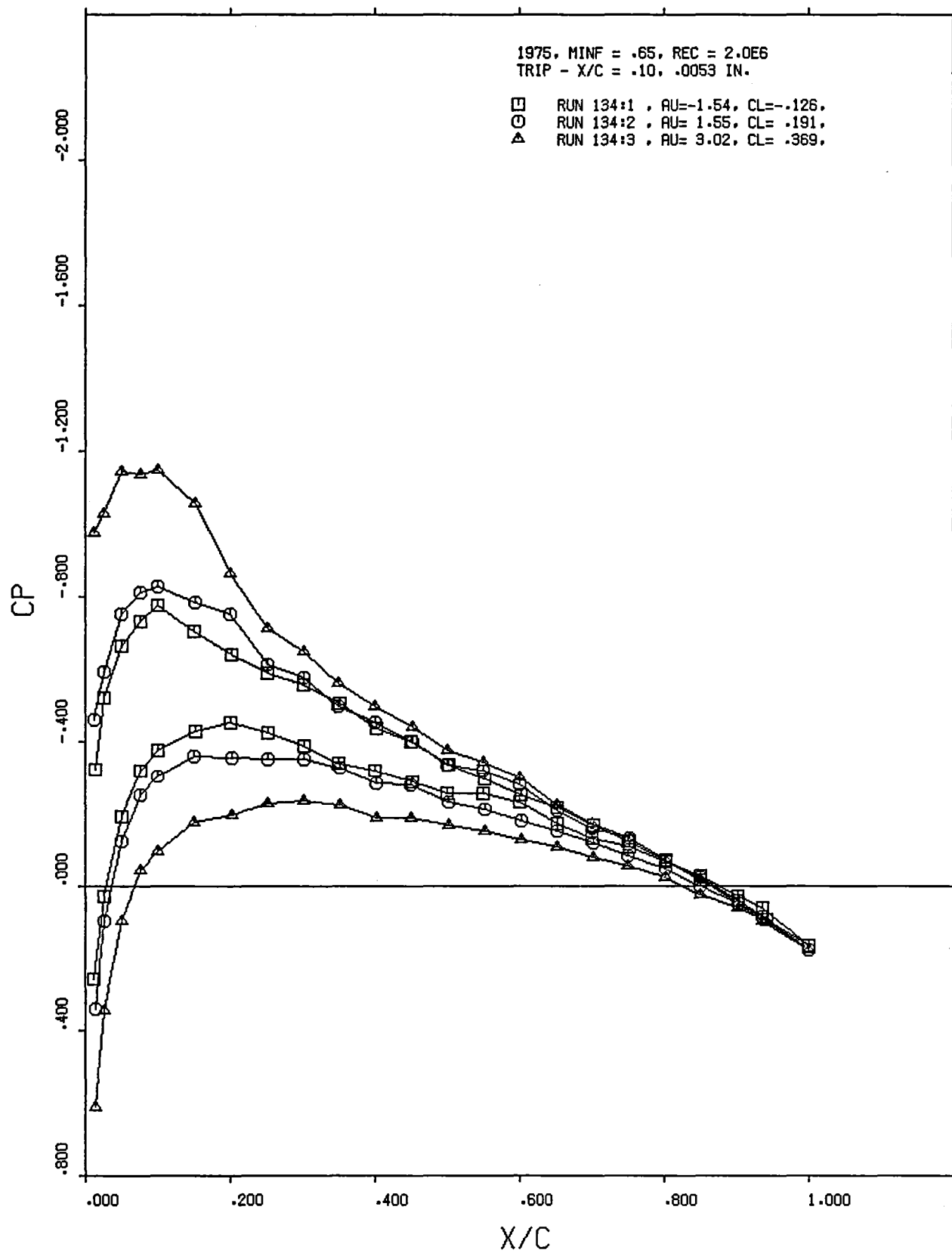


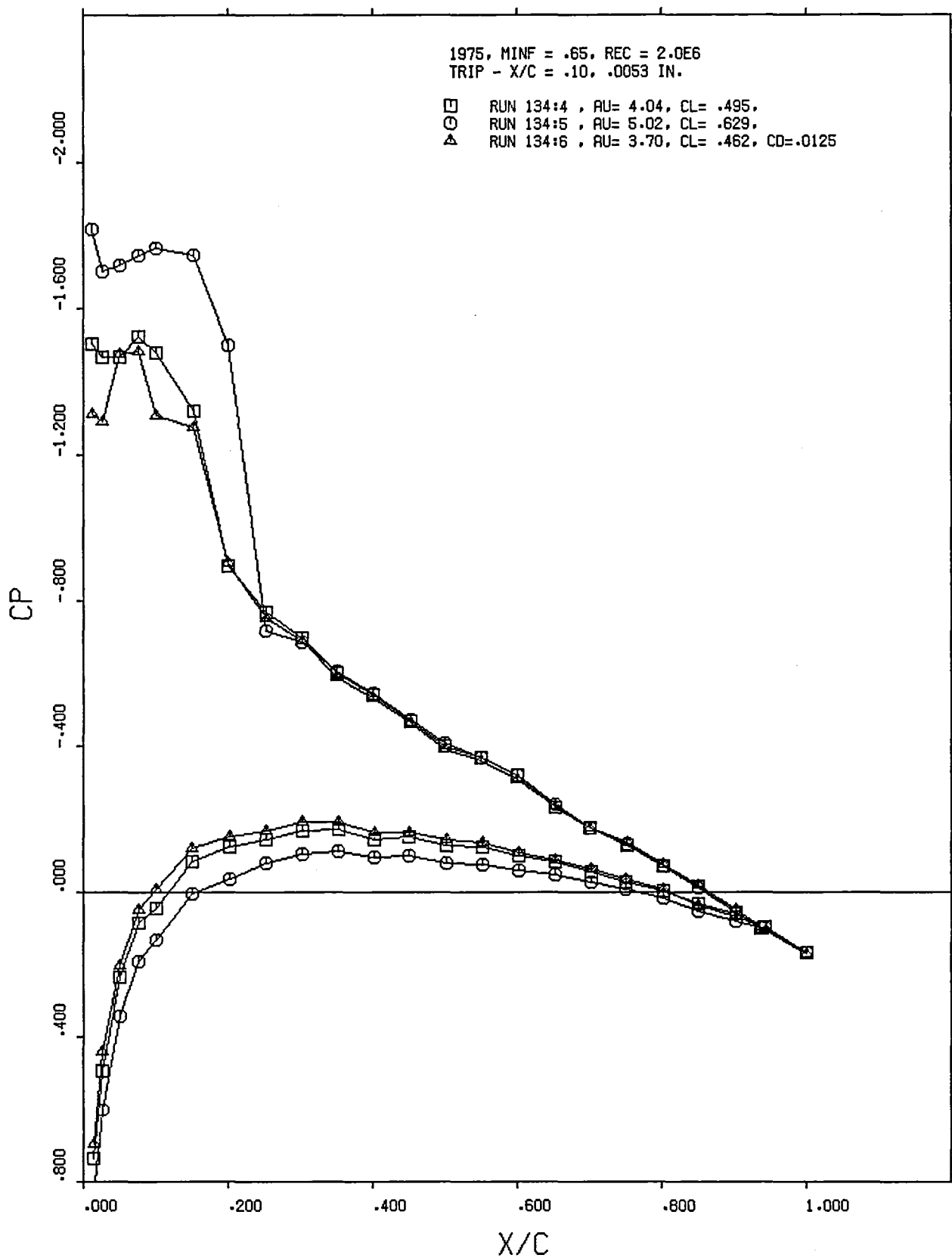


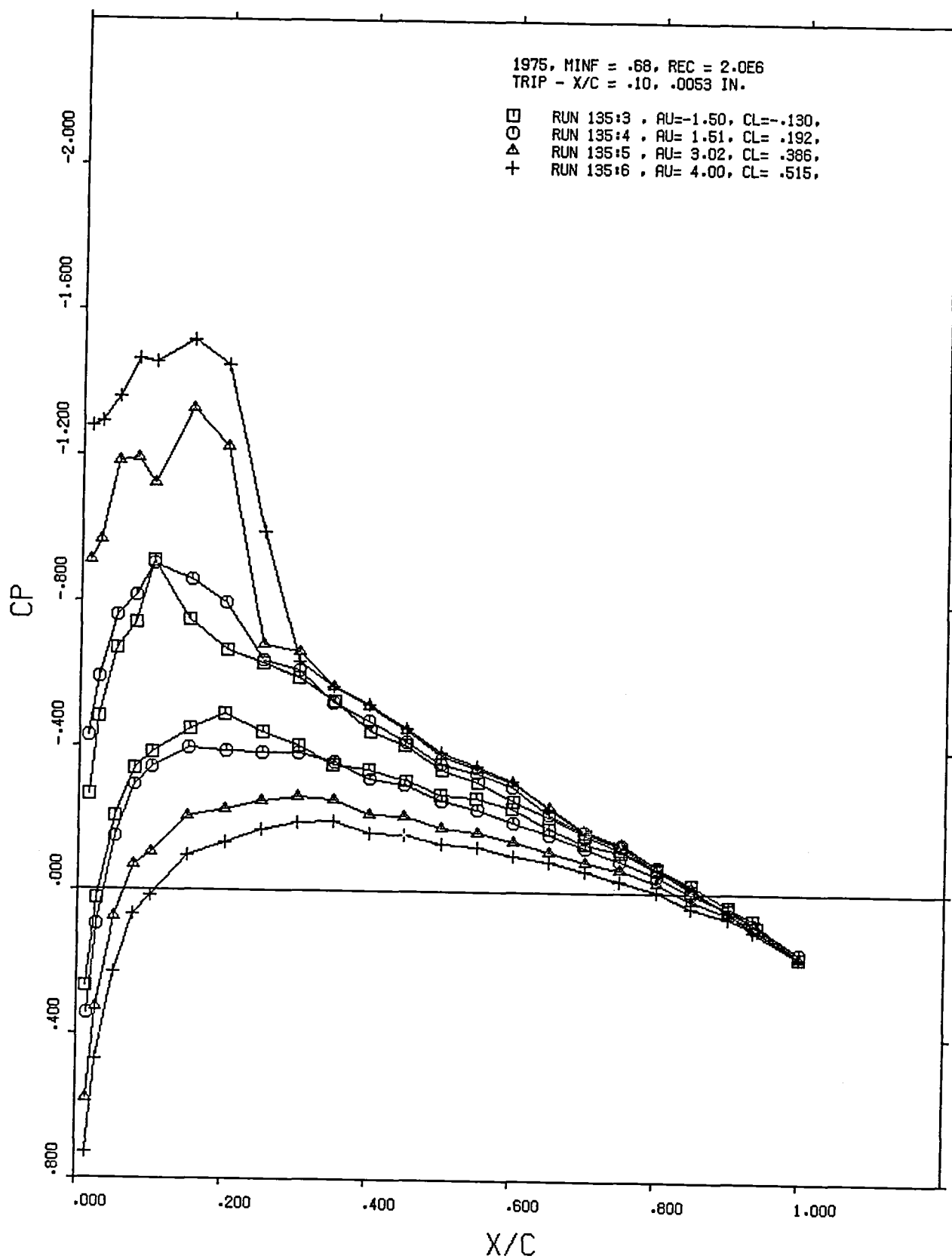


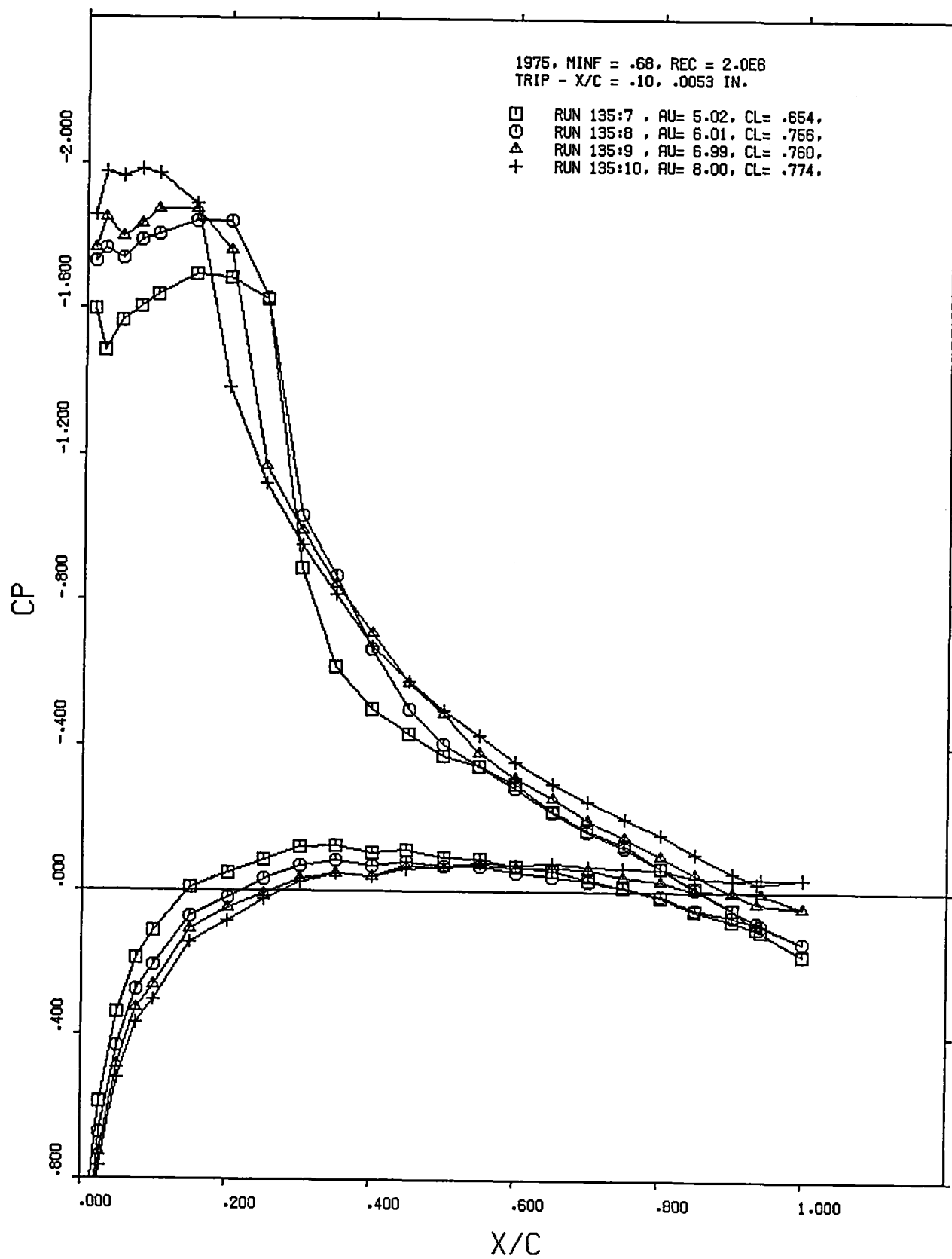


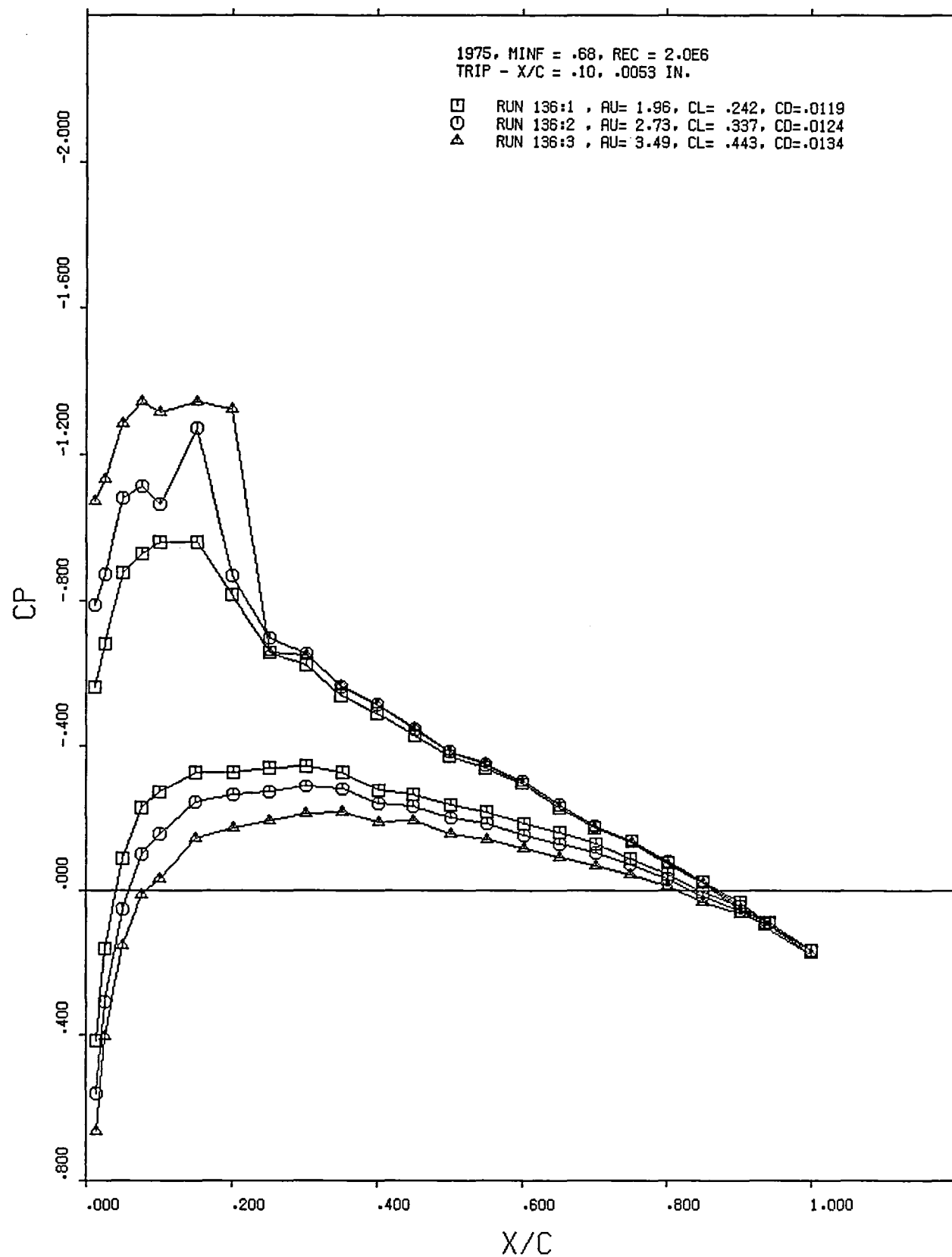




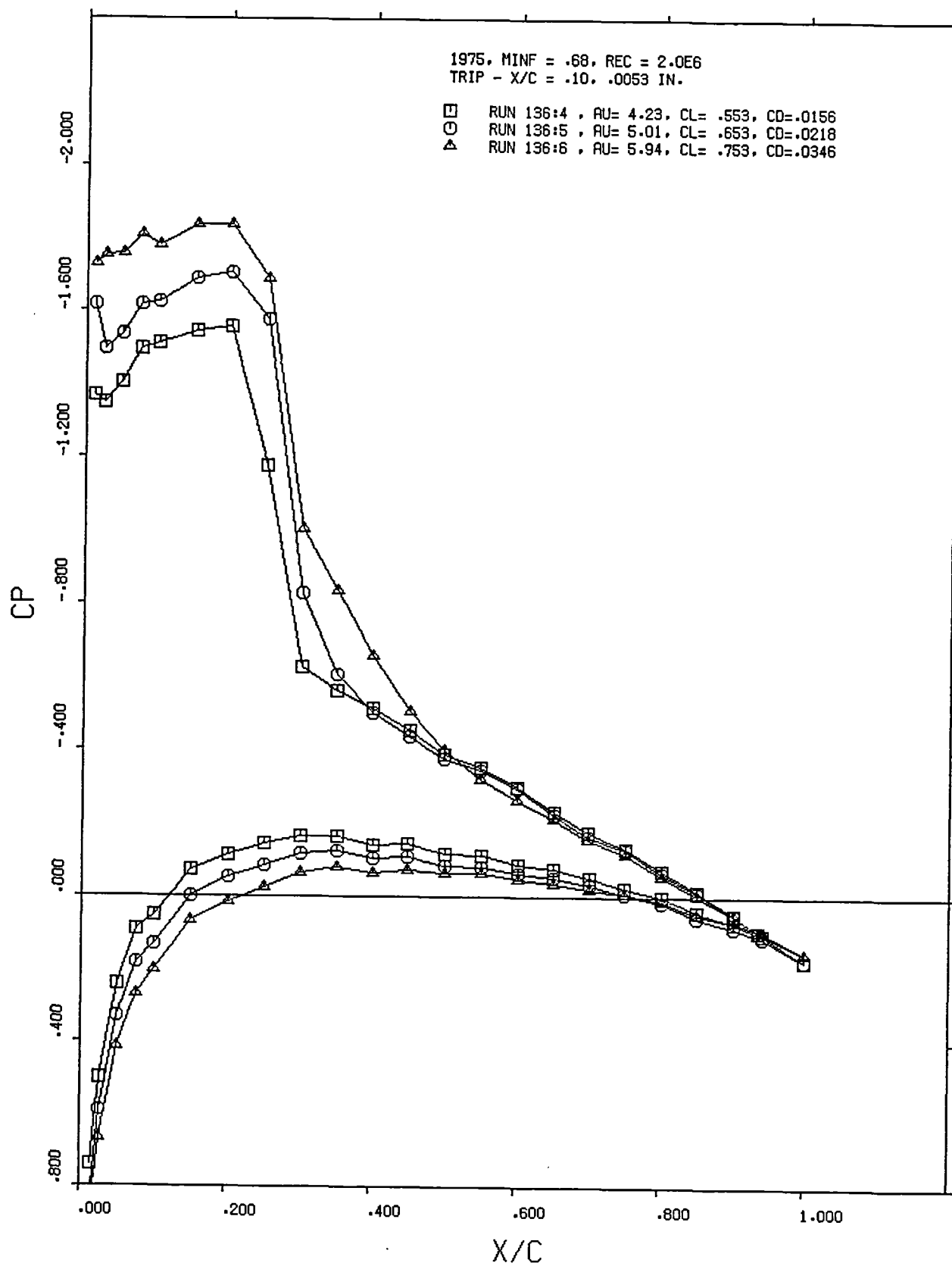


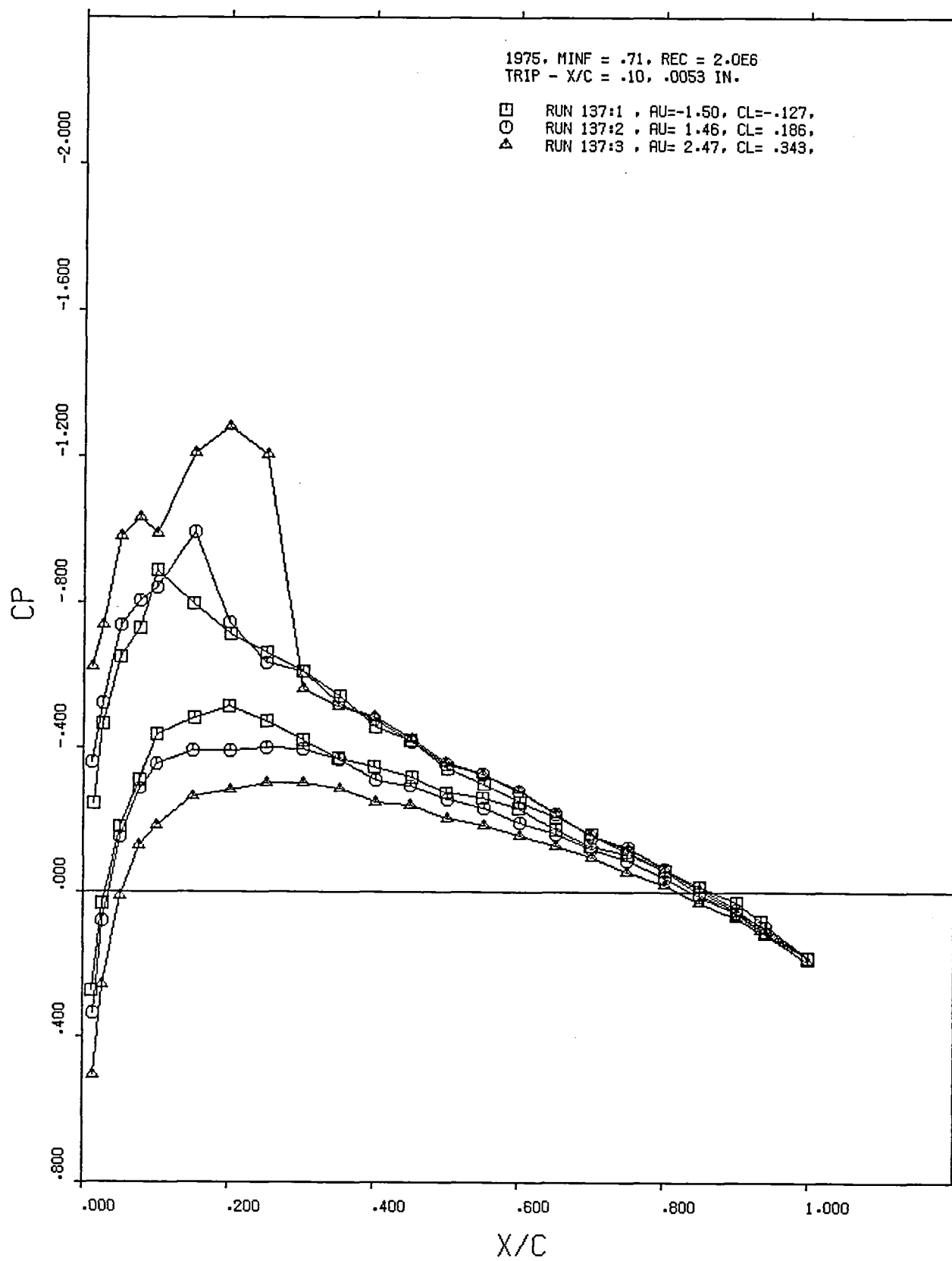


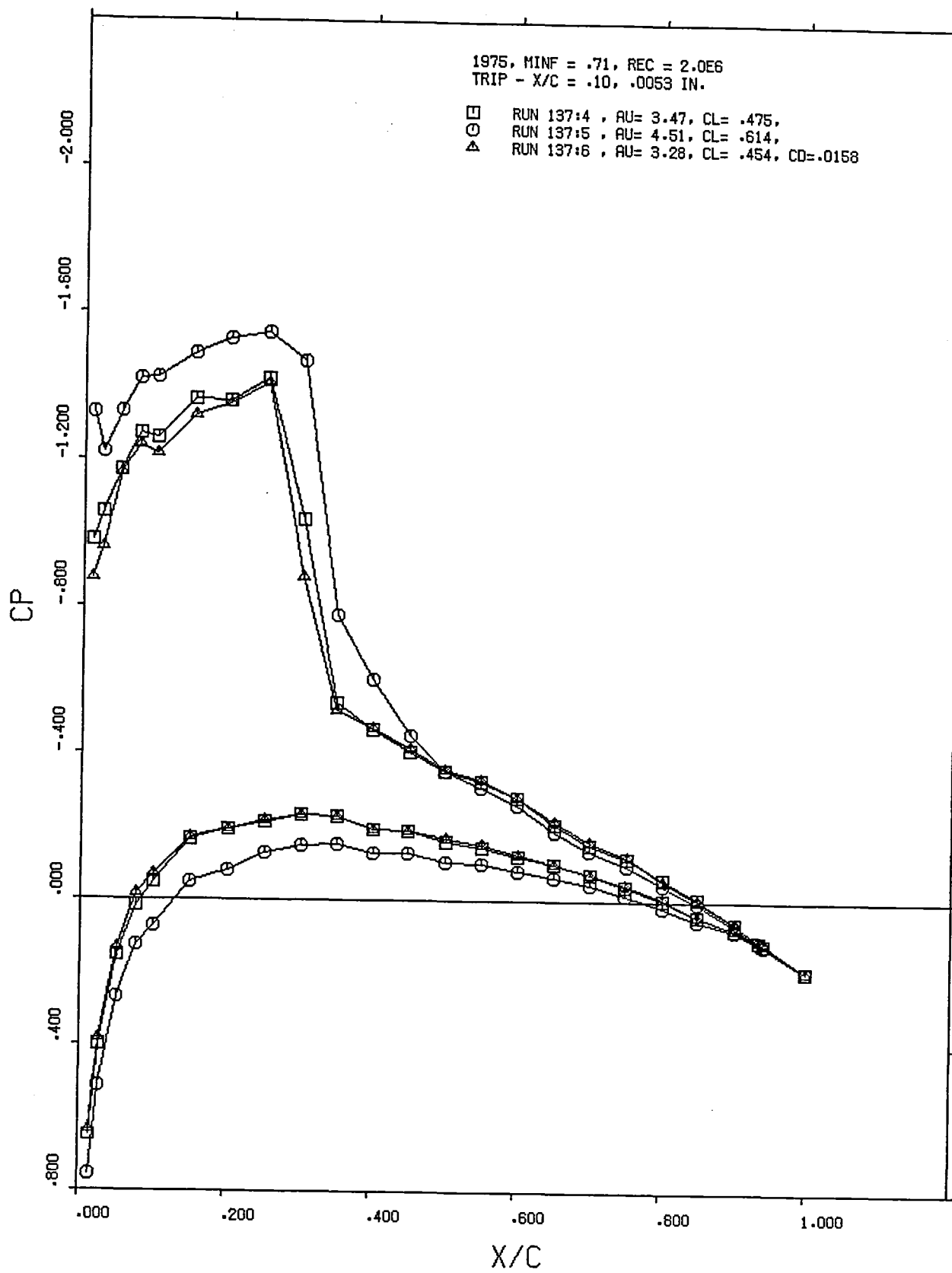


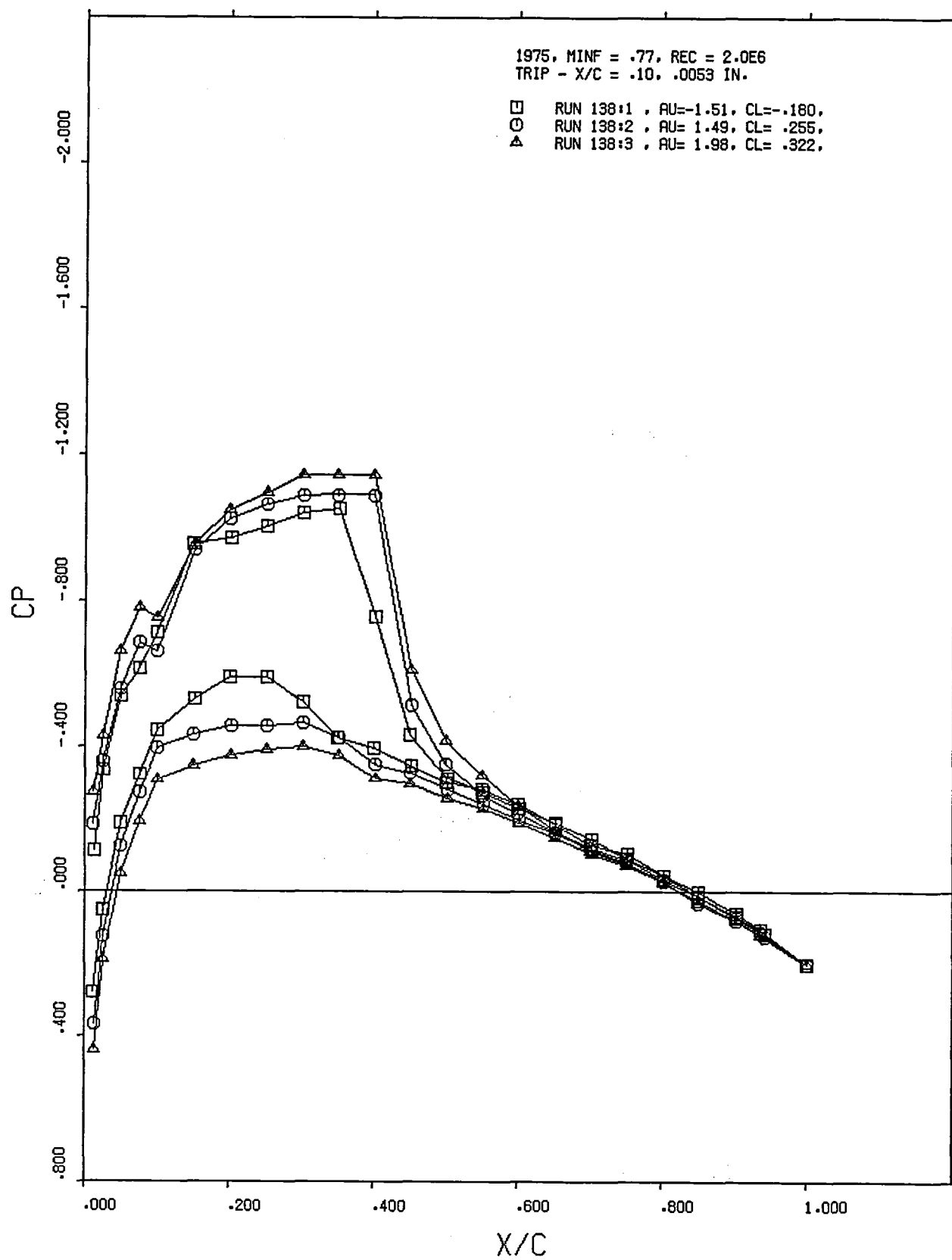


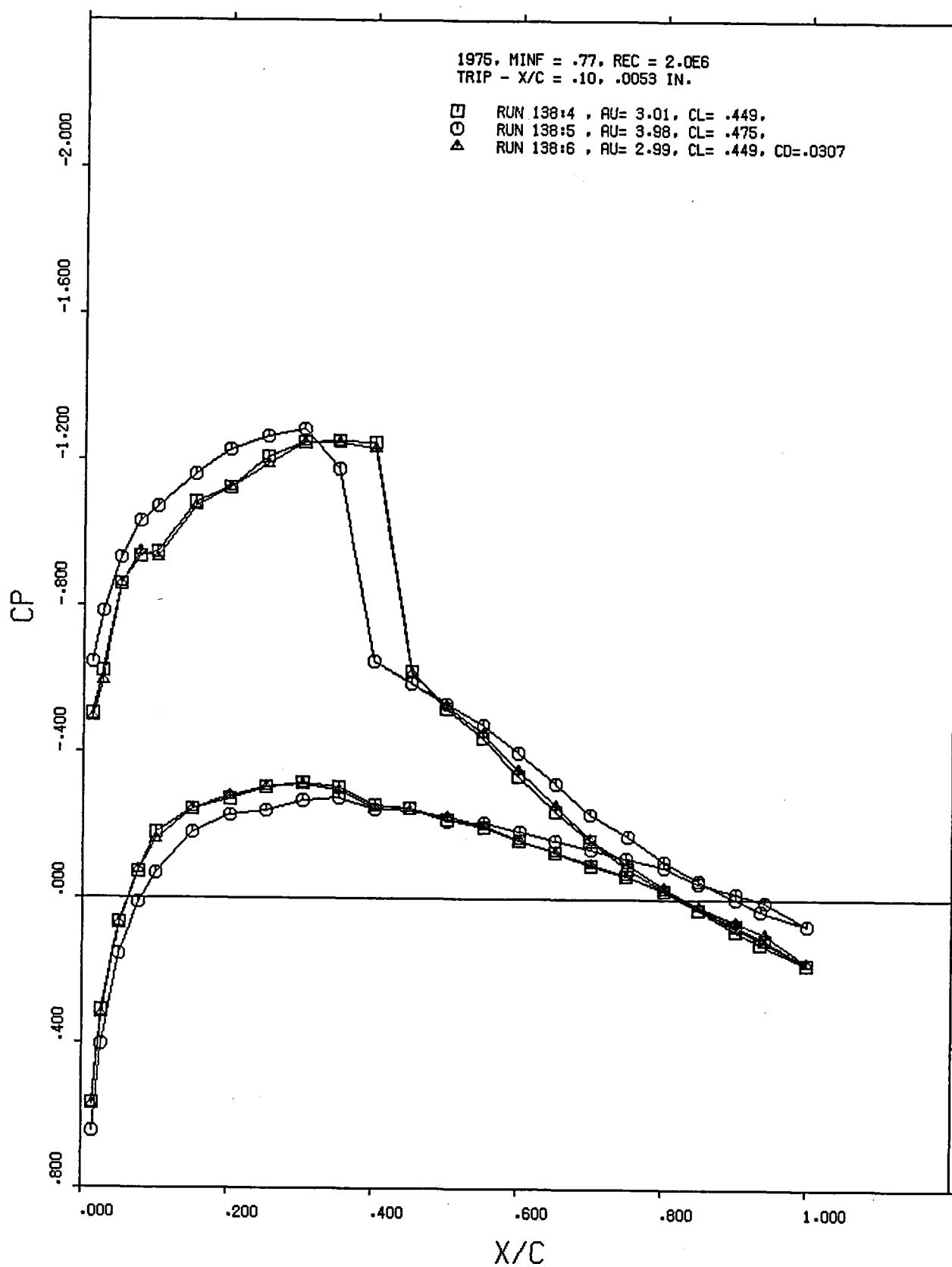


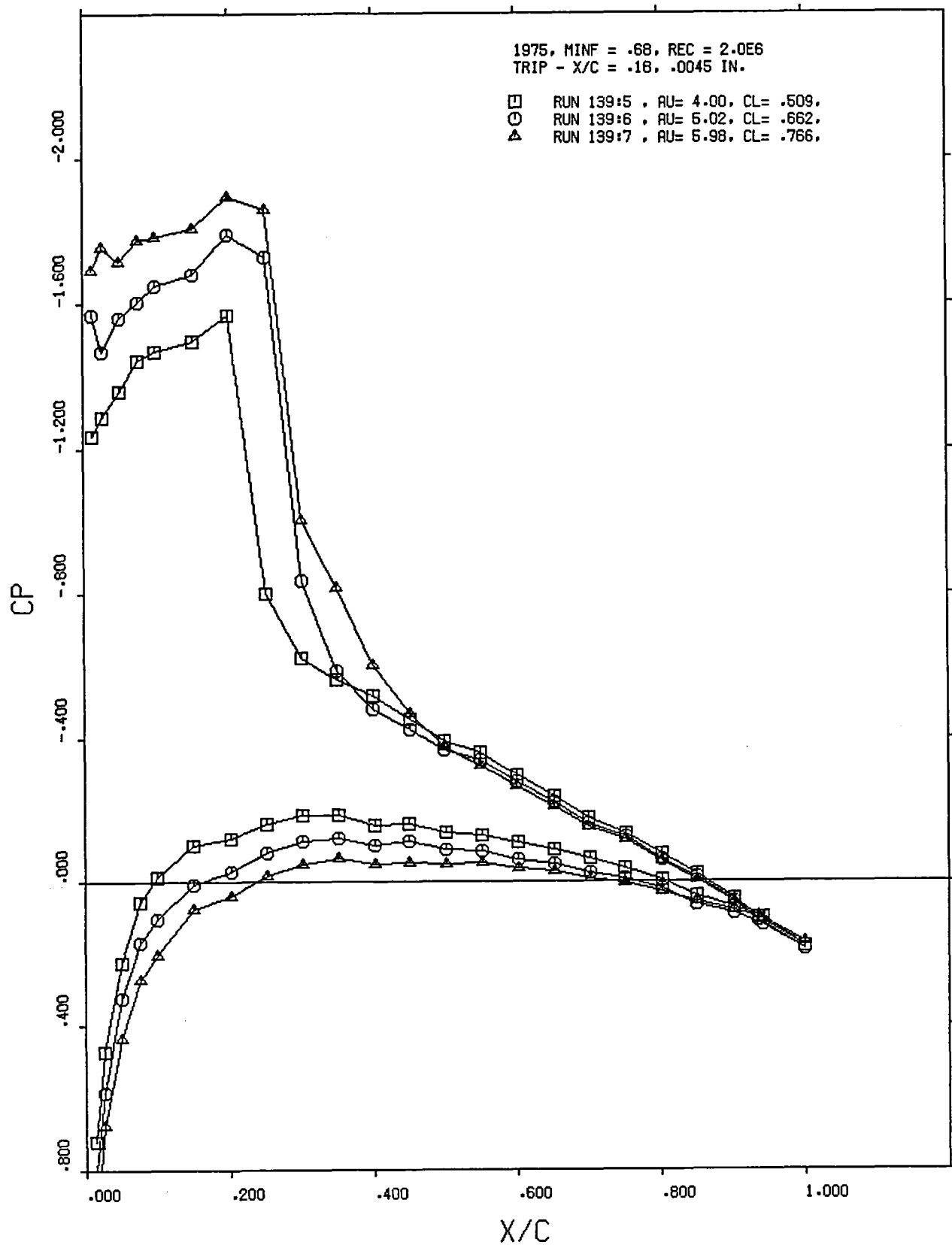


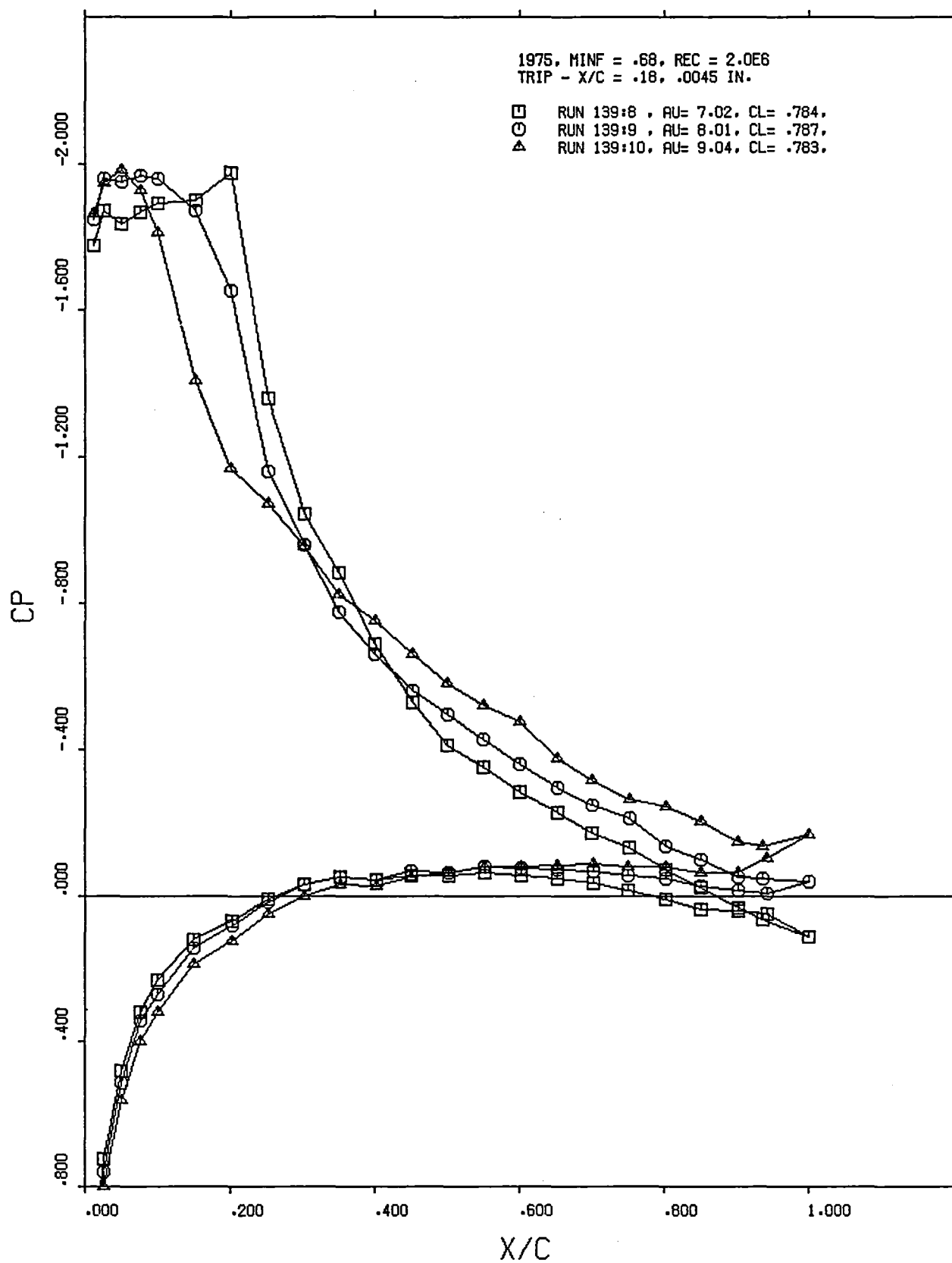


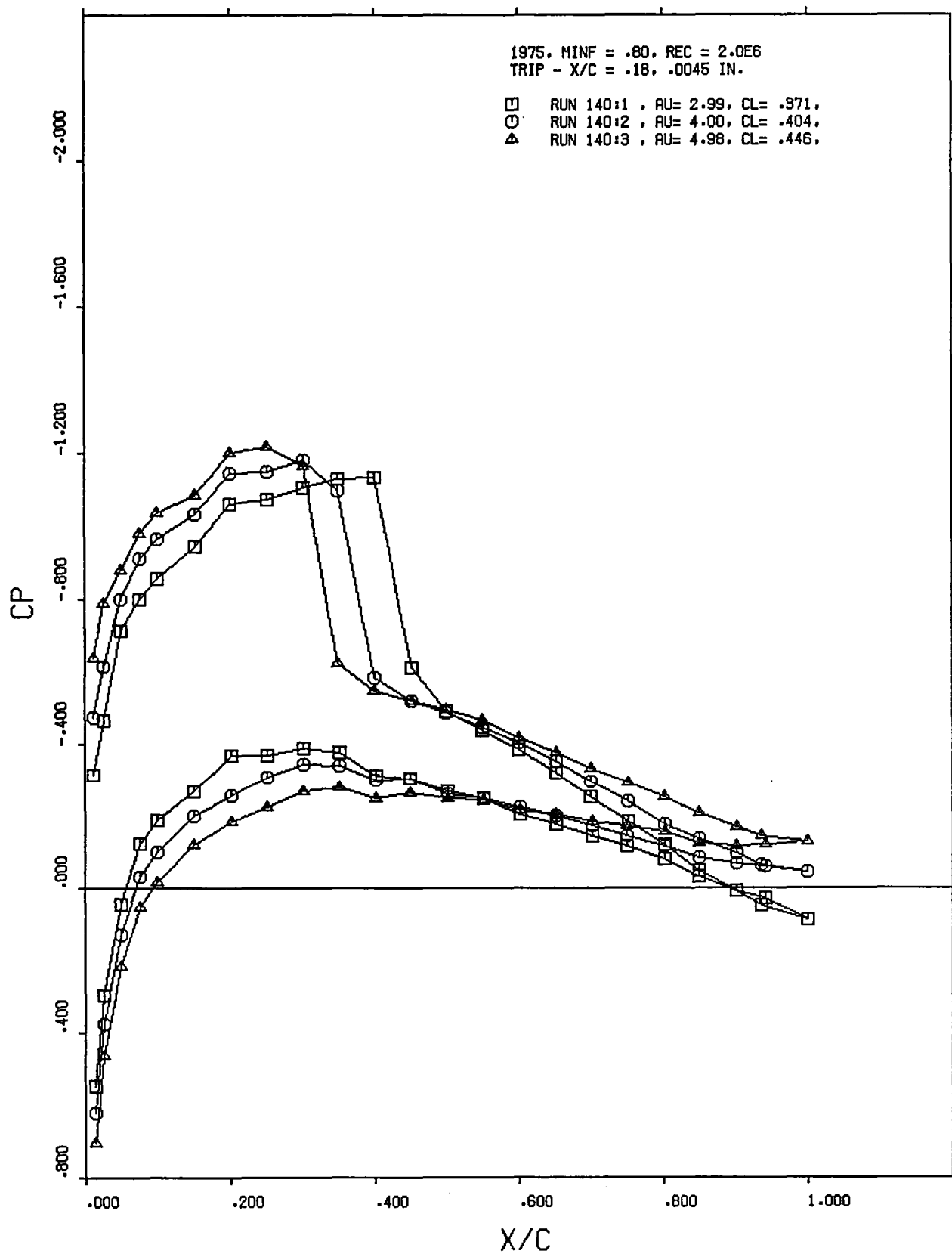




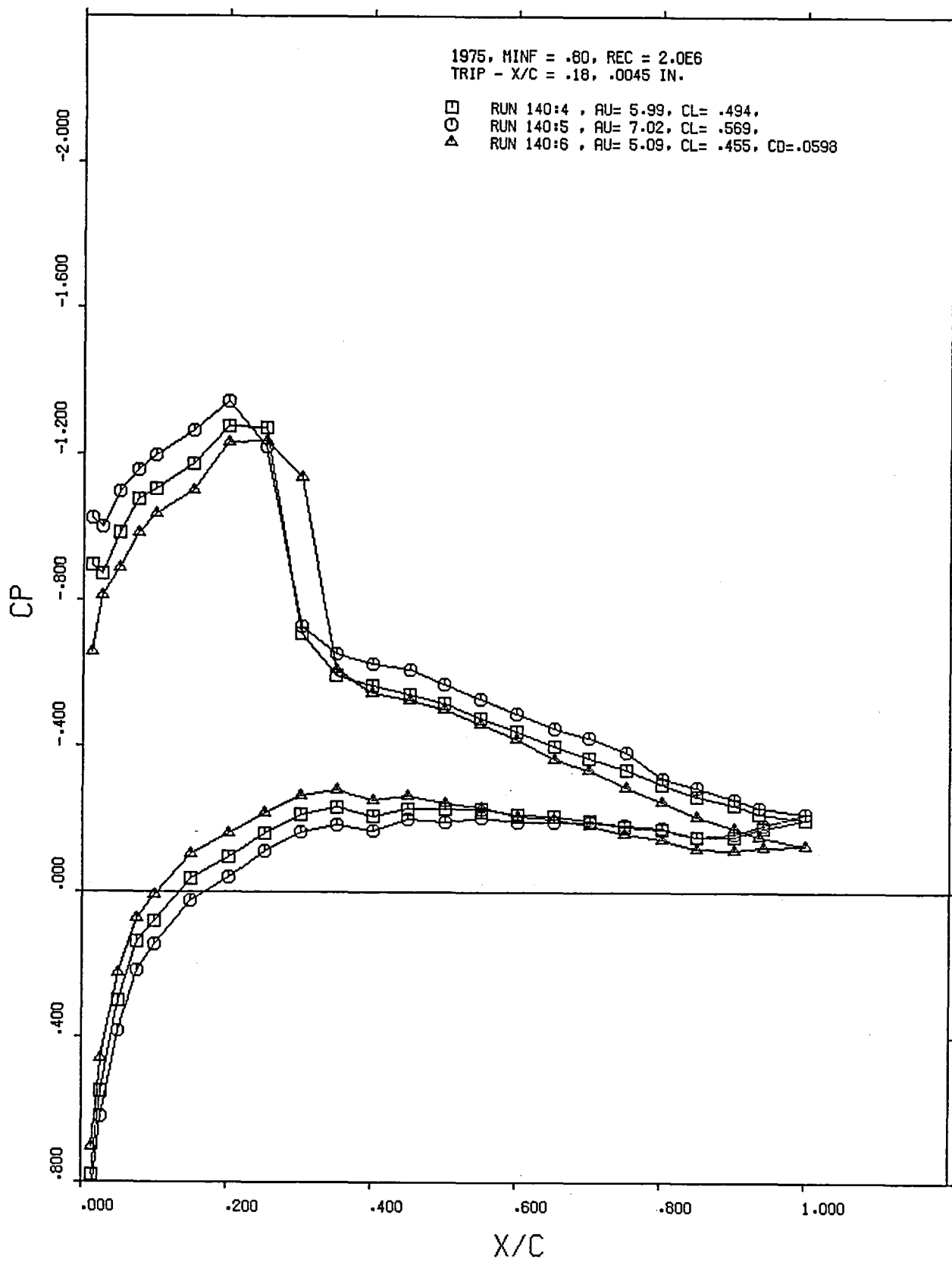


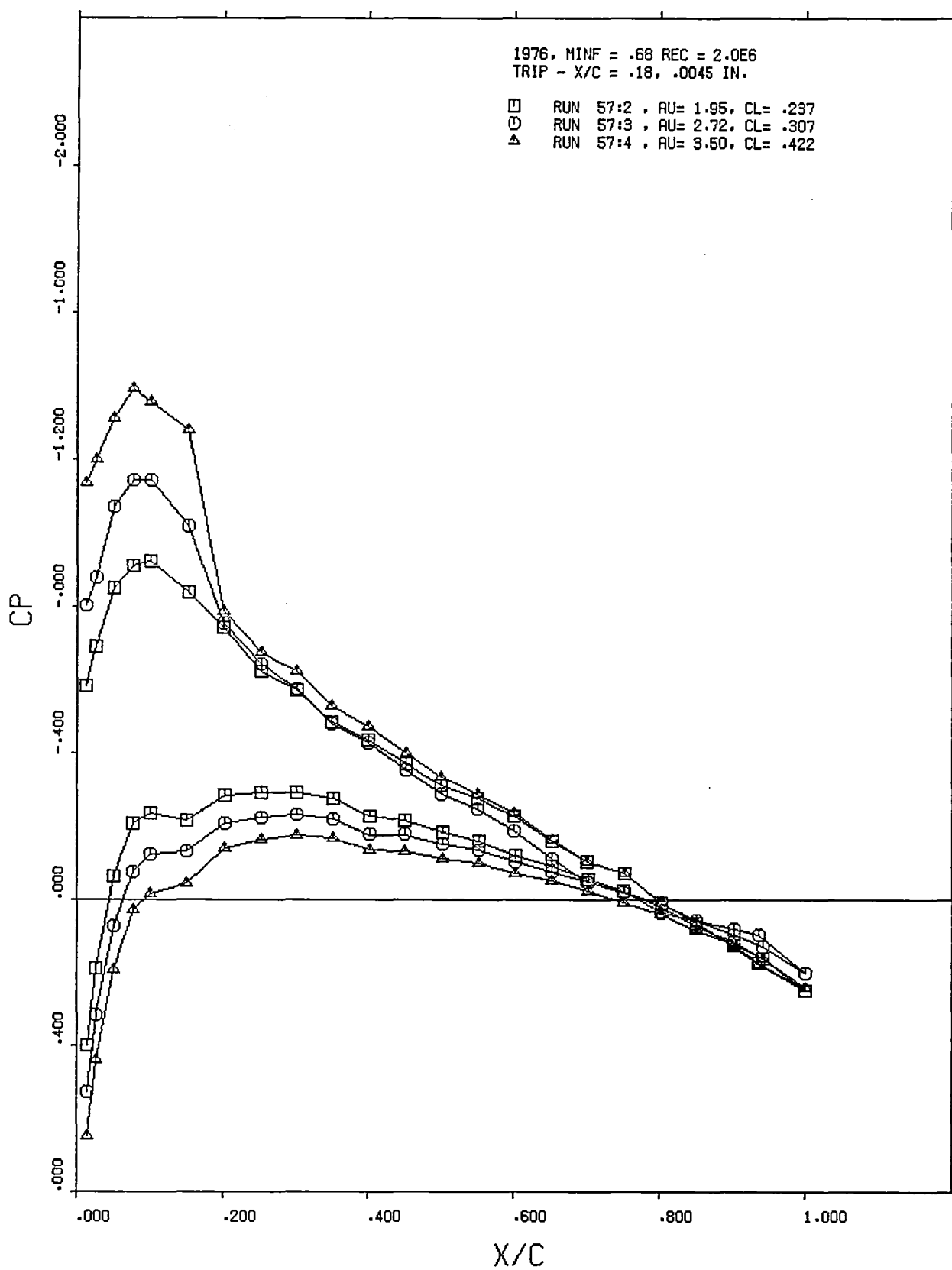


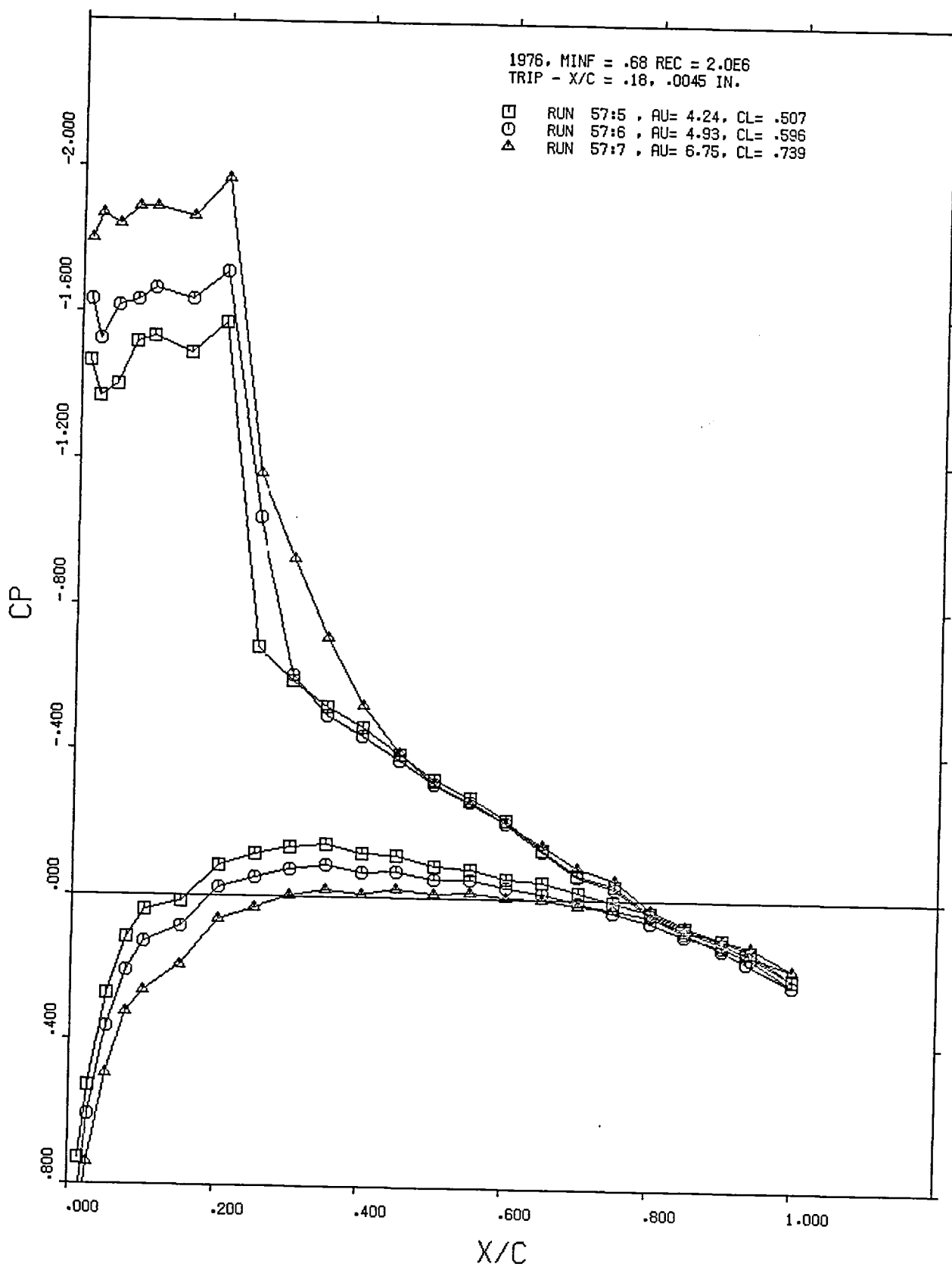


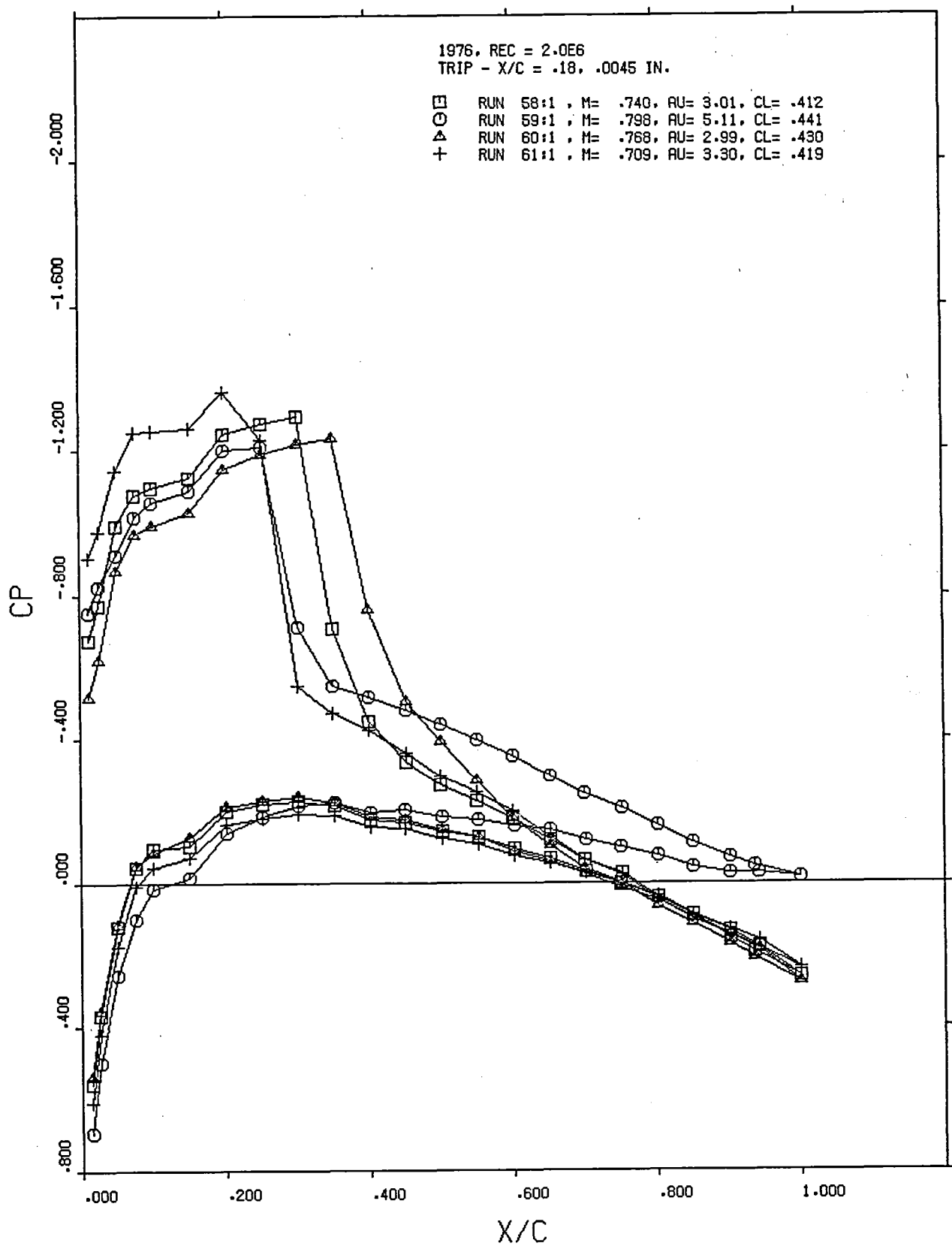


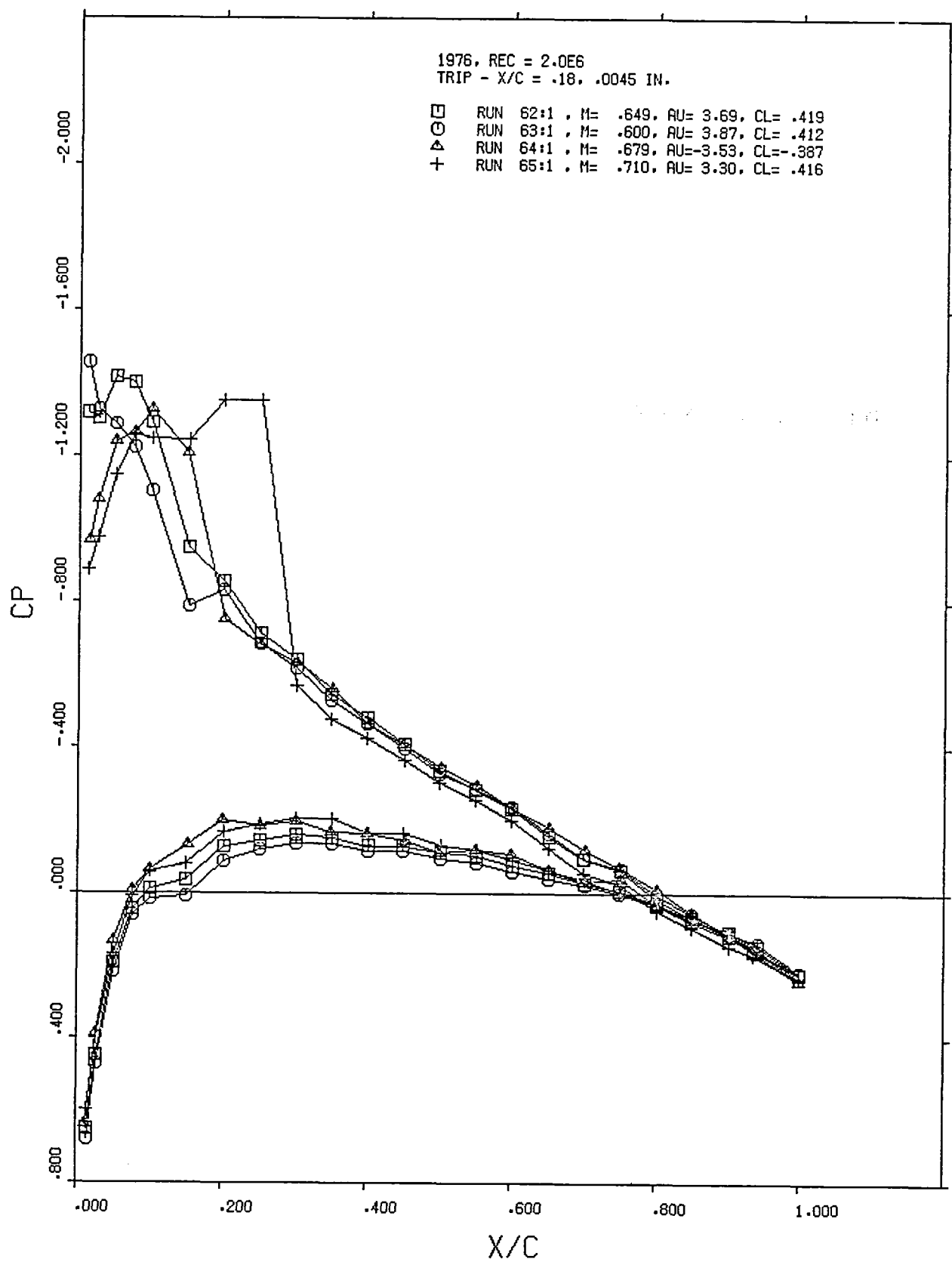












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